Locally Linearized Longitudinal and Lateral-Directional Aerodynamic Stability and Control Derivatives for the X-29A Aircraft

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VILLE AND DESCRIPTIONS

Gerald D. Budd

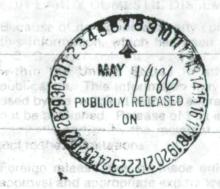
(NASA-TM-84919) LOCALLY LINEARIZED LONGITUDINAL AND LATERAL-DIRECTIONAL AERODYNAMIC STABILITY AND CONTROL DERIVATIES

N86-23566

FOR THE X-29A AIRCRAFT (NASA) 480 p January 1984 CSCL 01A G3/02 HC A21/MF A01

Unclas





Locally Linearized Longitudinal and Lateral-Directional Aerodynamic Stability and Control Derivatives for the X-29A Aircraft

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National Aeronautics and Space Administration Ames Research Center Dryden Flight Research Facility Edwards, California 93523 The locally linearized longitudinal and lateral-directional aerodynamic stability and control derivatives for the X-29A aircraft were calculated for altitudes ranging from sea level to 50,000 ft, Mach numbers from 0.2 to 1.5, and angles of attack from -5° to 25°. Several other parameters were also calculated, including aerodynamic force and moment coefficients, control surface position, normal acceleration, static margin, and reference angle of attack.

INTRODUCTION

The unusual aerodynamic configuration and high degree of longitudinal instability of the X-29A aircraft make it desirable to have linear aerodynamic stability and control data for analysis purposes. Typically, aerodynamic simulation data packages are formatted with higher-order terms and nonlinear increment corrections.

A local, total-force-and-moment coefficient perturbation technique was used to linearize the aerodynamic stability and control derivatives. This technique was implemented on the batch simulation computer system at the NASA Dryden Flight Research Facility.

The nonlinear aerodynamic data were taken from reference 1 and subsequent updates. This data base has been active on Dryden's batch simulation since February 1983. Reference 1 was based on references 2 to 9. Reference 2 was the primary transonic wind tunnel data set. The wind tunnel tests are described in references 10 and 11.

This linearized plot package is interim because of anticipated revisions to the simulation data package.

NOMENCLATURE

an normal acceleration, g $b \qquad (\text{wing) span, ft}$ $\bar{c} \qquad \text{mean aerodynamic (geometric) chord, ft}$ $c_A \qquad \text{axial force coefficient, deg}^{-1}$ $c_{A_Q} = \frac{\partial c_A}{\partial \frac{Q\bar{c}}{2U}} \qquad \text{variation of axial force coefficient with pitch rate, rad}^{-1}$ $c_{A_Q} = \frac{\partial c_A}{\partial \alpha} \qquad \text{variation of axial force coefficient with angle of attack, deg}^{-1}$

$$\begin{array}{lll} C_{A_{\bar{G}}} &=& \frac{3 C_{A}}{3 \frac{4 C_{C}}{2 U}} & \mbox{variation of axial force coefficient with rate of change of} \\ C_{A_{\bar{G}_{C}}} &=& \frac{3 C_{A}}{3 \delta_{C}} & \mbox{variation of axial force coefficient with canard angle, deg^{-1}} \\ C_{A_{\bar{G}_{f}}} &=& \frac{3 C_{A}}{3 \delta_{f}} & \mbox{variation of axial force coefficient with flap angle, deg^{-1}} \\ C_{A_{\bar{G}_{S}}} &=& \frac{3 C_{A}}{3 \delta_{S}} & \mbox{variation of axial force coefficient with strake angle, deg^{-1}} \\ C_{D} &=& \frac{D}{QS} & \mbox{drag coefficient (airplane)} \\ C_{D_{Q}} &=& \frac{3 C_{D}}{3 \frac{QC}{2 U}} & \mbox{variation of drag coefficient with pitch rate, rad^{-1}} \\ C_{D_{\bar{G}_{C}}} &=& \frac{3 C_{D}}{3 \frac{C_{D}}{2 U}} & \mbox{variation of drag coefficient with rate of change of angle of attack, rad^{-1}} \\ C_{D_{\bar{G}_{C}}} &=& \frac{3 C_{D}}{3 \delta_{C}} & \mbox{variation of drag coefficient with canard angle, deg^{-1}} \\ C_{D_{\bar{G}_{f}}} &=& \frac{3 C_{D}}{3 \delta_{C}} & \mbox{variation of drag coefficient with flap angle, deg^{-1}} \\ C_{D_{\bar{G}_{g}}} &=& \frac{3 C_{D}}{3 \delta_{S}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{\bar{G}_{g}}} &=& \frac{3 C_{D}}{3 \delta_{S}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{\bar{G}_{g}}} &=& \frac{3 C_{D}}{3 \delta_{S}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{\bar{G}_{g}}} &=& \frac{1}{3 C_{D}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{\bar{G}_{g}}} &=& \frac{1}{3 C_{D}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{\bar{G}_{g}}} &=& \frac{1}{3 C_{D}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{\bar{G}_{g}}} &=& \frac{1}{3 C_{D}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{\bar{G}_{g}}} &=& \frac{1}{3 C_{D}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{G}_{g}} &=& \frac{1}{3 C_{D}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}} \\ C_{D_{G}_{g}} &=& \frac{1}{3 C_{D}} & \mbox{variation of drag coefficient with strake angle, deg^{-1}}$$

variation of lift coefficient with pitch rate, rad $^{-1}$

 $c_{\mathbf{L}^{\mathbf{d}}} = \frac{9 \frac{3c}{d\underline{c}}}{9c^{\mathbf{L}}}$

$$\begin{array}{lll} & \frac{\partial c_L}{\partial \alpha} & \text{airplane lift curve slope, deg}^{-1} \\ & \frac{\partial c_L}{\partial \frac{\partial c}{\partial 2U}} & \text{variation of lift coefficient with rate of change of angle of attack, rad}^{-1} \\ & \frac{\partial c_L}{\partial c} & \frac{\partial c_L}{\partial \delta c} & \text{variation of lift coefficient with canard angle, deg}^{-1} \\ & \frac{\partial c_L}{\partial \delta_c} & \text{variation of lift coefficient with flap angle, deg}^{-1} \\ & \frac{\partial c_L}{\partial \delta_c} & \text{variation of lift coefficient with strake angle, deg}^{-1} \\ & \frac{\partial c_L}{\partial \delta_c} & \text{variation of lift coefficient with strake angle, deg}^{-1} \\ & \frac{\partial c_L}{\partial \delta_c} & \text{variation of lift coefficient with strake angle, deg}^{-1} \\ & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with roll rate} \\ & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with yaw rate} \\ & C_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with sideslip angle (i.e., dihedral angle), deg}^{-1} \\ & C_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with alleron angle (i.e., lateral control power), deg}^{-1} \\ & C_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder angle, deg}^{-1} \\ & C_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \frac{\partial c_L}{\partial \delta_c} & \text{variation of rolling moment coefficient with rudder} \\ & c_L & \frac{\partial c_L}{\partial \delta_c} & \frac{\partial c_L}{\partial \delta_c} & \frac{\partial c_L}{\partial \delta_c} & \frac{\partial c_L}{\partial \delta_c$$

$$C_{m_q} = \frac{\partial C_m}{\partial \frac{q\bar{c}}{2U}}$$
 variation of pitching moment coefficient with pitch rate, rad⁻¹

$$C_{m_{G}} = \frac{\partial c_{m}}{\partial \alpha} \qquad \text{variation of pitching moment coefficient with angle of attack (i.e., static longitudinal stability), deg^{-1}$$

$$C_{m_{G}} = \frac{\partial c_{m}}{\partial \frac{\partial c_{m}}{\partial c}} \qquad \text{variation of pitching moment coefficient with rate of change of angle of attack, rad^{-1} }$$

$$C_{m_{G}} = \frac{\partial c_{m}}{\partial c} \qquad \text{variation of pitching moment coefficient with canard angle (i.e., longitudinal control power), deg^{-1} }$$

$$C_{m_{G}} = \frac{\partial c_{m}}{\partial \delta_{g}} \qquad \text{variation of pitching moment coefficient with flap angle (i.e., longitudinal control power)}$$

$$C_{m_{G}} = \frac{\partial c_{m}}{\partial \delta_{g}} \qquad \text{variation of pitching moment coefficient with strake angle (i.e., longitudinal control power), deg^{-1} }$$

$$C_{n} = \frac{N}{g_{S}} \qquad \text{variation of normal force coefficient}$$

$$C_{n} = \frac{\partial c_{n}}{\partial c_{s}} \qquad \text{variation of normal force coefficient with pitch roll, rad^{-1} }$$

$$C_{n_{G}} = \frac{\partial c_{n}}{\partial c_{s}} \qquad \text{variation of yawing moment coefficient with roll rate}$$

$$C_{n_{G}} = \frac{\partial c_{n}}{\partial c_{s}} \qquad \text{variation of yawing moment coefficient with yaw rate}$$

$$c_{N_{\alpha}} = \frac{\partial c_{N}}{\partial c_{N}}$$
 variation of normal force coefficient with angle of attack, deg⁻¹

$$C_{N_{\alpha}} = \frac{\partial C_{N}}{\partial \alpha C}$$
 variation of normal force coefficient with rate of change of angle of attack, rad⁻¹

$$c_{N\delta_C} = \frac{\partial c_N}{\partial s}$$
 variation of normal force coefficient with canard angle, deg⁻¹

$c_{N\delta_f} = \frac{\partial c_N}{\partial \delta_f}$	variation of normal force coefficient with flap angle, deg^{-1}
$C_{N\delta_{S}} = \frac{\partial_{C_{N}}}{\partial \delta_{S}}$	variation of normal force coefficient with strake angle, deg-1
$C_{n\beta} = \frac{\partial C_n}{\partial \beta}$	variation of yawing moment coefficient with sideslip angle, deg-1
C _{nβ} DYNAMIC =	$C_{n_{\beta}} \cos \alpha - C_{\ell_{\beta}} \sin \alpha \frac{I_{zz}}{I_{xx}}$ (dutch roll stability parameter)
$c_{n\delta_{a}} = \frac{\partial c_{n}}{\partial \delta_{a}}$	variation of yawing moment coefficient with aileron angle, deg-1
$c_{n\delta_{r}} = \frac{\partial c_{n}}{\partial \delta_{r}}$	variation of yawing moment coefficient with rudder angle, deg-1
$C_{y} = \frac{F_{y}}{\overline{q}s}$	side force coefficient
20	variation of side force coefficient with roll rate
$C_{Yr} = \frac{\partial C_{Y}}{\partial \frac{rb}{2u}}$	variation of side force coefficient with yaw rate
$C_{Y\beta} = \frac{\partial C_{Y}}{\partial \beta}$	variation of side force coefficients with sideslip angle, deg^{-1}
$c_{y\delta_a} = \frac{\partial c_y}{\partial \delta_a}$	variation of side force coefficient with aileron angle, deg^{-1}
$c_{y\delta_r} = \frac{\partial c_y}{\partial \delta_r}$	variation of side force coefficient with rudder angle, deg-1
D .	drag, lb
Fy	side force along Y-axis, lb
g	acceleration of gravity, ft/sec ²
I _{xx} ,I _{yy} ,I _{zz}	moments of inertia about X, Y, Z axes, respectively, slug-ft ²

lift, 1b L L rolling moment, ft-lb pitching moment, ft-lb М M# Mach number mean aerodynamic (geometric) chord, ft MAC normal force, 1b roll rate, rad/sec р pitch rate, rad/sec q dynamic pressure, lb/ft2 $\bar{\mathbf{q}}$ yaw rate, rad/sec r reference (wing) area, ft² S forward velocity (along X-axis), ft/sec U WT weight, lb center of gravity location along X-axis, in XCG. angle of attack, deg β sideslip angle, deg $\delta_{\mathbf{a}}$ aileron deflection, deg $\delta_{\mathbf{C}}$ canard deflection, deg δf flap deflection, deg $\delta_{\mathbf{r}}$ rudder deflection, deg δs strake deflection, deg air density, slug/ft3 ρ

FIGURES

Figure	Description	Unit
1	c_L vs. c_D	
2	C _M vs. C _L	•
3	A _n vs. Alpha	g .
4	Alpha vs. Mach number	deg
5	Static margin vs. Mach number	percent MAC
6	Static margin vs. Alpha	percent MAC
7	Delta canard vs. Mach number	deg
8	Delta canard vs. Alpha	deg
9	Delta flap vs. Mach number	deg
10	Delta flap vs. Alpha	deg
11	Delta strake vs. Mach number	deg
12	Delta strake vs. Alpha	deg
13	C _L -lift vs. Mach number	
14	C _L -lift vs. Alpha	one that the
15	C _D vs. Mach number	jage dader vangr
16	C _D vs. Alpha	~~~
17	C _M vs. Mach number	Alle dans wish
18	C _M vs. Alpha	100 mg mg
19	CA vs. Mach number	
20	CA vs. Alpha	00a tar 400
21	C _N -normal vs. Mach number	
22	C _N -normal vs. Alpha	
23	C _L -canard vs. Mach number	per deg
24	C _L -canard vs. Alpha	per deg
25	CD-canard vs. Mach number	per deg

Figure	Description	Unit
26	C _D -canard vs. Alpha	per deg
27	C _M -canard vs. Mach number	per deg
28	C _M -canard vs. Alpha	per deg
29	CA-canard vs. Mach number	per deg
30	CA-canard vs. Alpha	per deg
31	C _N -canard vs. Mach number	per deg
32	C _N -canard vs. Alpha	per deg
33	C _L -flap vs. Mach number	per deg
34	C _L -flap vs. Alpha	per deg
35	C _D -flap vs. Mach number	per deg
36	C _D -flap vs. Alpha	per deg
37	C _M -flap vs. Mach number	per deg
38	C _M -flap vs. Alpha	per deg
39	CA-flap vs. Mach number	per deg
40	C _A -flap vs. Alpha	per deg
41	C _N -flap vs. Mach number	per deg
42	C _N -flap vs. Alpha	per deg
43	C _L -strake vs. Mach number	per deg
44	C _L -strake vs. Alpha	per deg
45	C _D -strake vs. Mach number	per deg
46	C _D -strake vs. Alpha	per deg
47	C _M -strake vs. Mach number	per deg
48	C _M -strake vs. Alpha	per deg
49	CA-strake vs. Mach number	per deg
50	C _A -strake vs. Alpha	per deg
51	C _N -strake vs. Mach number	per deg
52	C _N -strake vs. Alpha	per deg

Figure	Description	Unit
53	Cy-aileron vs. Mach number	per deg
54	Cy-aileron vs. Alpha	per deg
55	C ₁ -aileron vs. Mach number	per deg
56	C ₁ -aileron vs. Alpha	per deg
57	C _n -aileron vs. Mach number	per deg
58	C _n -aileron vs. Alpha	per deg
59	Cy-rudder vs. Mach number	per deg
60	Cy-rudder vs. Alpha	per deg
61 .	C ₁ -rudder vs. Mach	per deg
62	Cl-rudder vs. Alpha	per deg
63	Cn-rudder vs. Mach number	per deg
64	C _n -rudder vs. Alpha	per deg
65	C _L -alpha vs. Mach number	per deg
66	$C_{\mathbf{L}}$ -alpha vs. Alpha	per deg
67	CD-alpha vs. Mach number	per deg
68	C _D -alpha vs. Alpha	per deg
69	C _M -alpha vs. Mach number	per deg
70	C _M -alpha vs. Alpha	per deg
71	CA-alpha vs. Mach number	per deg
72	C _A -alpha vs. Alpha	per deg
73	C _N -alpha vs. Mach number	per deg
74	C _N -alpha vs. Alpha	per deg
75	Cy-beta vs. Mach number	per deg
76	Cy-beta vs. Alpha	per deg
77	C ₁ -beta vs. Mach number	per deg
78	C ₁ -beta vs. Alpha	per deg
79	Cn-beta vs. Mach number	per deg
•		

Figures	Description	<u>Unit</u>
80	C _n -beta vs. Alpha	per deg
81	Cn-beta dynamic vs. Mach number	per deg
82	C _n -beta dynamic vs. Alpha	per deg
83	C _L -alpha dot vs. Mach number	per deg
84	C _L -alpha dot vs. Alpha	per rad
85 [′]	C _D -alpha dot vs. Mach number	per rad
. 86	CD-alpha dot vs. Alpha	per rad
87	C _M -alpha dot vs. Mach number	per rad
88	C _M -alpha dot vs. Alpha	per rad
89	CA-alpha dot vs. Mach number	per rad
90	CA-alpha dot vs. Alpha	per rad
91	C _N -alpha dot vs. Mach number	per rad
92	C _N -alpha dot vs. Alpha	per rad
93	C _L -q vs. Mach number	per rad
94	C _L -q vs. Alpha	per rad
95	C _D -q vs. Mach number	per rad
96	C _D -q vs. Alpha	per rad
97	C _M -q vs. Mach number	per rad
98	C _M -q vs. Alpha	per rad
99	CA-q vs. Mach number	per rad
- 100	C _A -q vs. Alpha	per rad
101.	C _N -q vs. Mach Number	per rad
102	C _N -q vs. Alpha	per rad
103	Cy-roll rate vs. Mach number	per rad
104	Cy-roll rate vs. Alpha	per rad
105	C ₁ -roll rate vs. Mach number	per rad
106	C _l -roll rate vs. Alpha	per rad

Figure	Description	Unit
107	Cn-roll rate vs. Mach number	per rad
108	C _n -roll rate vs. Alpha	per rad
109	Cy-yaw vs. Mach number	per rad
110	C _y -yaw vs. Alpha	per rad
111	C ₁ -yaw vs. Mach number	per rad
112	C _l -yaw vs. Alpha	per rad
113	C _n -yaw vs. Mach number	per rad
114	C _n -yaw vs. Alpha	per rad
•		· .
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DISCUSSION AND RESULTS

The X-29A longitudinal and lateral-directional aerodynamic stability and control derivatives presented may be used for linear analysis purposes. It must be emphasized that the derivatives have been locally linearized about the trim points. All the data points presented are at a trim condition.

Two types of trimming procedures were used in the calculation of these derivatives: (1) straight-and-level trim, which is steady-state 1g trim at a specified altitude and Mach number; and (2) alpha trim which is steady, state trim to a specified angle of attack at a given altitude and Mach number.

Care should be exercised when using this interim data set to avoid confusion. Occasionally a trim data point was perturbated about a breakpoint in the nonlinear simulation aerodynamic data base. An example of this is figure 48(b), Cm-delta strake as a function of alpha for Mach 0.6 and an altitude of 10,000 ft. The perturbation caused the 14° alpha trim point to be displaced downward an extreme amount.

In addition, the scaling of the dependent variables (Y-axis) was not always consistent because of the automatic scaling procedure used.

CONCLUDING REMARKS

Locally linearized longitudinal and lateral-directional aerodynamic stability and control derivatives were calculated for the X-29A aircraft, along with several other parameters. Data were obtained for altitudes of sea level to 50,000 ft, Mach numbers from 0.2 to 1.5, and angles of attack ranging from -5° to 25°.

The aerodynamic characteristics of the aircraft appear to be consistent and reasonable, indicating that the linearization technique used was acceptable.

National Aeronautics and Space Administration Ames Research Center Dryden Flight Research Facility Edwards, Calif., August 24, 1983

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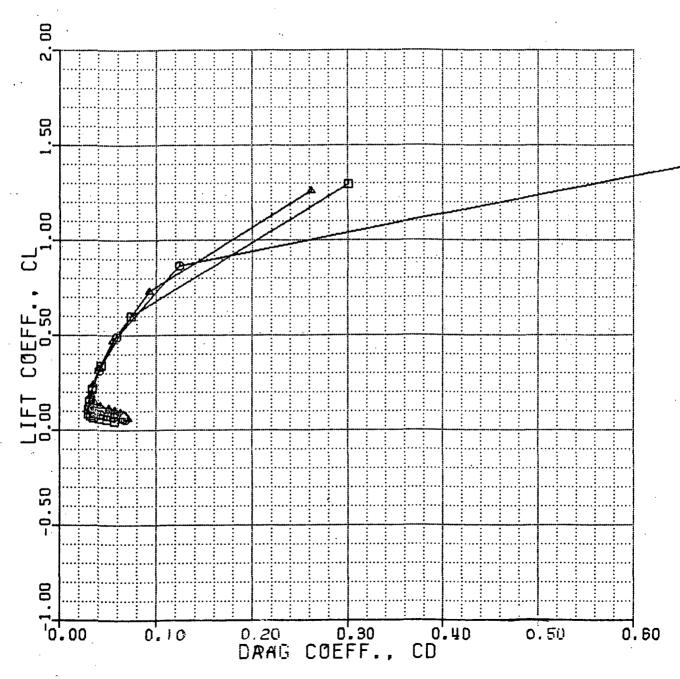
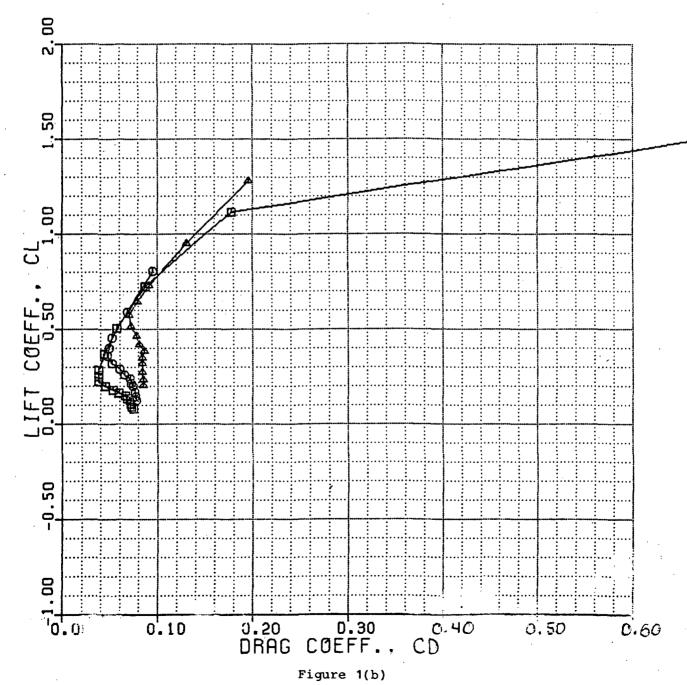


Figure 1(a)

```
CL VS CD
```

7-14-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5



CL VS CD

7-12-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

Q ALT = S.L. ALP: -4 TO 22 Q ALT = 10K ALP: -4 TO 22

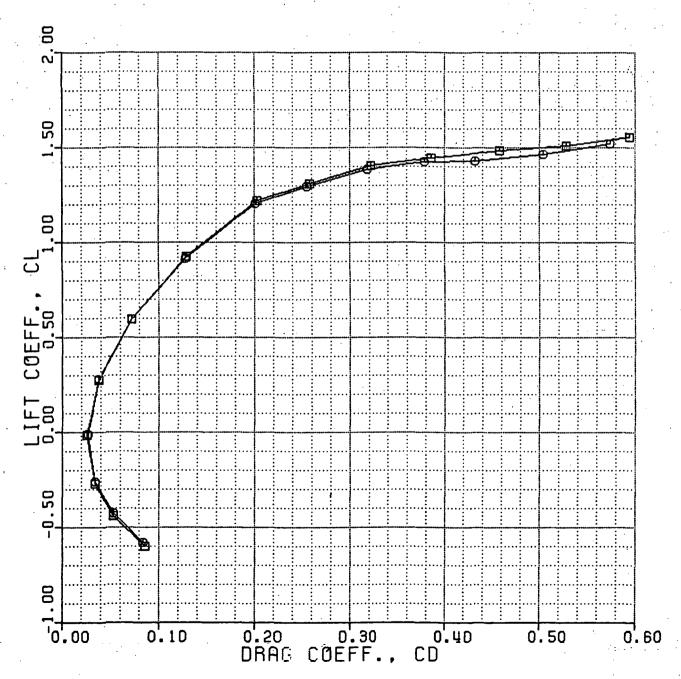


Figure 1(c)

CL VS CD

7-12-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 O ALT = 20K ALP: -4 TO 20

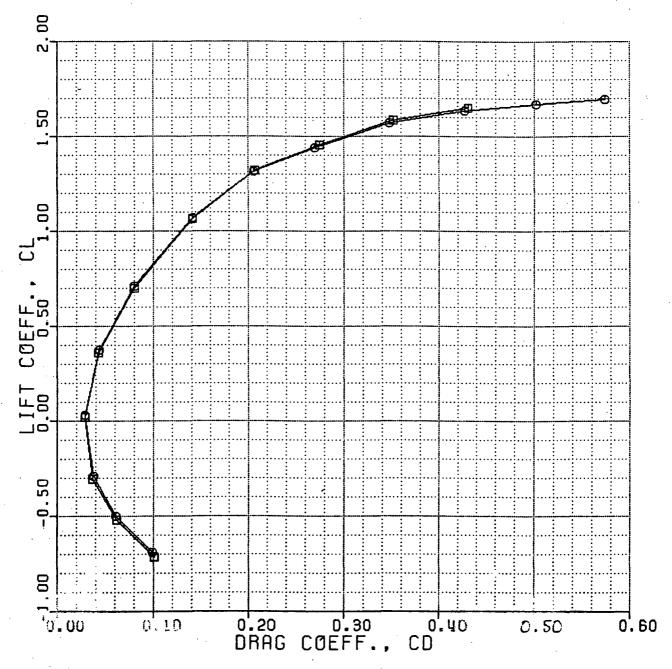


Figure 1(d)

```
CL VS CD
```

```
7-12-83 X-29A M# = 0.8 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM
```

```
P ALT = 10K ALP: 0 T0 10
P ALT = 20K ALP: -4 T0 12
ALT = 30K ALP: -4 T0 14
ALT = 40K ALP: -4 T0 18
ALT = 50K ALP: -4 T0 22
```

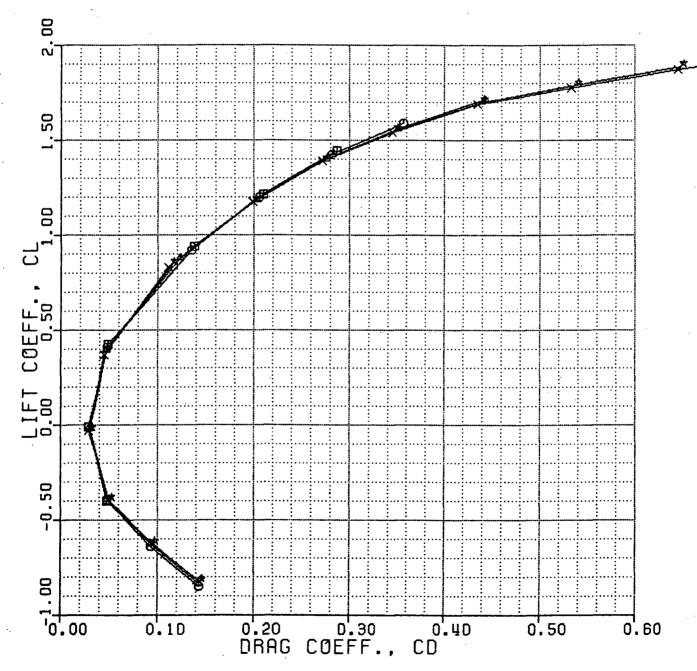


Figure 1(e)

ORIGINAL PAGE 19 OF POOR QUALITY

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CL VS CD
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7-14-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

PALT = 20K ALP: 0 T0 10

PALT = 30K ALP: -2 T0 12

ALT = 40K ALP: -4 T0 14

ALT = 50K ALP: -4 T0 18

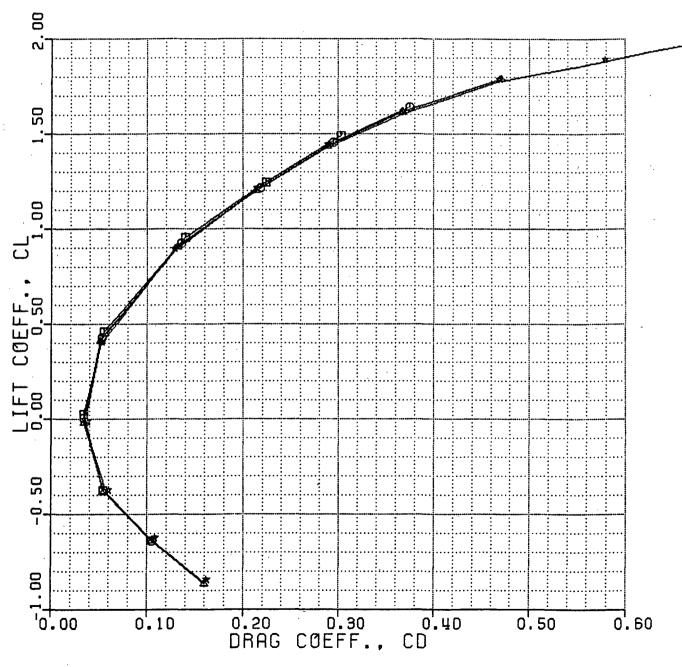


Figure 1(f)

CL VS CD

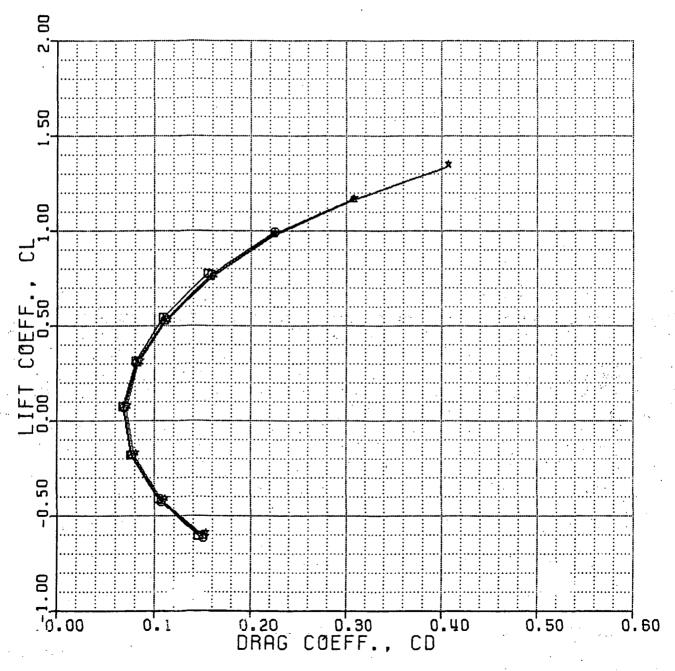
7-14-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14



CL VS CD

7-14-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8 9 ALT = 40K ALP: -4 TO 10 A ALT = 50K ALP: -4 TO 12

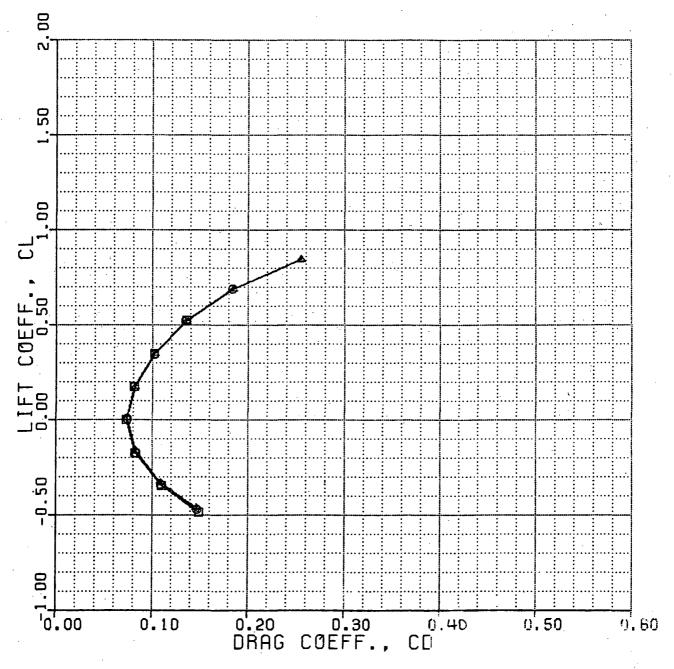


Figure 1(h)

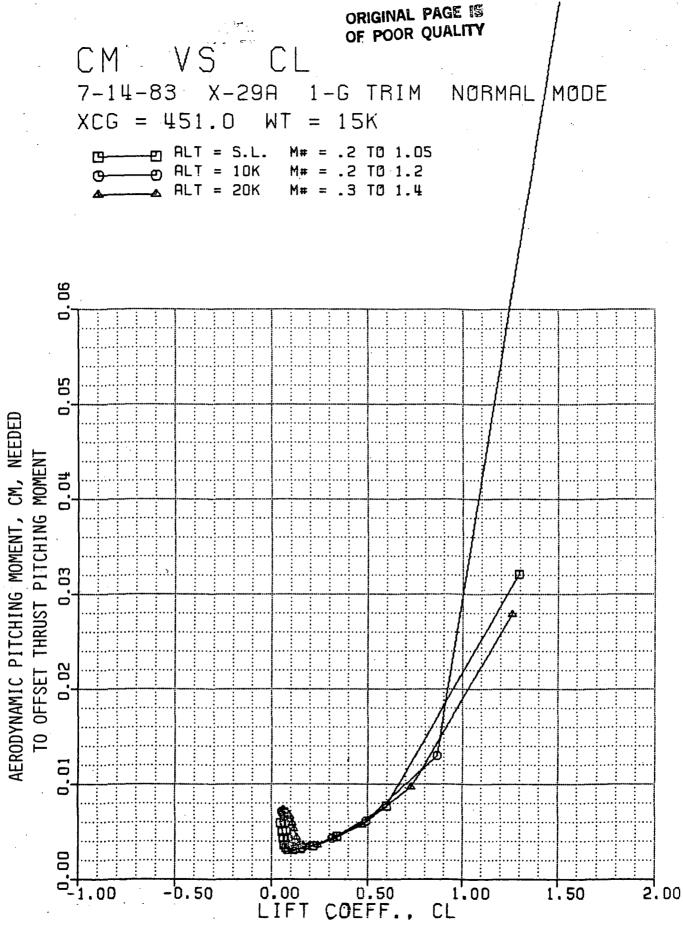


Figure 2(a)

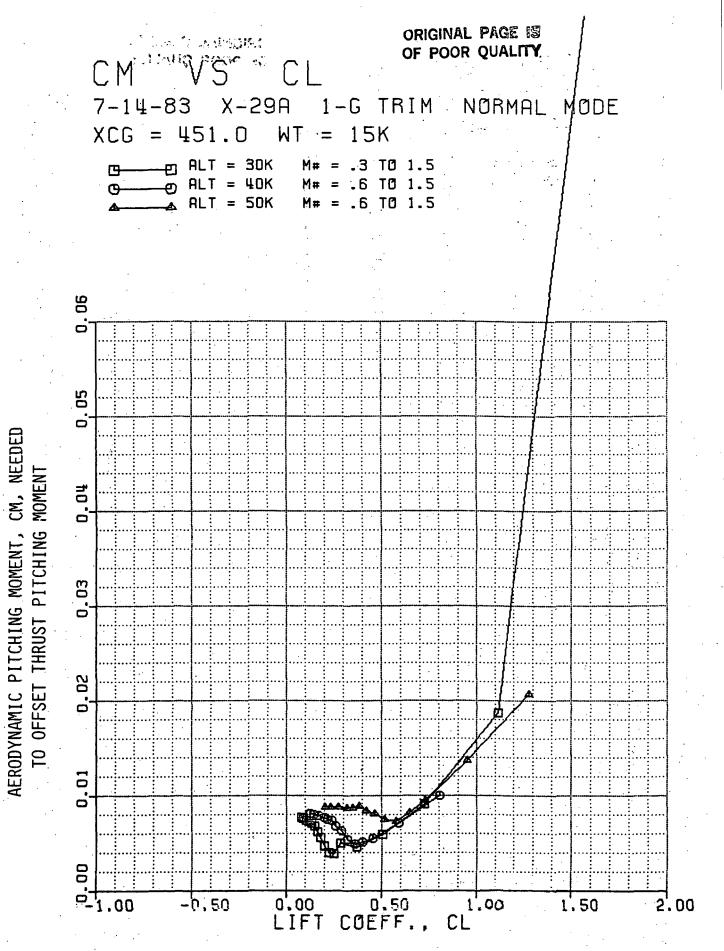
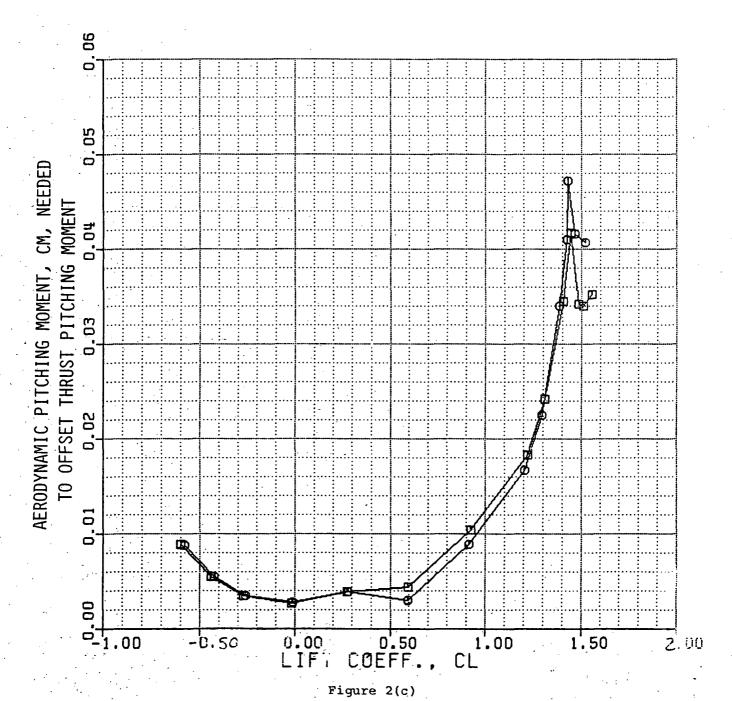


Figure 2(b)

CM VS CL ORIGINAL PAGE IS OF POOR QUALITY

7-12-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM



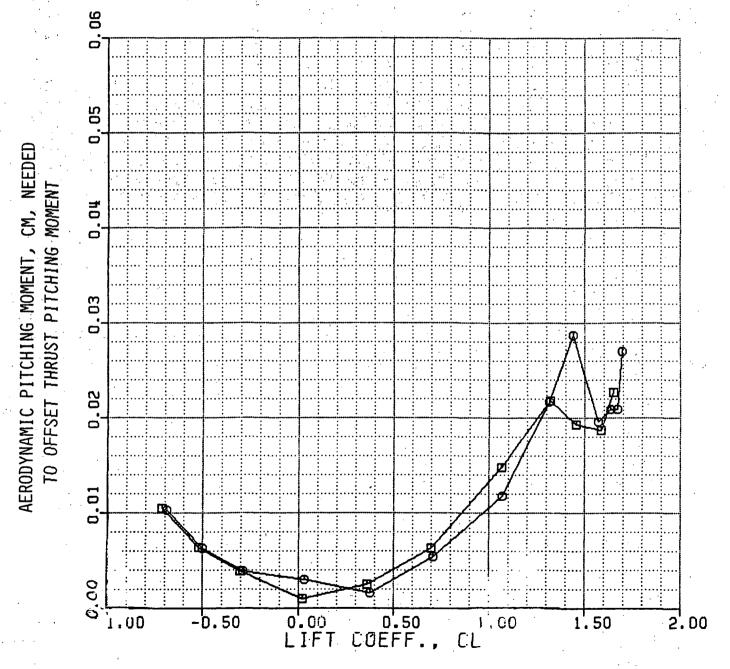


Figure 2(d)

ORIGINAL PAGE IS

CM VS CL

7-12-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P P RLT = 10K ALP: 0 T0 10

P P ALT = 20K ALP: -4 T0 12

A ALT = 30K ALP: -4 T0 14

A ALT = 40K ALP: -4 T0 18

A ALT = 50K ALP: -4 T0 22
```

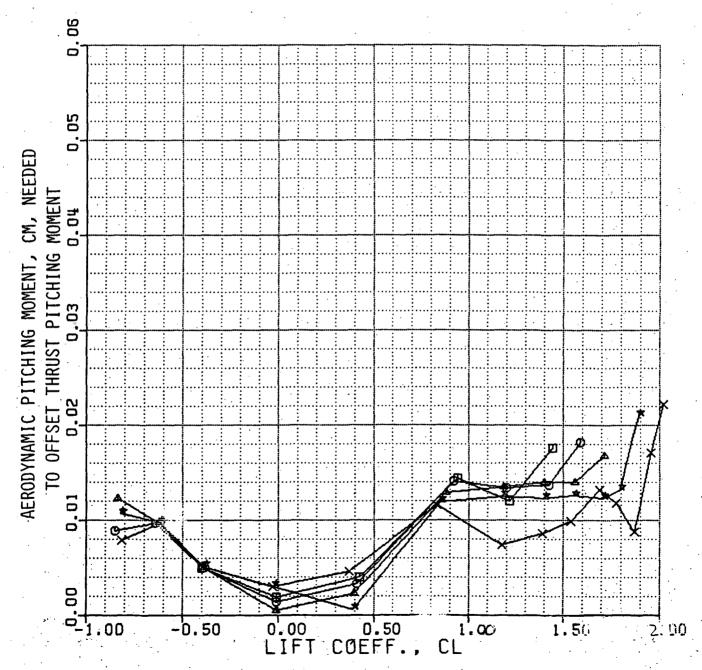


Figure 2(e)

CM VS CL

7-14-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: 0 T0 10

P ALT = 30K ALP: -2 T0 12

A ALT = 40K ALP: -4 T0 14

A ALT = 50K ALP: -4 T0 18

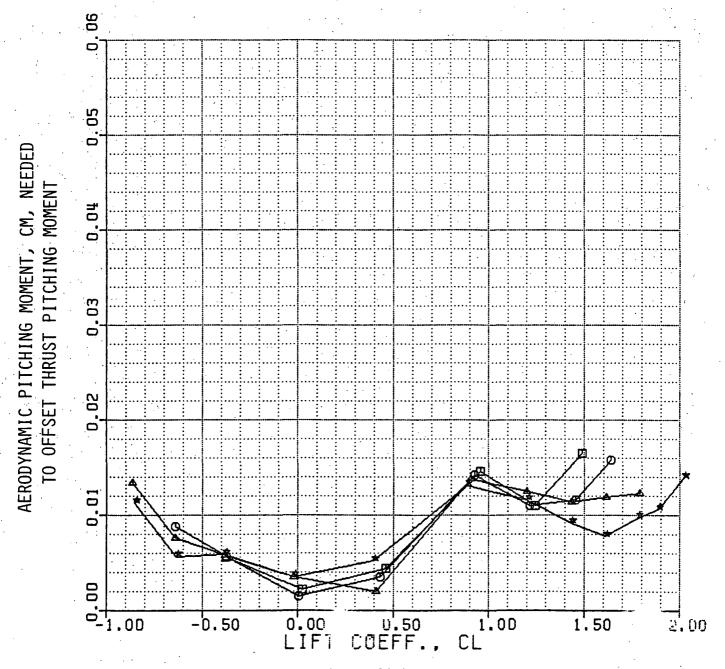


Figure 2(f)

```
CM
           X-29A
7-14-83
                    M# = 1.2
                                NORMAL MODE
                             ALPHA TRIM
XCG = 451.0
                WT =
                       15K
        ALT = 20K
        ALT = 30K
                  ALP: -4 TØ 10
                  ALP: -4 TØ 12
        ALT = 40K
       ★ ALT = 50K
                  ALP: -4 TO 14
```

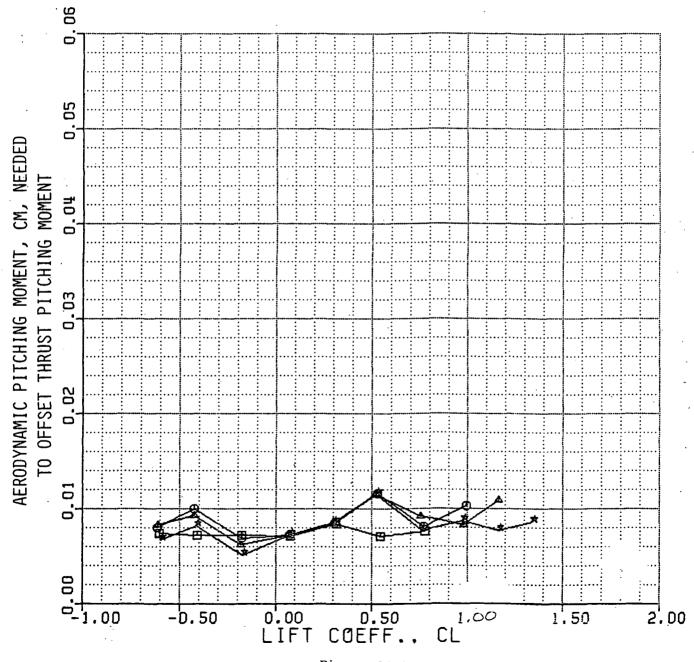


Figure 2(g)

ORIGINAL PAGE IS OF POOR QUALITY

CM VS CL

7-14-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8 9 ALT = 40K ALP: -4 TO 10 A ALT = 50K ALP: -4 TO 12

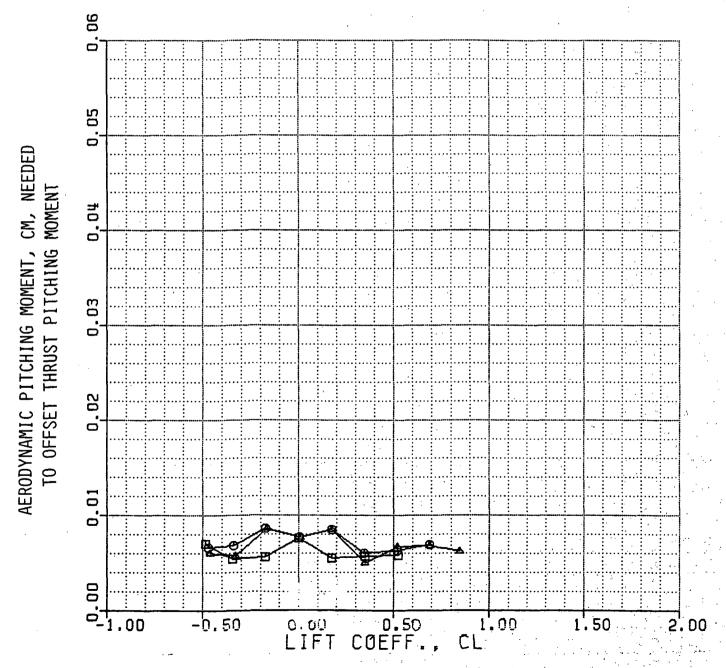


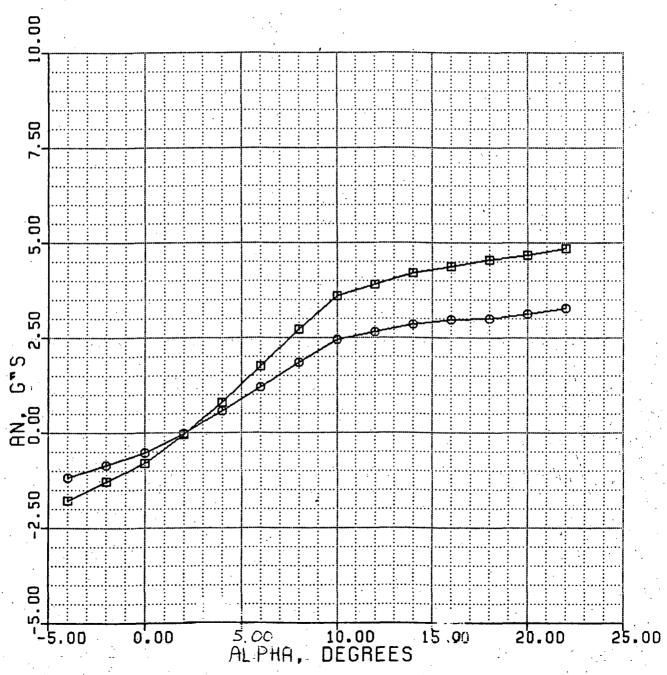
Figure 2(h)

ORIGINAL PAGE IS OF POOR QUALITY

AN VS ALPHA

7-12-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

n ALT = S.L. ALP: -4 TO 22 n ALT = 10K ALP: -4 TO 22



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AN VS ALPHA

7-12-83 X-29A M# = 0.6 NØRMAL MØDE

XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

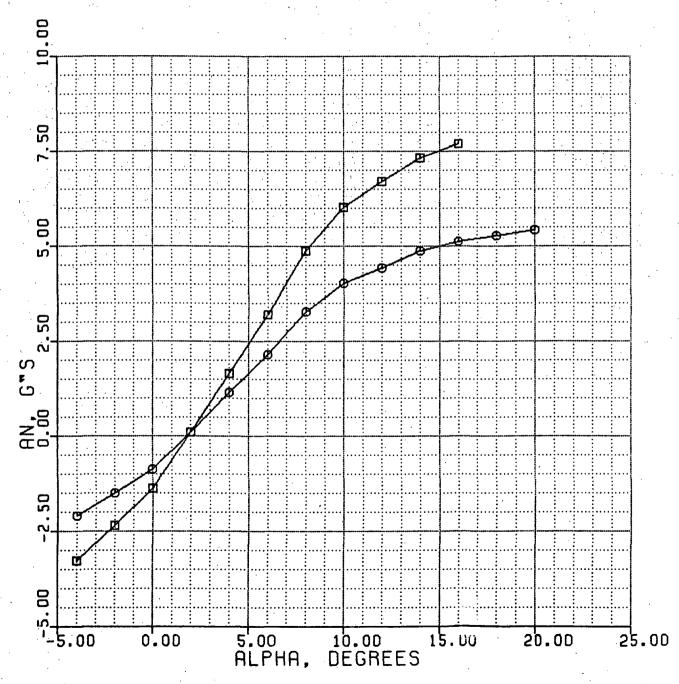
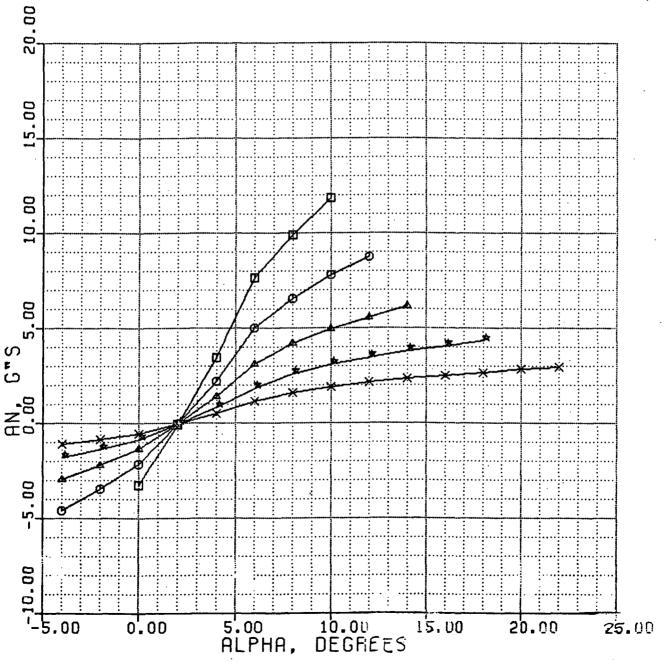


Figure 3(b)

```
VS ALPHA
                           OF POOR QUALITY
XCG = 451.0 WT = 15K ALPHA TRIM
    _____ALT = 10K
               ALP: 0 TØ 10
    _______ALT = 20K
               ALP: -4 TO 12
     ▲ ALT = 30K
               ALP: -4 TO 14
   ____★ ALT = 40K
               ALP: -4 TO 18
   _____ ALT = 50K
              ALP: -4 TO 22
```



AN VS ALPHA

三十一 月五十分的 整

7-14-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

☐ ☐ ALT = 20K ALP: 0 T0 10 ☐ ☐ ALT = 30K ALP: -2 T0 12 ▲ ALT = 40K ALP: -4 T0 14 ★ ★ ALT = 50K ALP: -4 T0 18

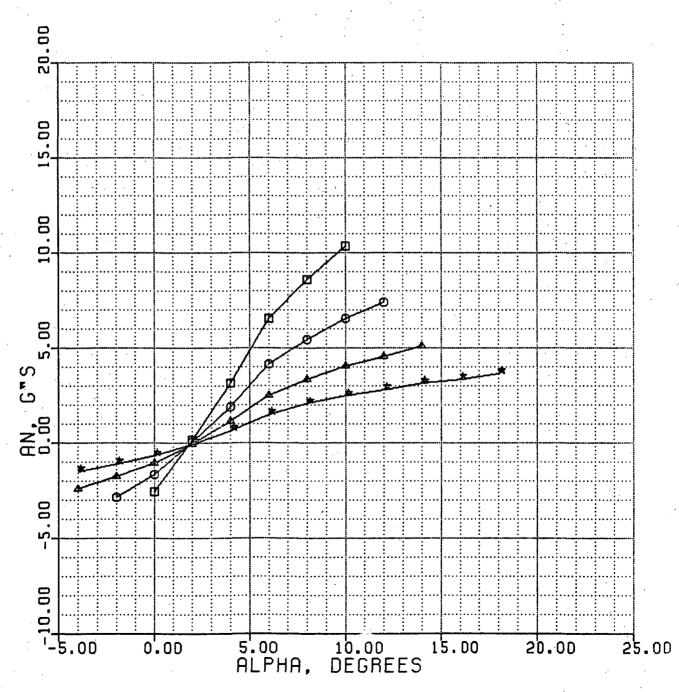


Figure 3(d)

AN VS ALPHA

7-14-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

☐ ☐ ☐ ☐ ALT = 20K ALP: -4 TØ 8 ☐ ☐ ☐ ALT = 30K ALP: -4 TØ 10 ▲ ALT = 40K ALP: -4 TØ 12 ★ ALT = 50K ALP: -4 TØ 14

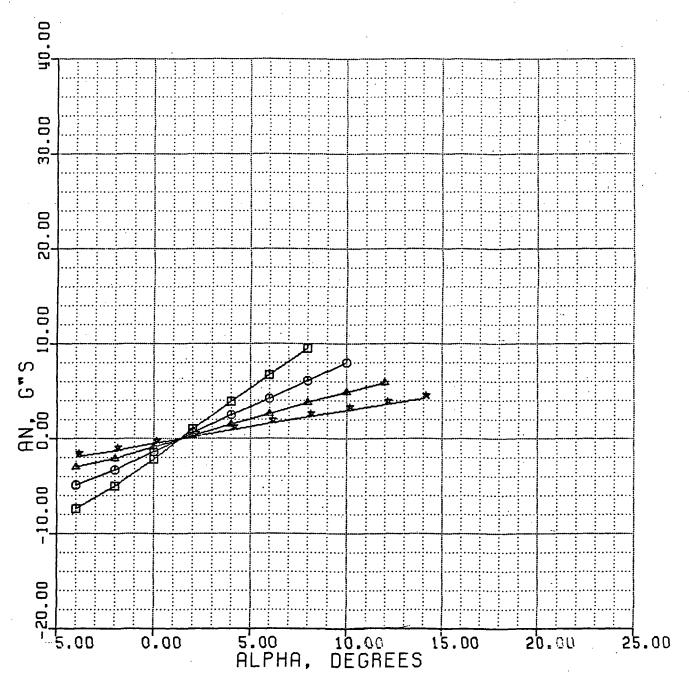


Figure 3(e)

AN VS ALPHA

7-14-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

O ALT = 30K ALP: -4 TO 8
O ALT = 40K ALP: -4 TO 10
A ALT = 50K ALP: -4 TO 12

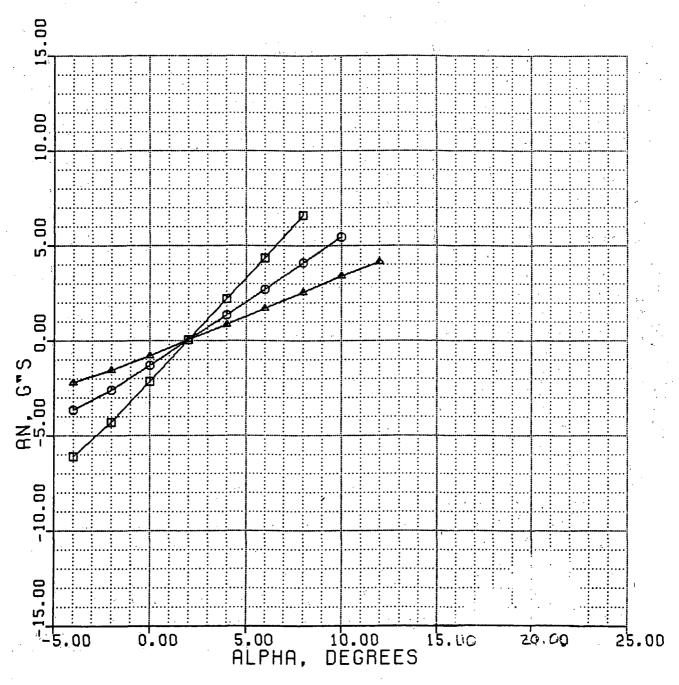


Figure 3(f)

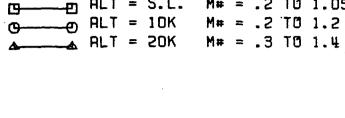
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ALPHA VS MACH # OF POOR QUALITY

7-5-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B RLT = S.L. M# = .2 TO 1.05



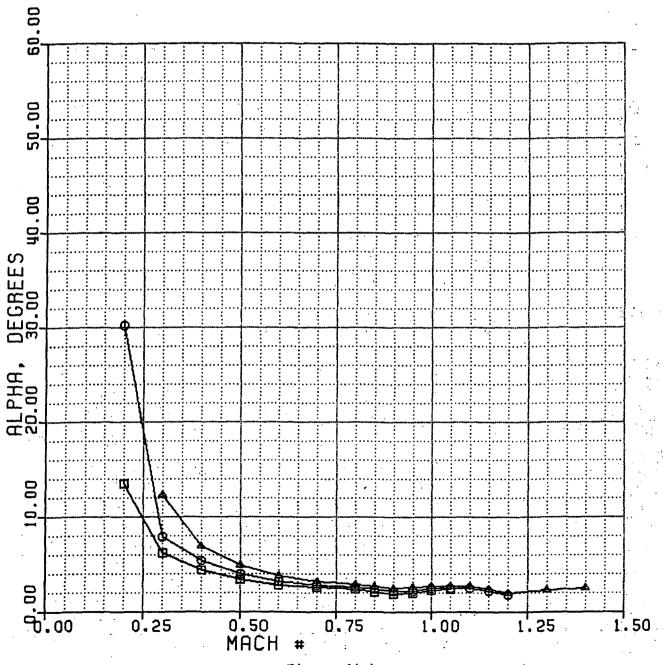


Figure 4(a)

ALPHA VS MACH #

7-7-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

 $M = .3 \text{ TO} \cdot 1.5$ -O ALT = 40K M# = .6 T0 1.5

ALT = 50K M# = .6 TO 1.5

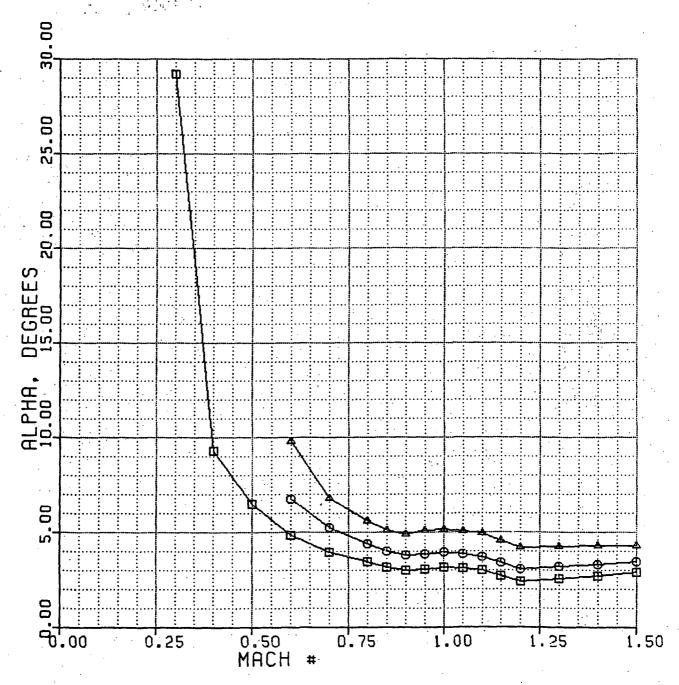


Figure 4(b)

STATIC MARGIN VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

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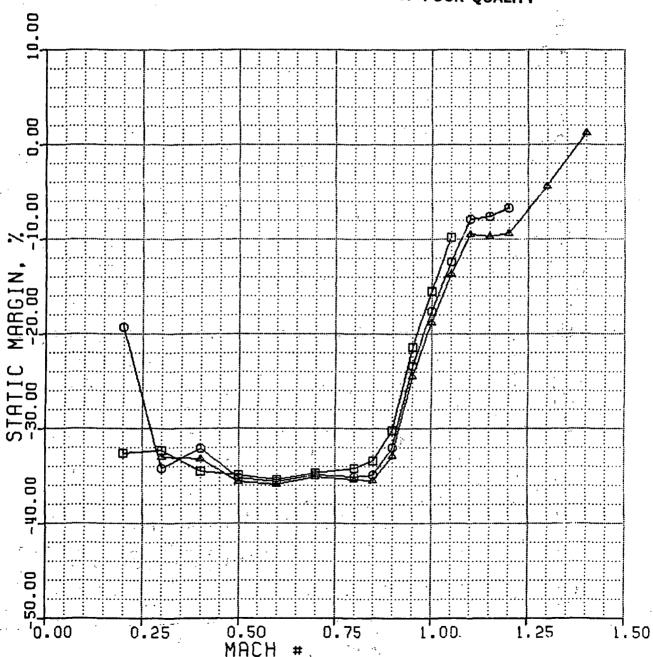
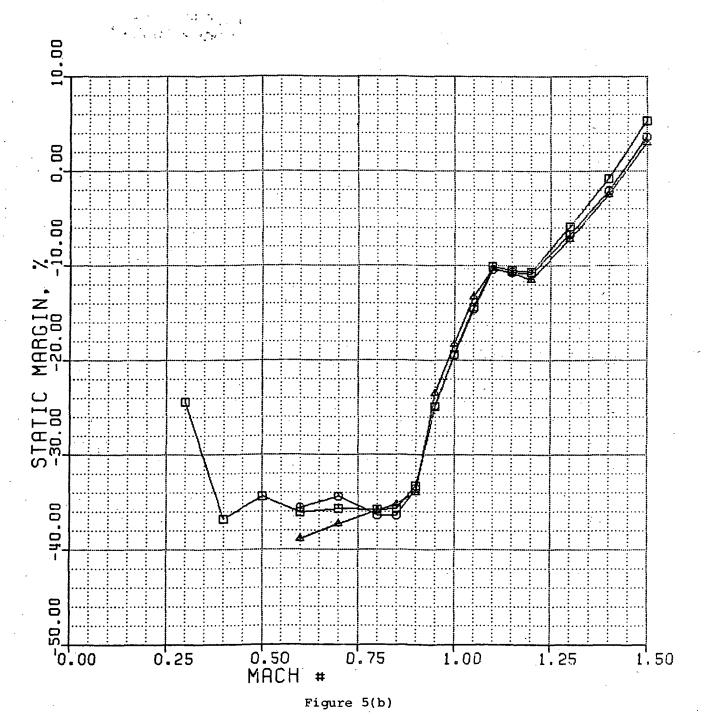


Figure 5(a)



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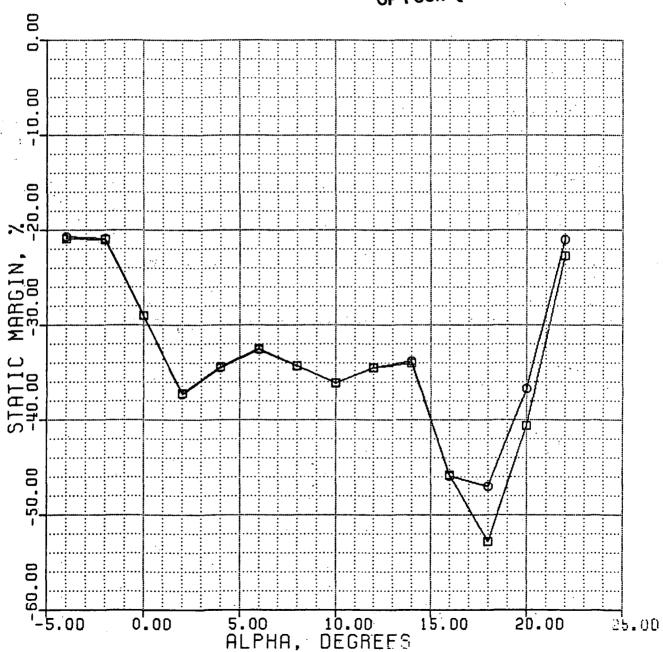


Figure 6(a)

STATIC MARGIN VS ALPHA

7-15-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

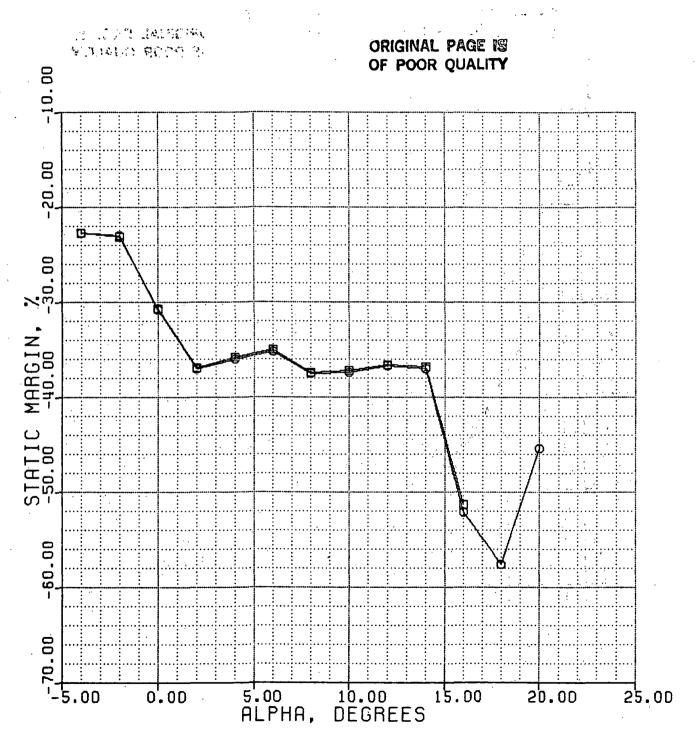


Figure 6(b)

STATIC MARGIN VS ALPHA 7-15-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM B ALT = 10K ALP: 0 TO 10 C O ALT = 20K ALP: -4 TO 12 ALT = 30K ALP: -4 TO 14 ALT = 40K ALP: -4 TO 18 X ALT = 50K ALP: -4 TO 22 ORIGINAL PAGE IS

OF POOR QUALITY

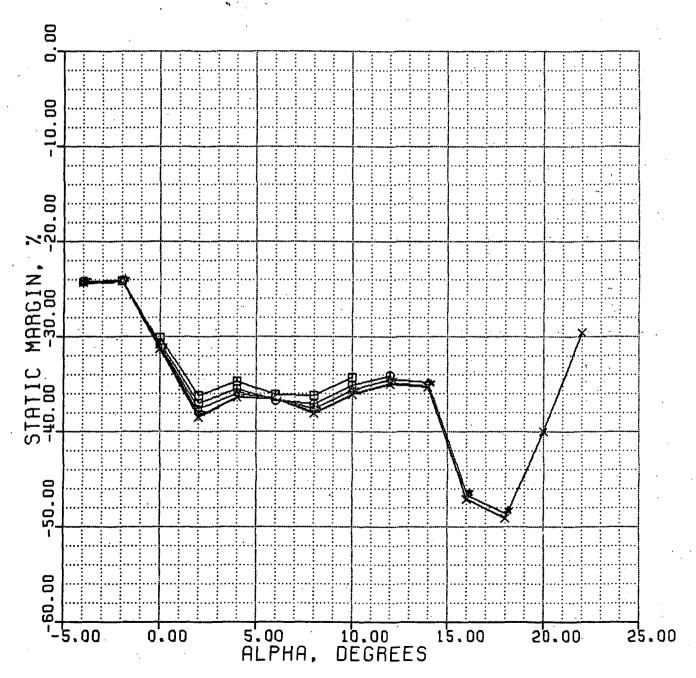
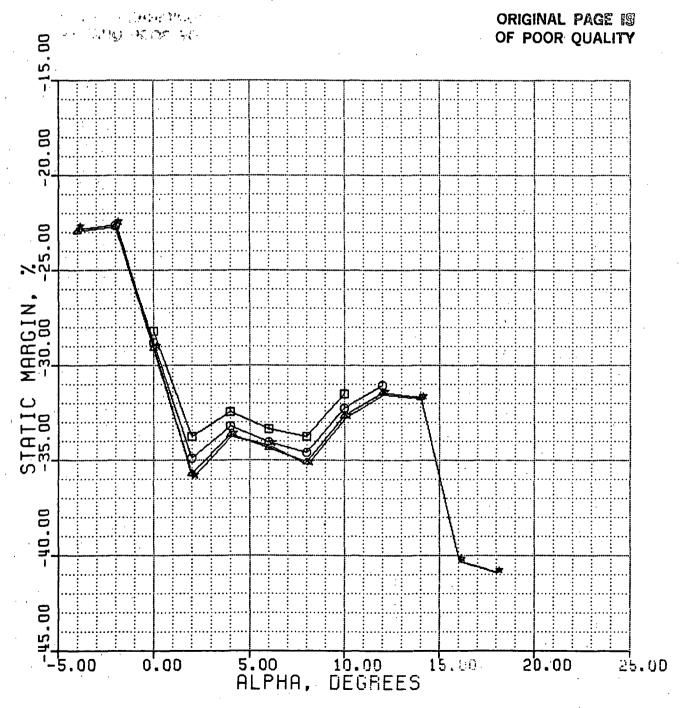


Figure 6(c)

STATIC MARGIN VS ALPHA 7-15-83 X-29A M# = 0.9 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 20K ALP: 0 T0 10 9 ALT = 30K ALP: -2 T0 12 A ALT = 40K ALP: -4 T0 14 A ALT = 50K ALP: -4 T0 18



STATIC MARGIN VS ALPHA

7-15-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

O ALT = 20K ALP: -4 TO 8
O O ALT = 30K ALP: -4 TO 10
A ALT = 40K ALP: -4 TO 12

* ALT = 50K ALP: -4 TO 14

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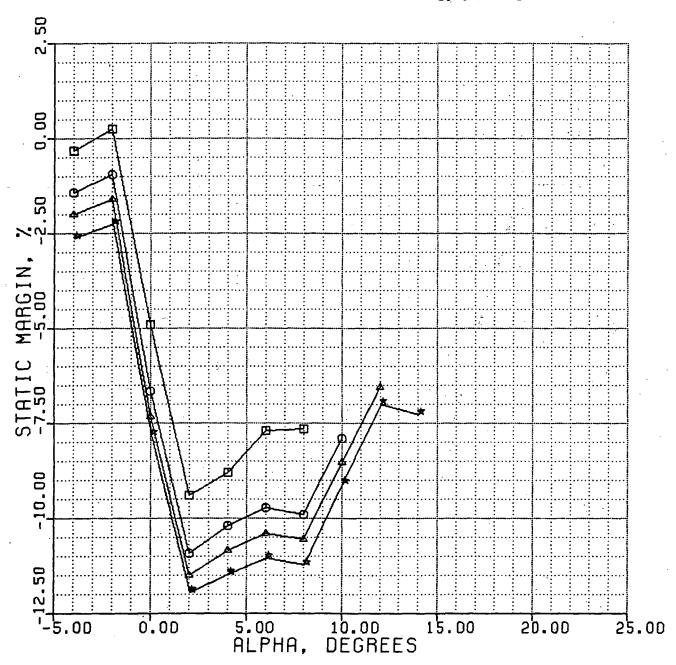


Figure 6(e)

STATIC MARGIN VS ALPHA

7-15-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8 9 ALT = 40K ALP: -4 TO 10 A ALT = 50K ALP: -4 TO 12

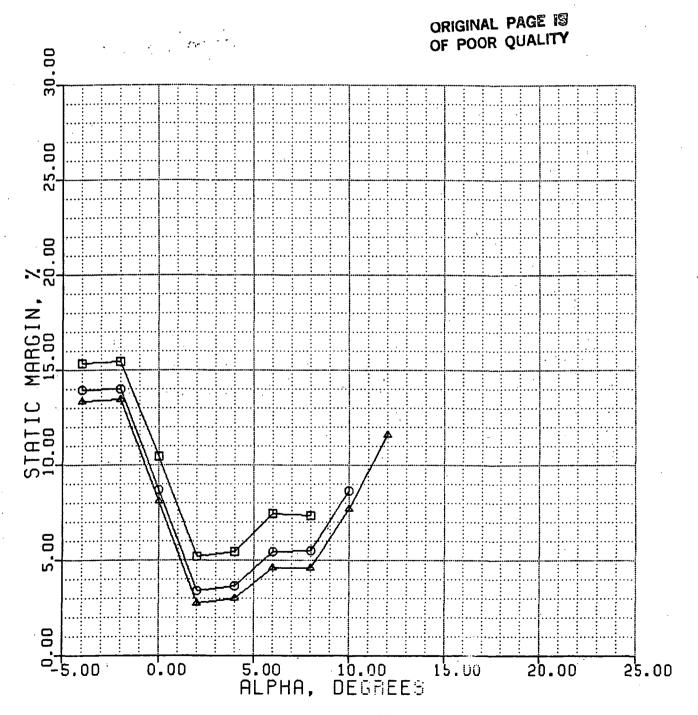
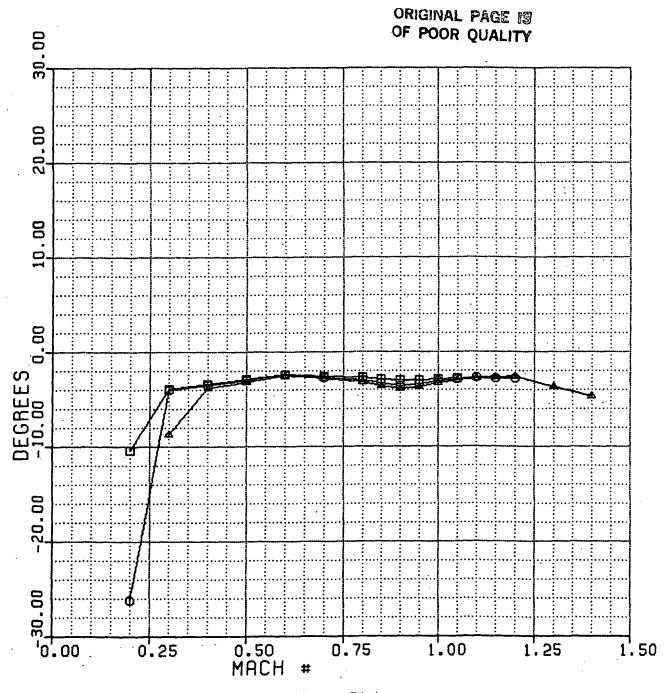


Figure 6(f)

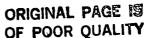


DELTA CANARD VS MACH # 7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

```
P ALT = 30K M# = .3 TO 1.5

P ALT = 40K M# = .6 TO 1.5

ALT = 50K M# = .6 TO 1.5
```



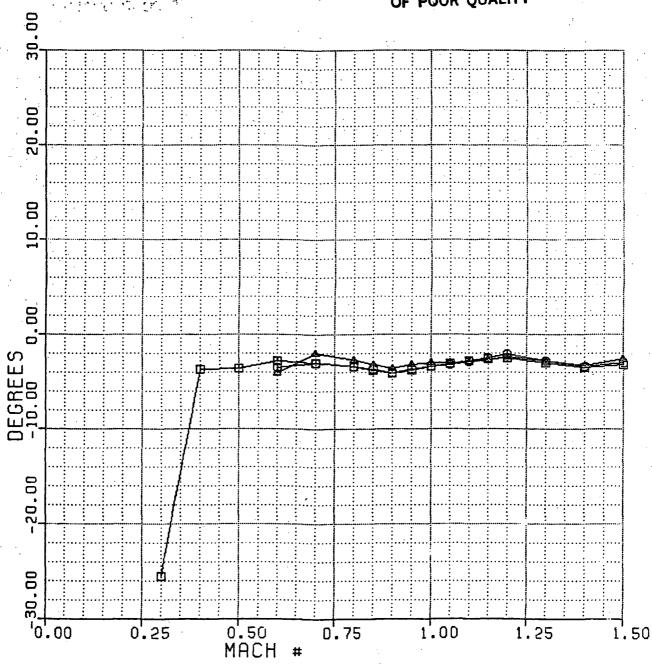
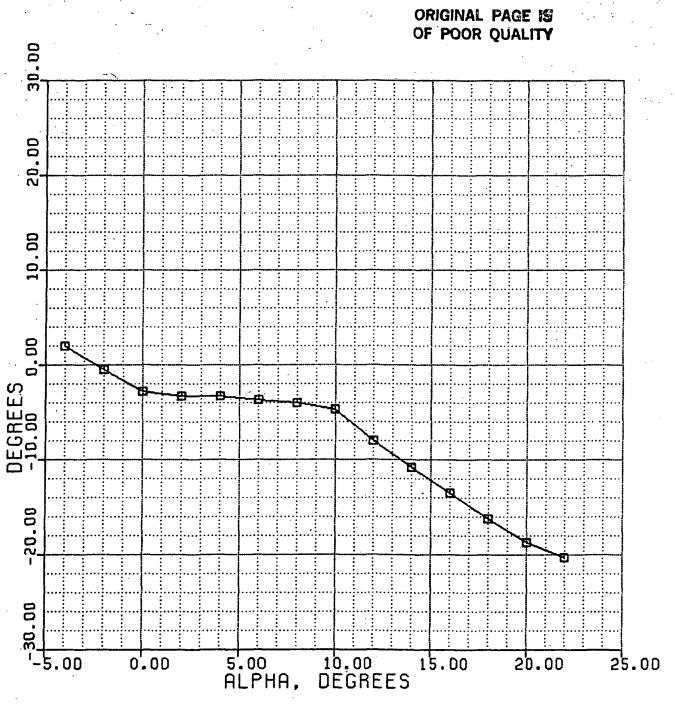


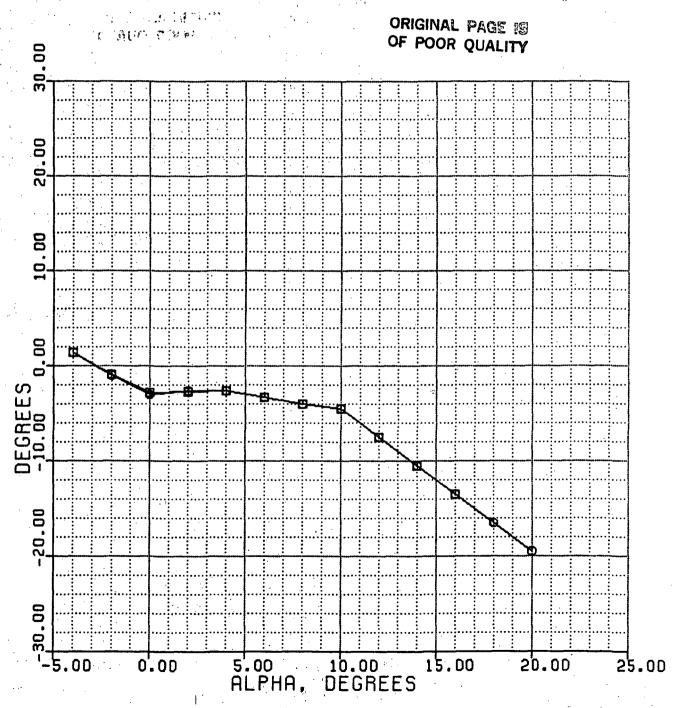
Figure 7(b)



DELTA CANARD VS ALPHA

6-16-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20



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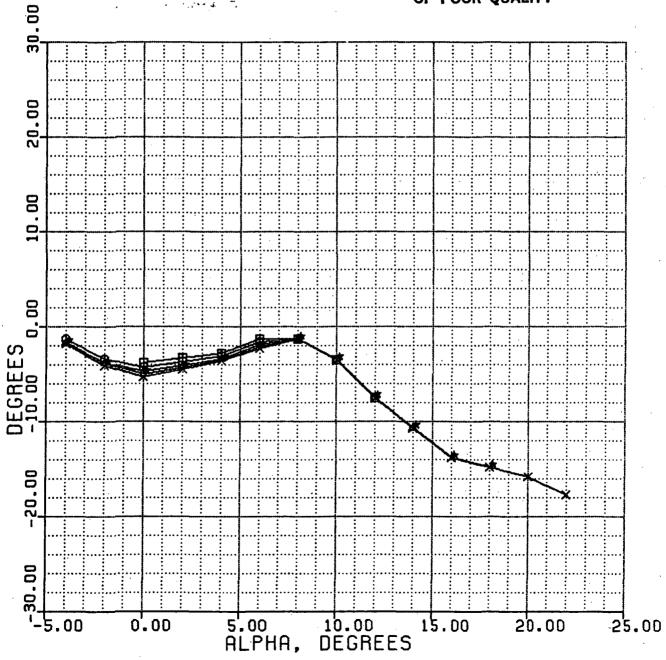


Figure 8(c)

★ ALT = 50K · ALP: -4 TO 18

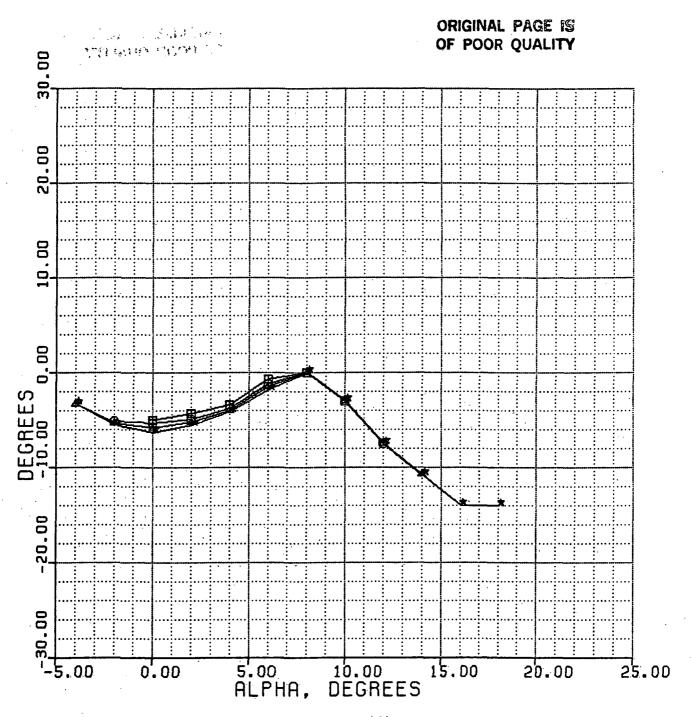


Figure 8(d)

DELTA CANARD VS ALPHA

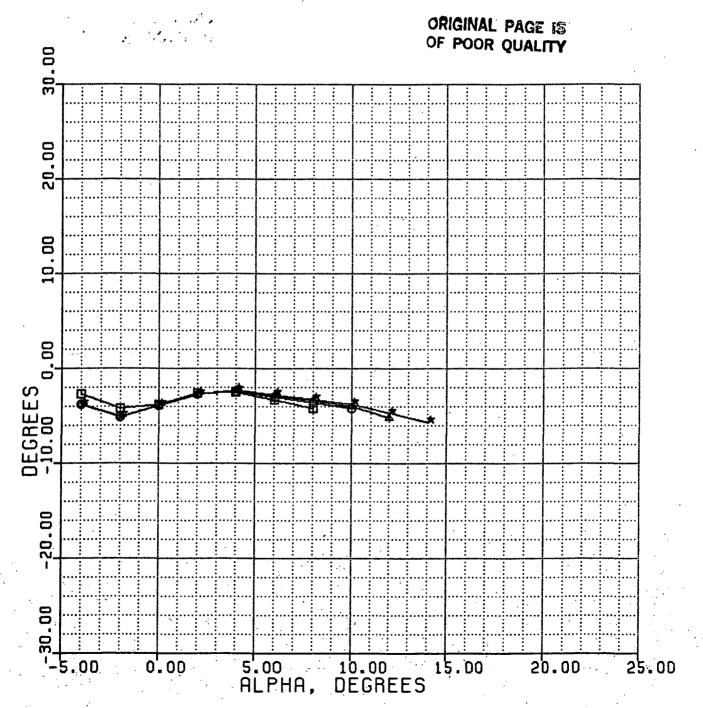
7-1-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14



DELTA CANARD VS ALPHA

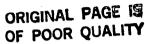
7-1-83 X-29A M# = 1.5 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

9 PLT = 30K PLP: -4 TO 8

9 PLT = 40K PLP: -4 TO 10

A PLT = 50K PLP: -4 TO 12



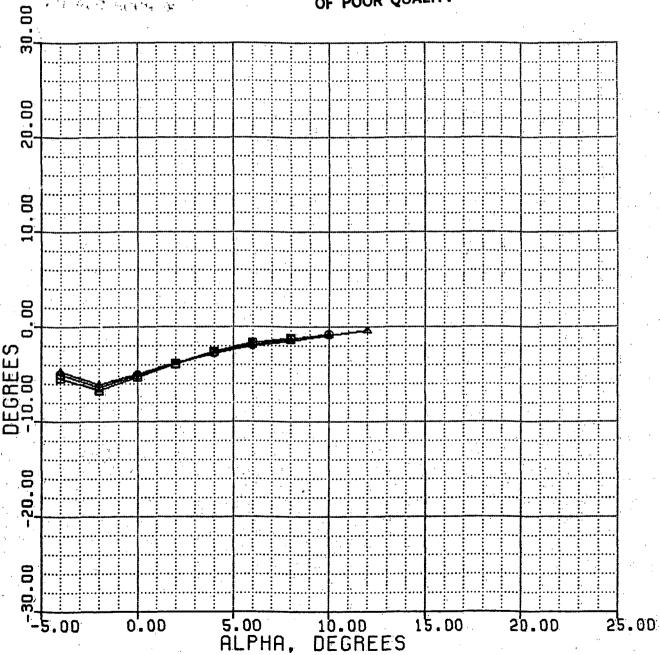


Figure 8(f)

```
DELTA FLAP VS MACH #

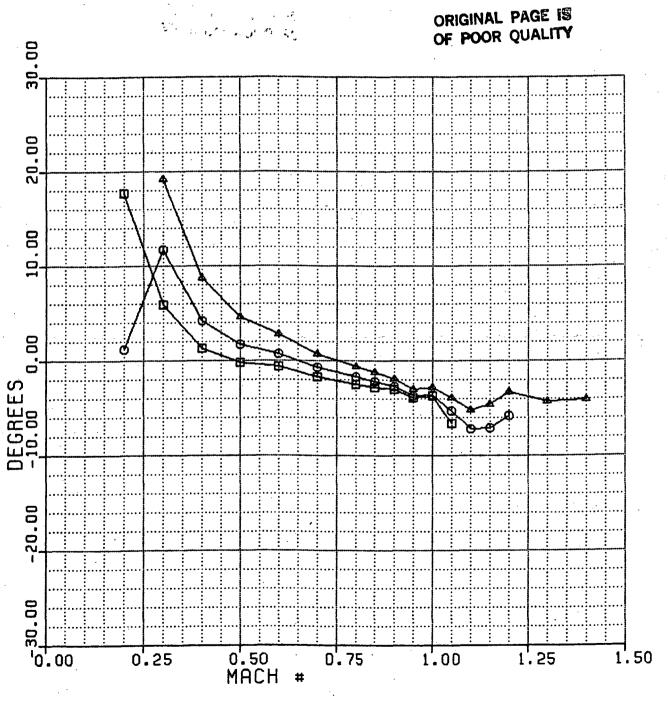
7-5-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B RLT = 5.L. M# = .2 TO 1.05

B RLT = 10K M# = .2 TO 1.2

ALT = 20K M# = .3 TO 1.4
```



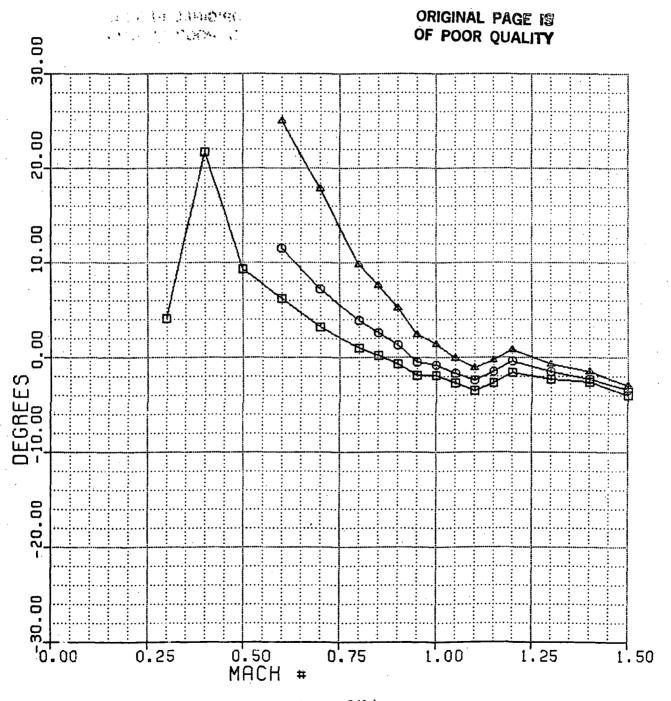


Figure 9(b)

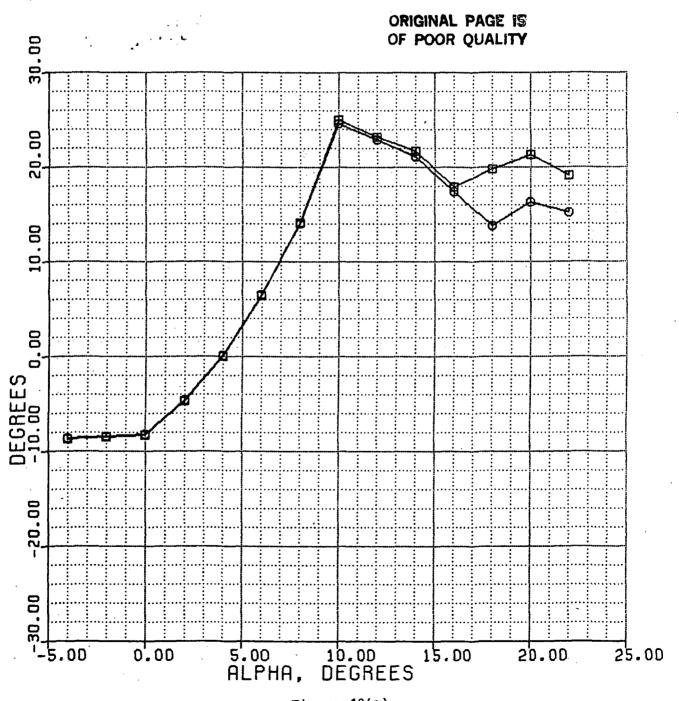
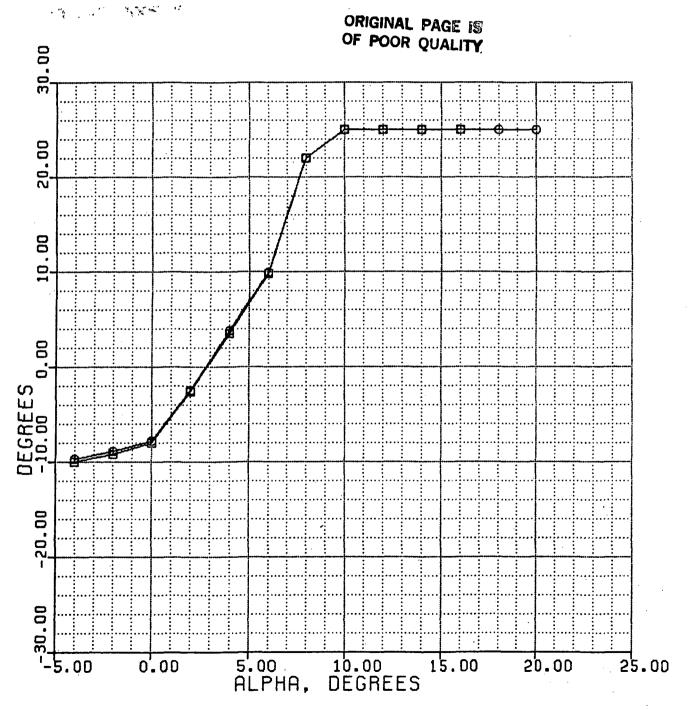


Figure 10(a)

DELTA FLAP VS ALPHA
6-16-83 X-29A M# = 0.6 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

B RLT = 10K ALP: -4 TØ 16
C RLT = 20K ALP: -4 TØ 20



DELTA FLAP VS ALPHA

6-17-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: 0 T0 10

P ALT = 20K ALP: -4 T0 12

A ALP = 30K ALP: -4 T0 14

A ALT = 40K ALP: -4 T0 18

A ALT = 50K ALP: -4 T0 22

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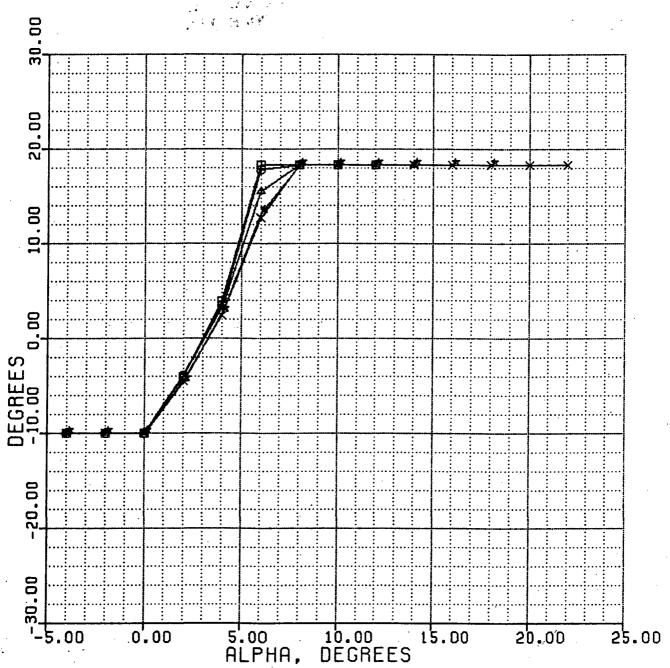


Figure 10(c)

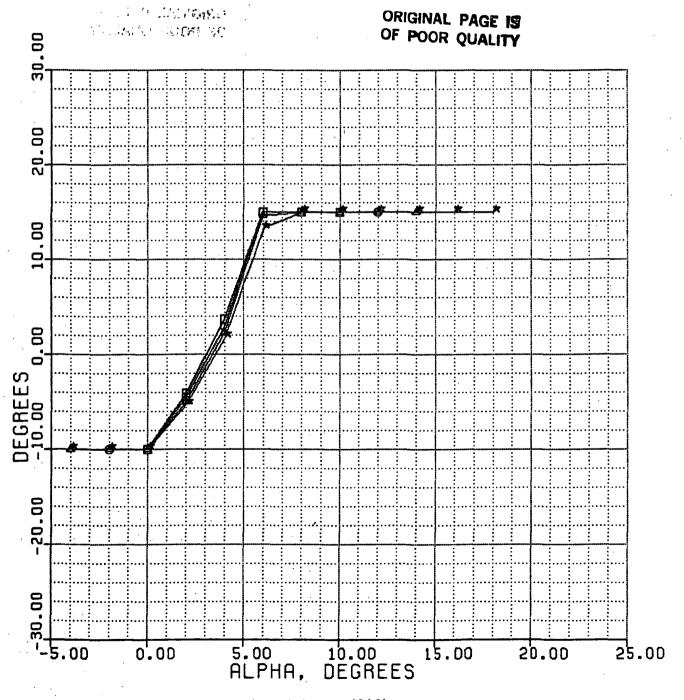
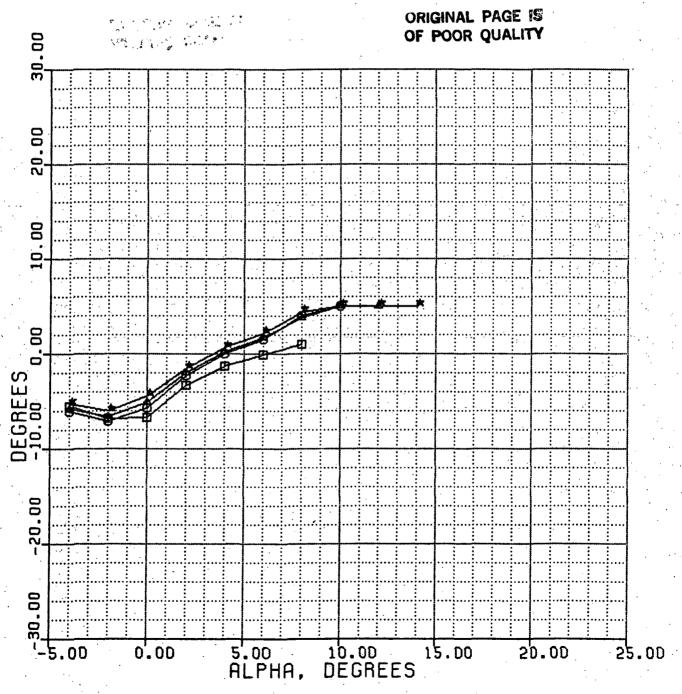


Figure 10(d)



DELTA FLAP VS ALPHA 7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8

9 ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12

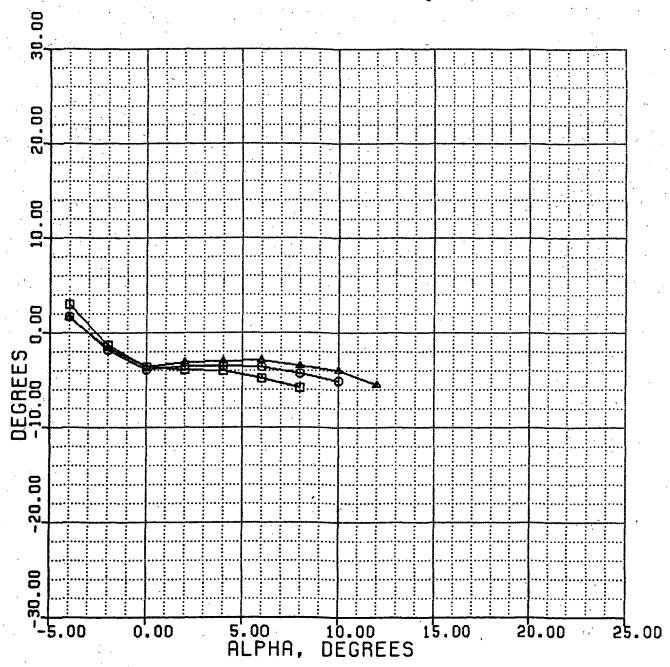
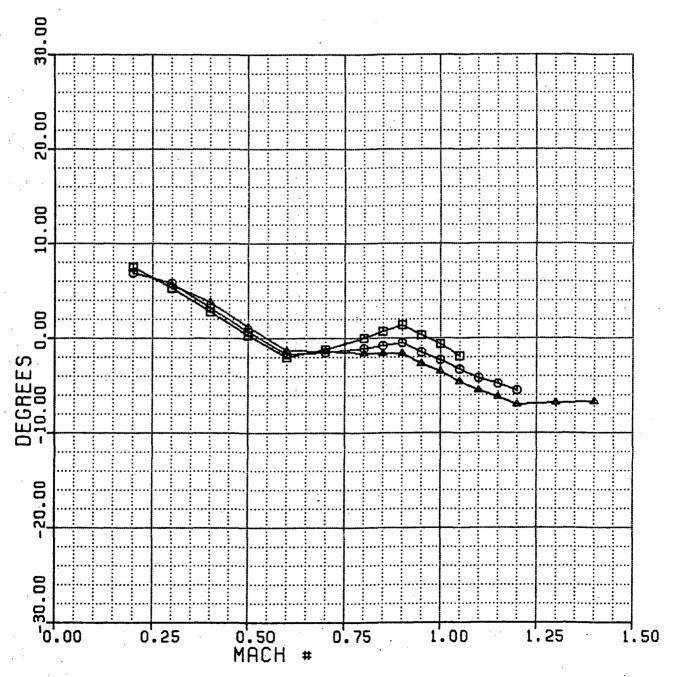


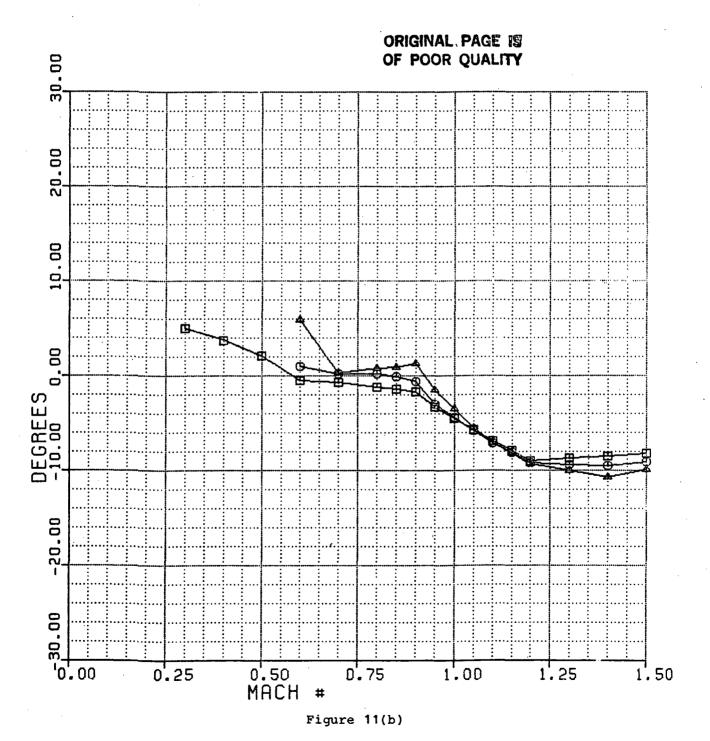
Figure 10(f)

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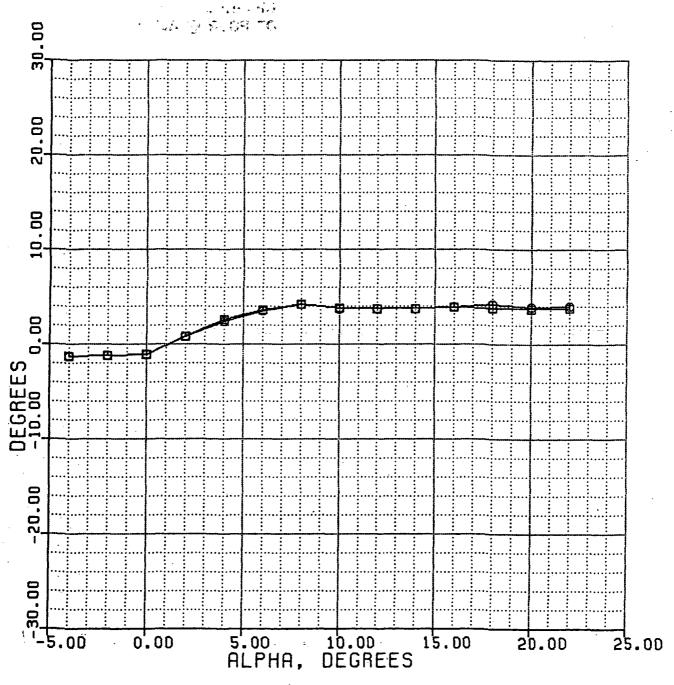
DELTA STRAKE VS MACH # 7-5-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

PALT = S.L. M# = .2 TO 1.05 PALT = 10K M# = .2 TO 1.2 A RLT = 20K M# = .3 TO 1.4





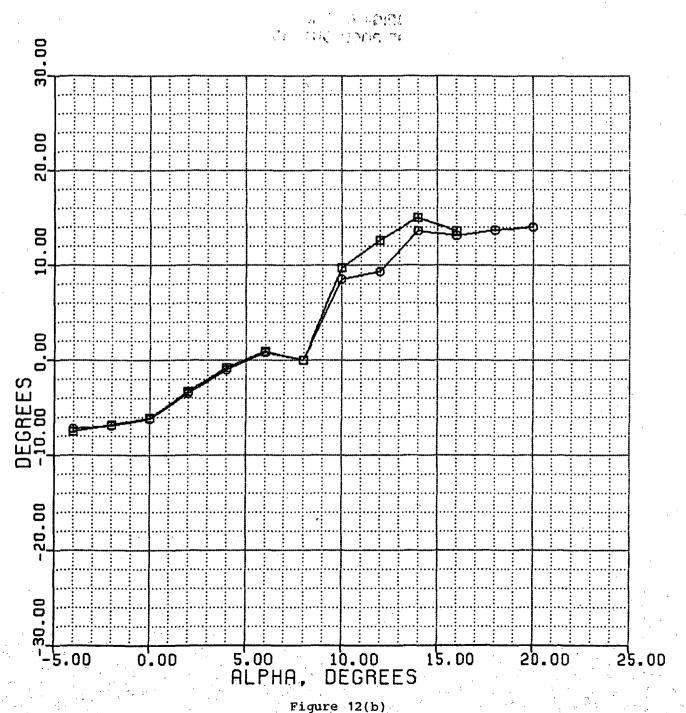
ORIGINAL PAGE IS OF POOR QUALITY



ORIGINAL PAGE IS OF POOR QUALITY

DELTA STRAKE VS ALPHA 6-16-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

O ALT = 10K ALP: -4 TO 16 O ALT = 20K ALP: -4 TO 20



DELTA STRAKE VS ALPHA

6-17-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

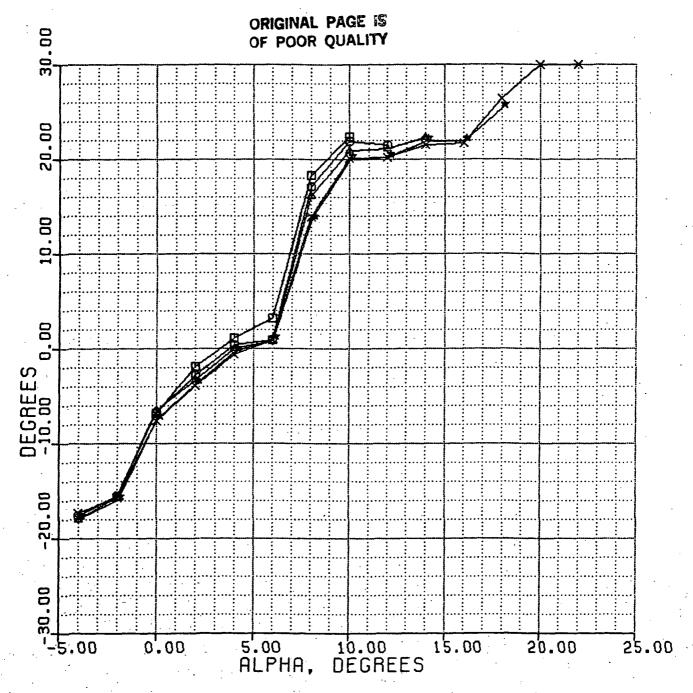
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P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALP = 30K ALP: -4 TO 14

A ALT = 40K ALP: -4 TO 18

X ALT = 50K ALP: -4 TO 22
```



DELTA STRAKE VS ALPHA

7-1-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

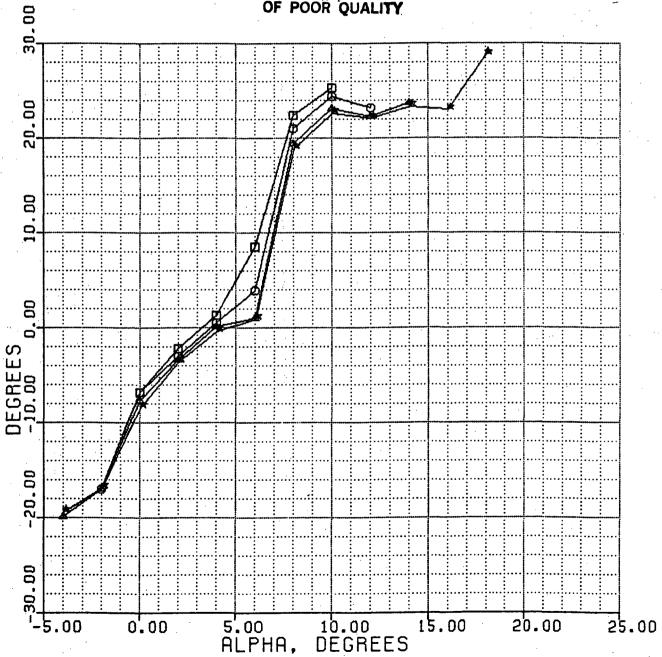


Figure 12(d)

DELTA STRAKE VS

7-1-83 X-29A M# = 1.2NORMAL MODE XCG = 451.0WT = 15K ALPHA TRIM

ALT = 20KALT = 30K-4 TO 10 ALT = 40K ★ ALT = 50K

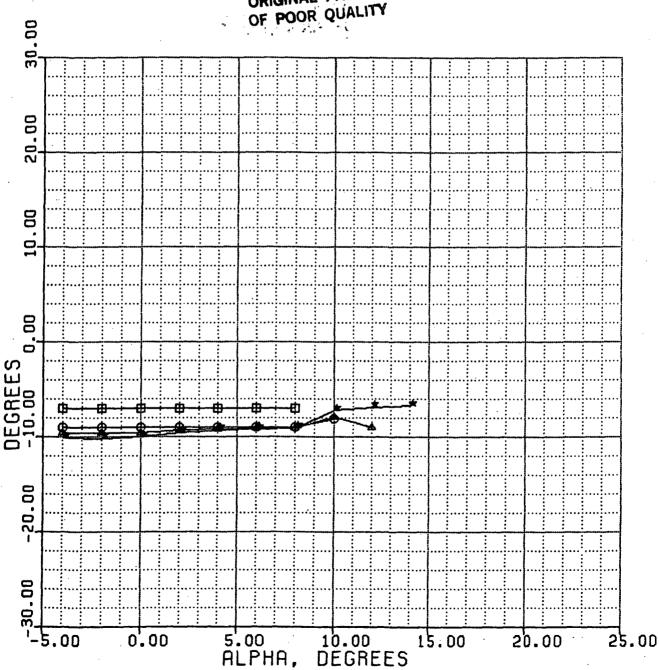


Figure 12(e)

DELTA STRAKE VS ALPHA

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 30K ALP: -4 TO 8

P ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12

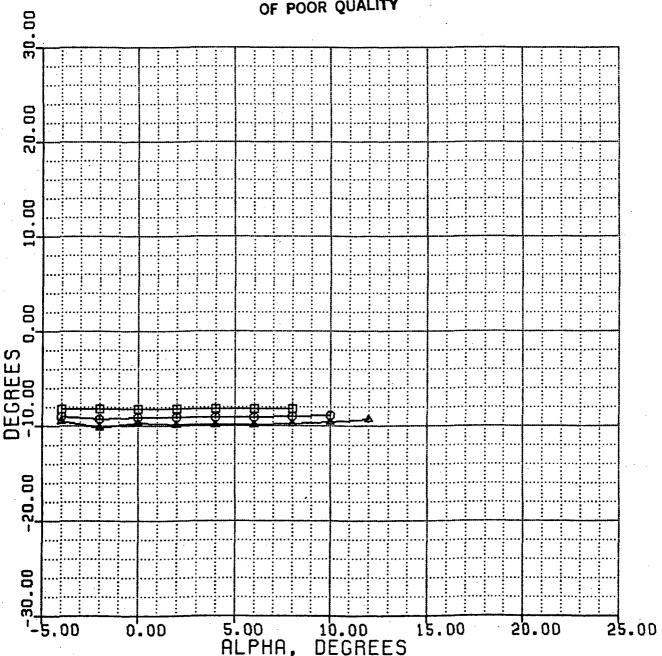


Figure 12(f)

CL-LIFT VS MACH # 7-5-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K P O RLT = 5.L. M# = .2 TO 1.00 O RLT = 10K M# = .2 TO 1.2 ALT = 20K M# = .3 TO 1.4

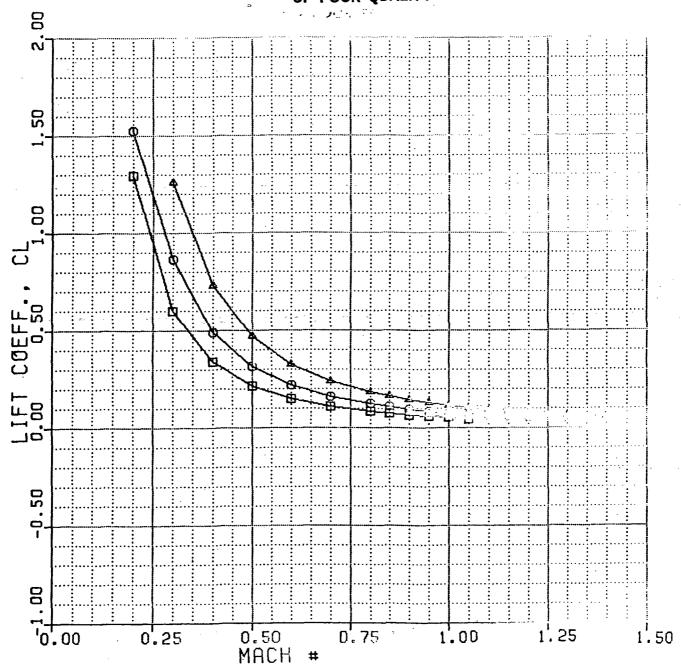
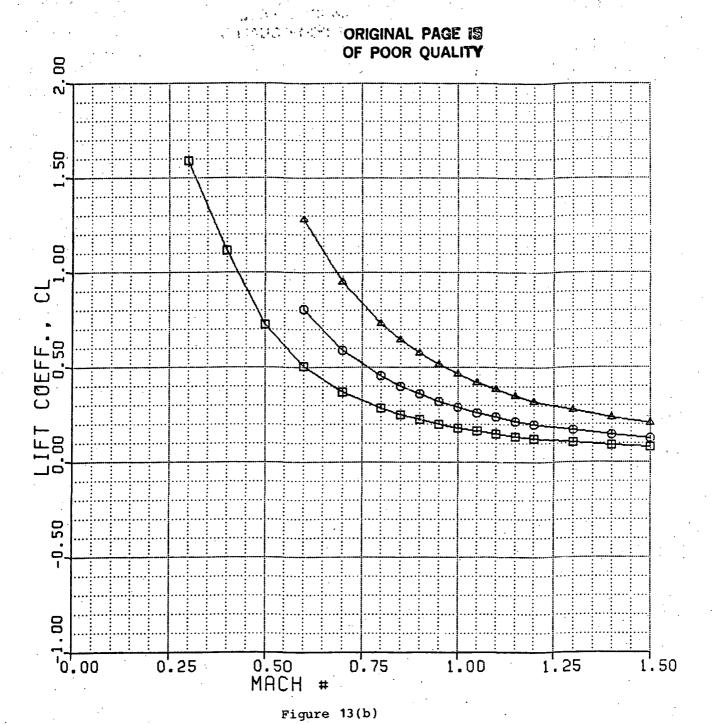


Figure 13(a)



CL-LIFT VS ALPHA

6-15-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = S.L. ALP: -4 TØ 22 9 ALT = 10K ALP: -4 TØ 22

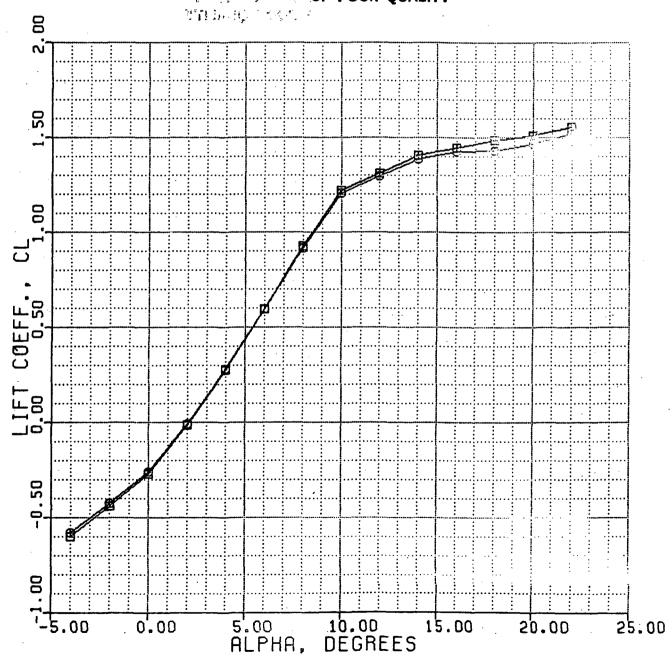


Figure 14(a)



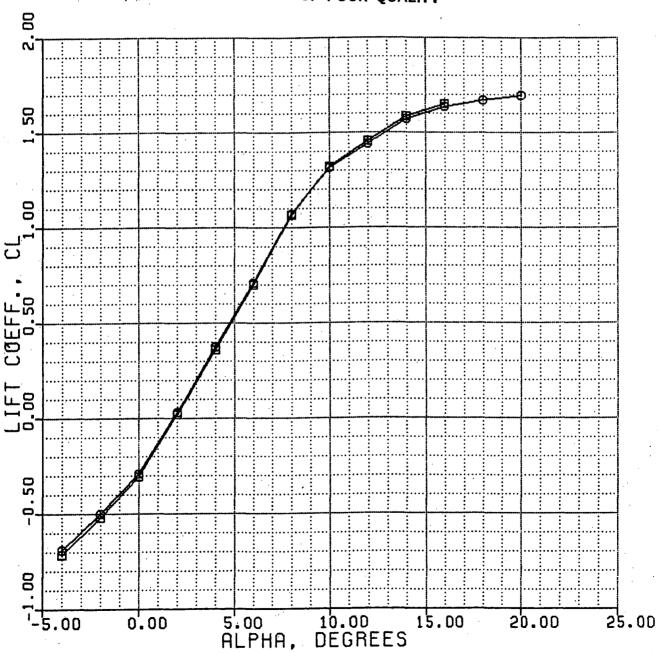
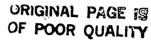


Figure 14(b)



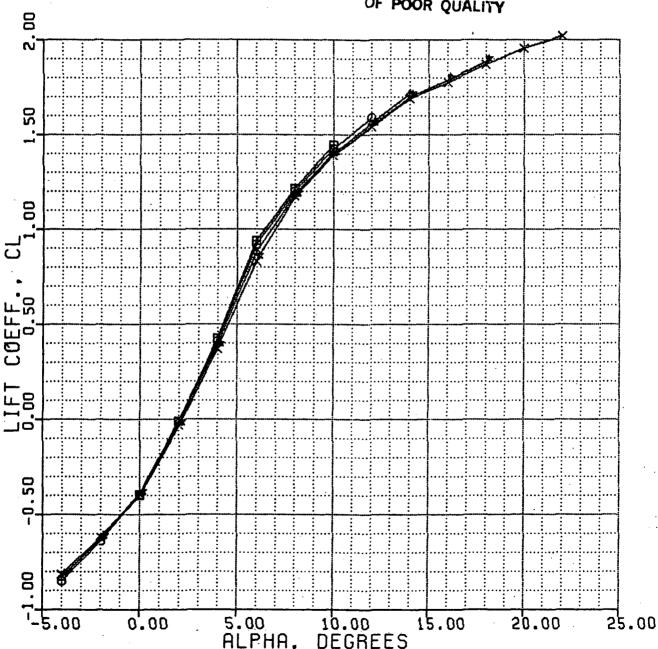


Figure 14(c)

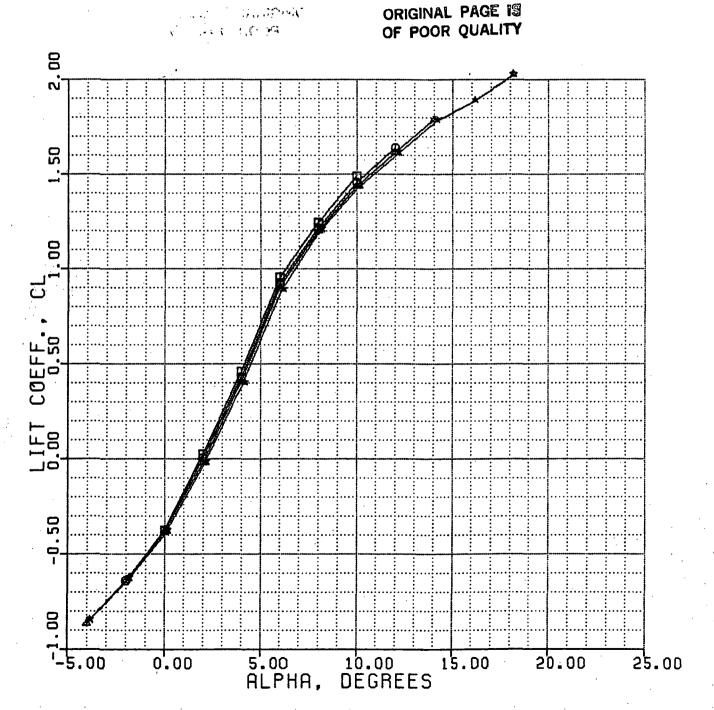


Figure 14(d)

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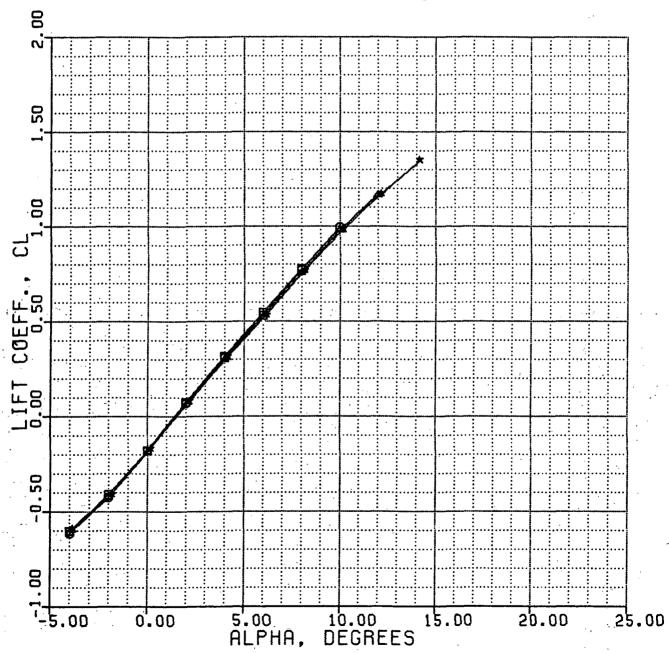


Figure 14(e)

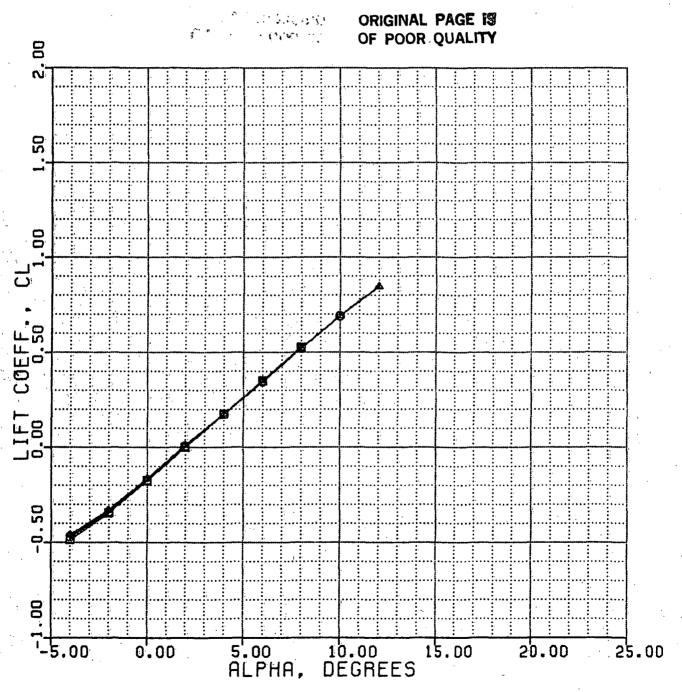


Figure 14(f)

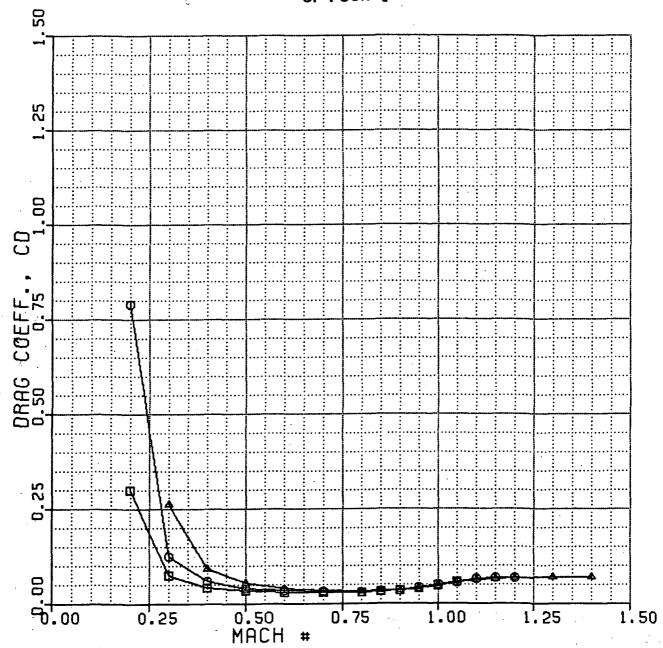


Figure 15(a)

```
CD VS MACH #

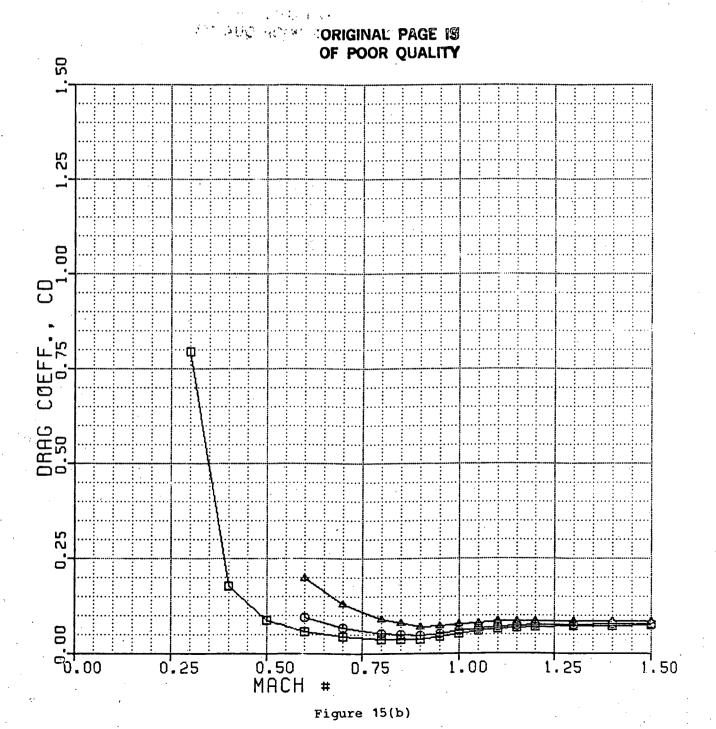
7-7-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B ALT = 30K M# = .3 TO 1.5

ALT = 40K M# = .6 TO 1.5

ALT = 50K M# = .6 TO 1.5
```



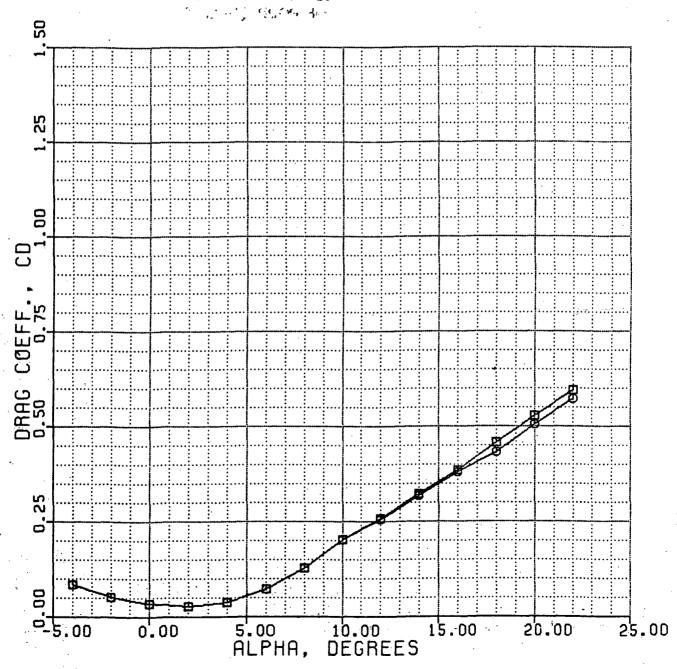


Figure 16(a)

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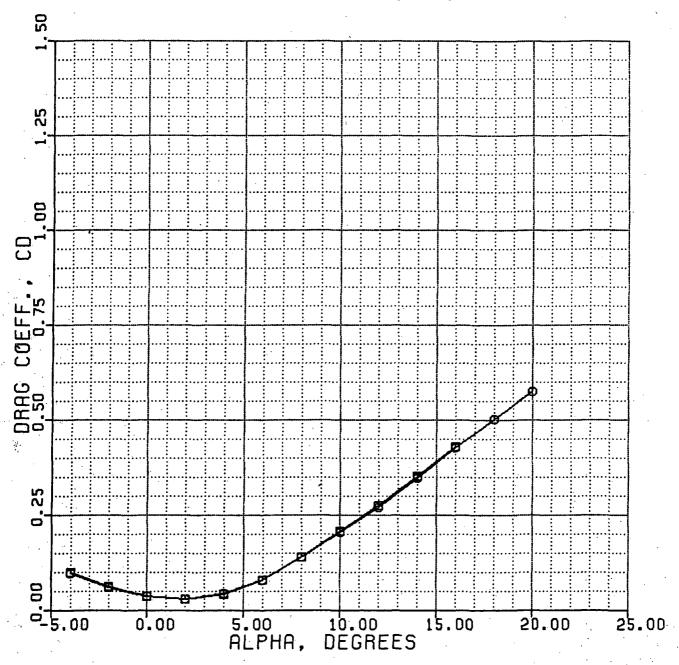


Figure 16(b)

CD VS ALPHA

6-17-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 T0 10

P ALT = 20K ALP: -4 T0 12

A ALP = 30K ALP: -4 T0 14

A ALT = 40K ALP: -4 T0 18

A ALT = 50K ALP: -4 T0 22
```

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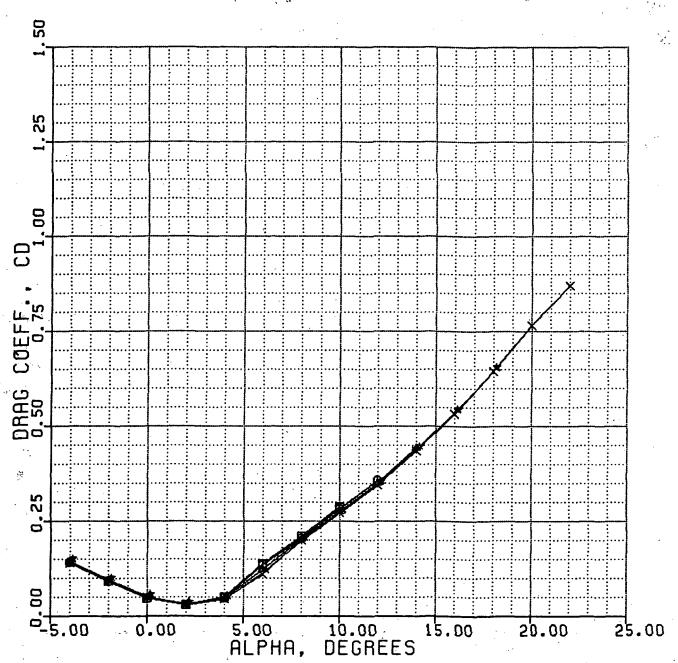


Figure 16(c)

ORIGINAL PAGE IS OF POOR QUALITY

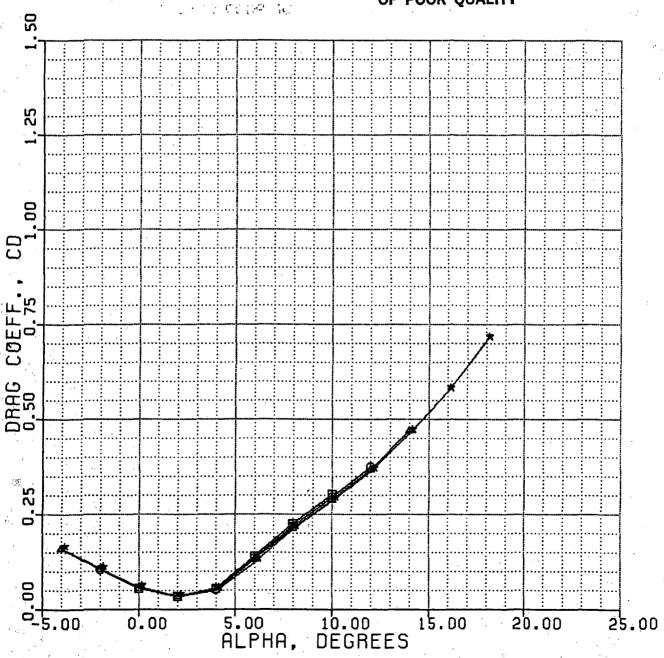


Figure 16(d)

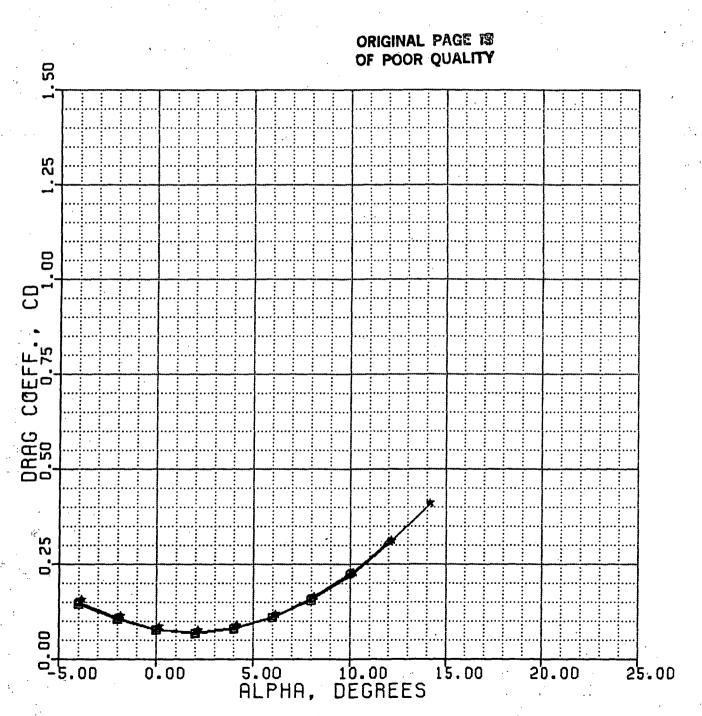


Figure 16(e)

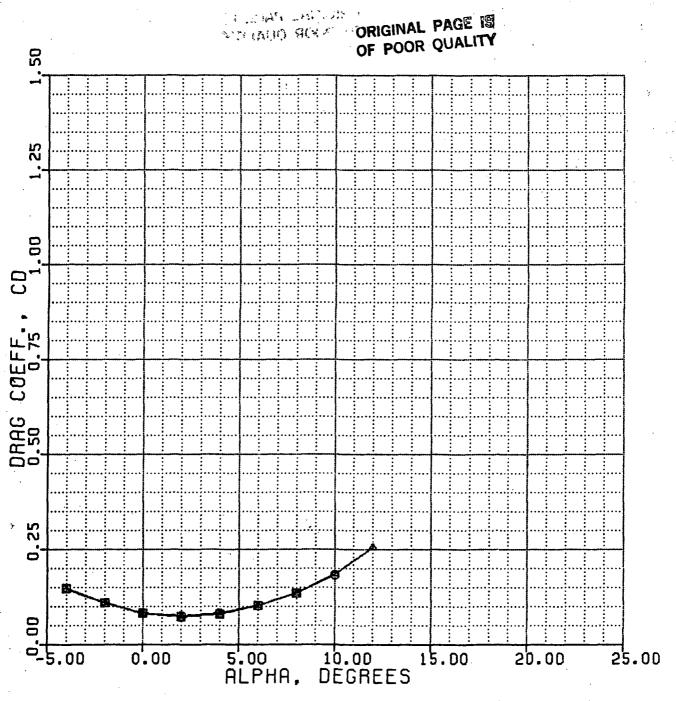


Figure 16(f)

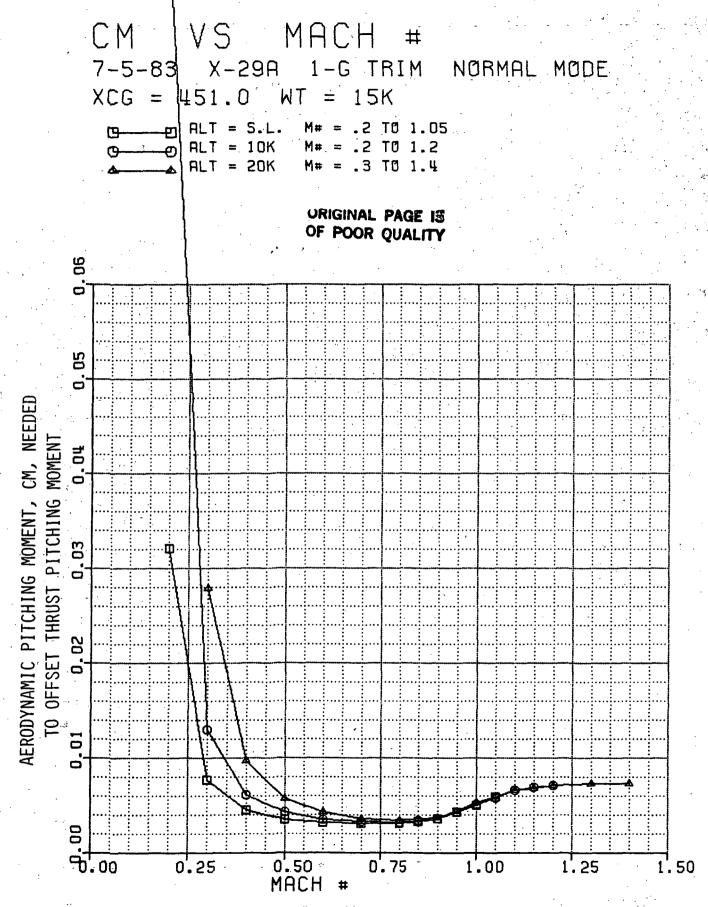
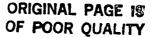


Figure 17(a)

AERODYNAMIC PITCHING MOMENT, CM, NEEDED TO OFFSET THRUST PITCHING MOMENT

Figure 17(b)



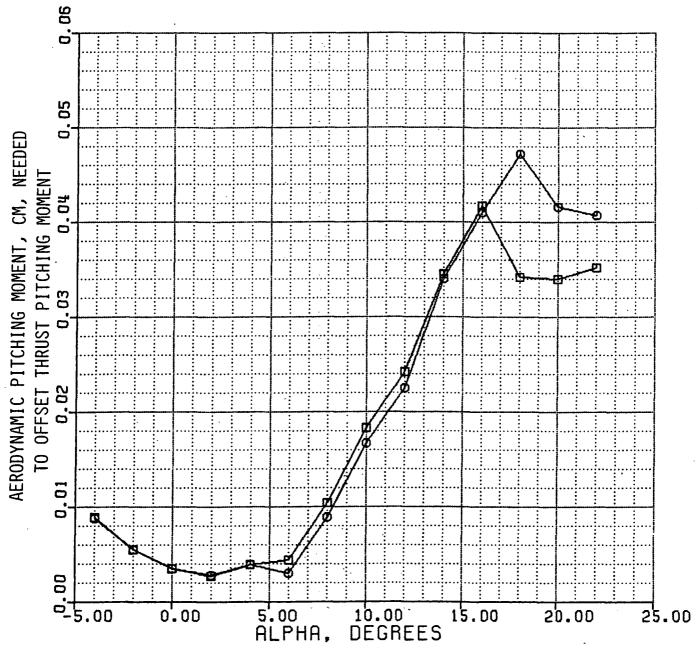
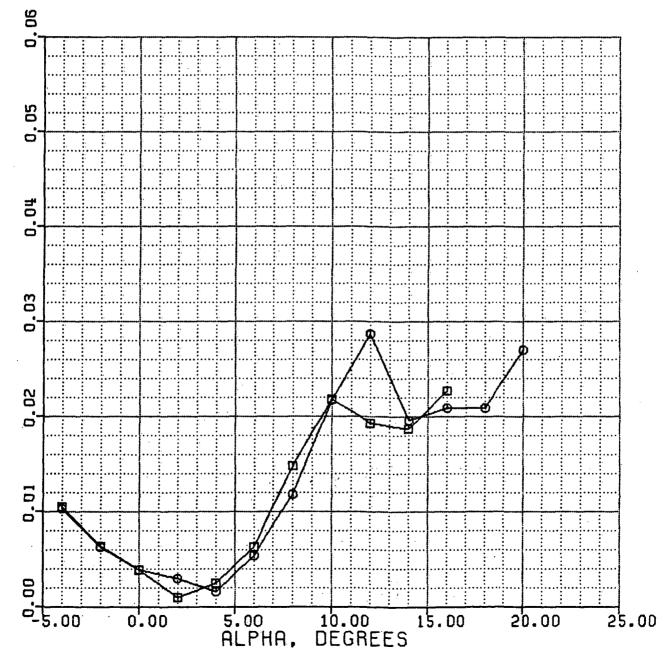


Figure 18(a)

AERODYNAMIC PITCHING MOMENT, CM, NEEDED TO OFFSET THRUST PITCHING MOMENT CM VS ALPHA
6-16-83 X-29A M# = 0.6 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 10K ALP: -4 TO 16
C ALT = 20K ALP: -4 TO 20

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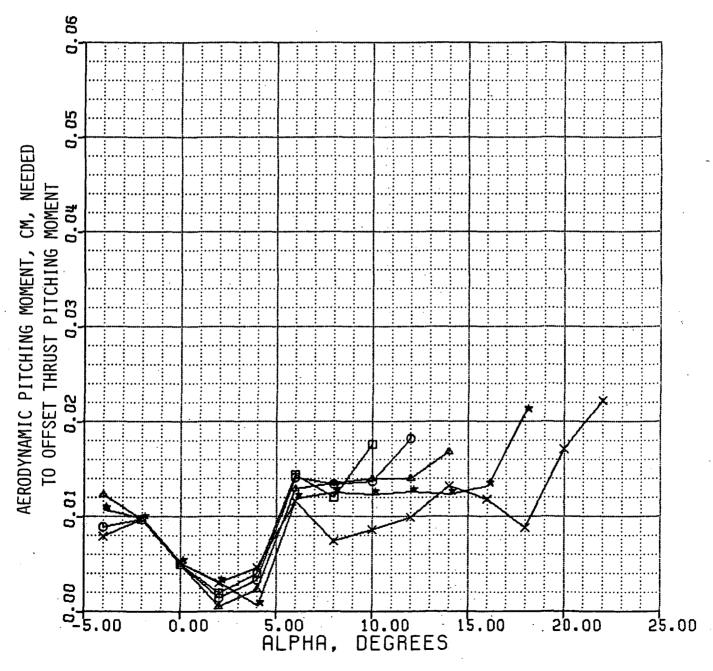
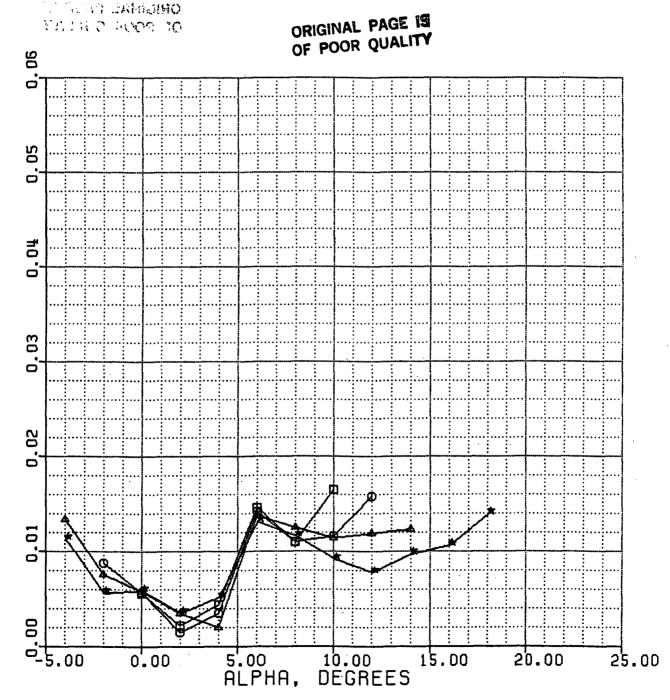


Figure 18(c)

VS CM X-29A 7-1-83 NORMAL MODE = 451.0 15K ALPHA TRIM WT 0 30K -2 TO = 40K -4 TO ALT = 50KALP: -4 TO 18



CM VS ALPHA

7-1-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

PALT = 20K ALP: -4 T0 8

PALT = 30K ALP: -4 T0 10

A ALT = 40K ALP: -4 T0 12

A ALT = 50K ALP: -4 T0 14

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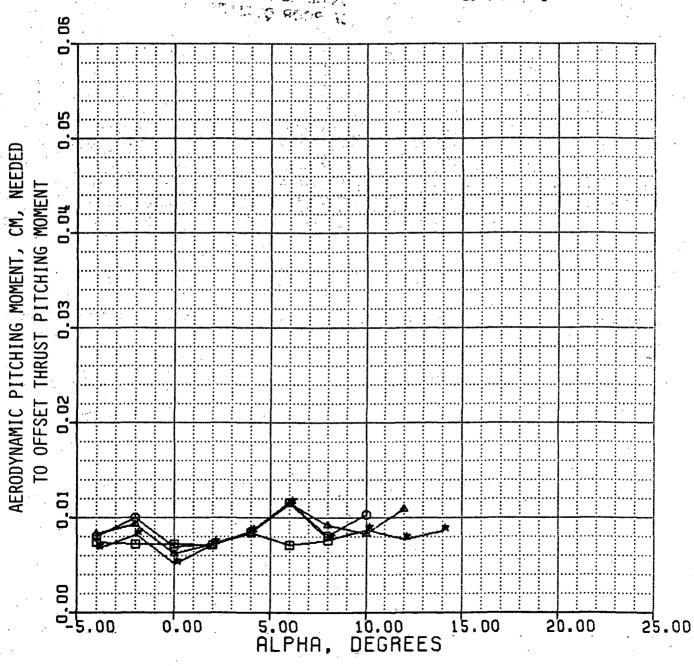


Figure 18(e)

CM VS ALPHA

7-1-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8 9 ALT = 40K ALP: -4 TO 10 A ALT = 50K ALP: -4 TO 12

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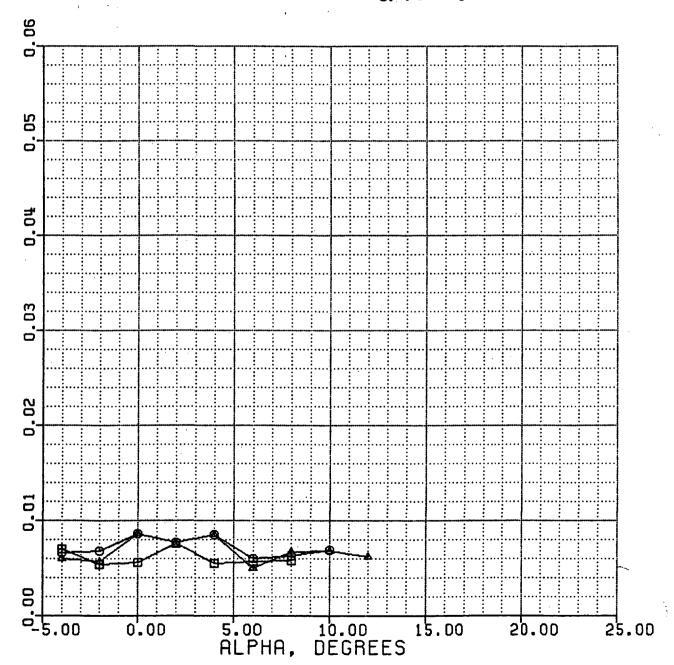


Figure 18(f)

CA VS MACH #

7-5-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

P ALT = S.L. M# = .2 TO 1.05

P ALT = 10K M# = .2 TO 1.2

A ALT = 20K M# = .3 TO 1.4

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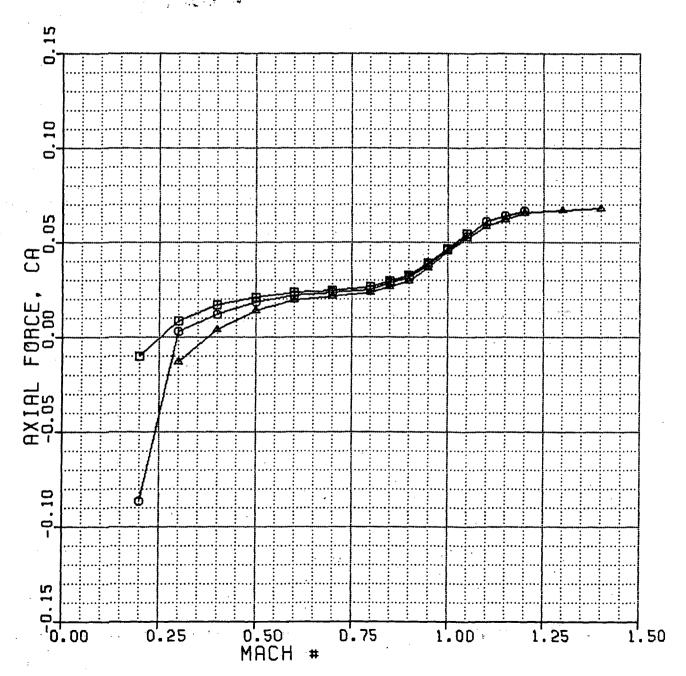


Figure 19(a)



ORIGINAL PAGE 19 OF POOR QUALITY

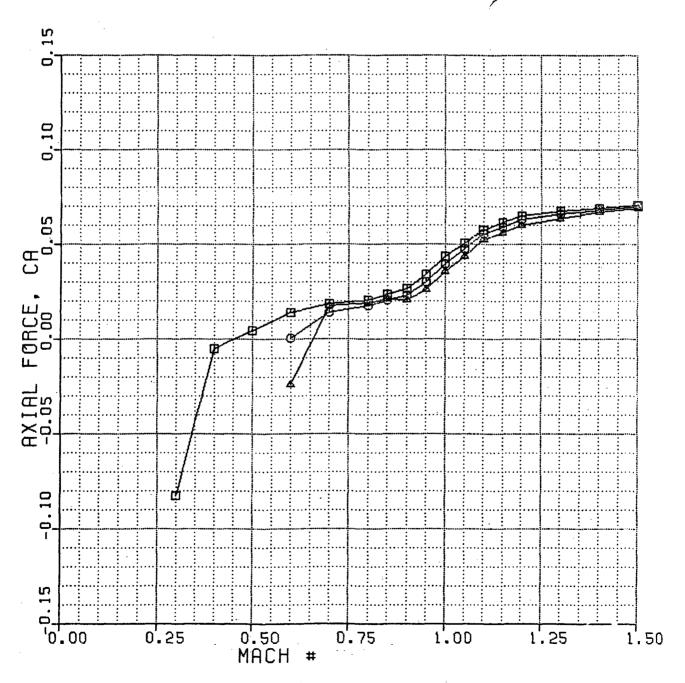


Figure 19(b)

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CA VS ALPHA

6-15-83 X-29A M# = 0.4 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = S.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22

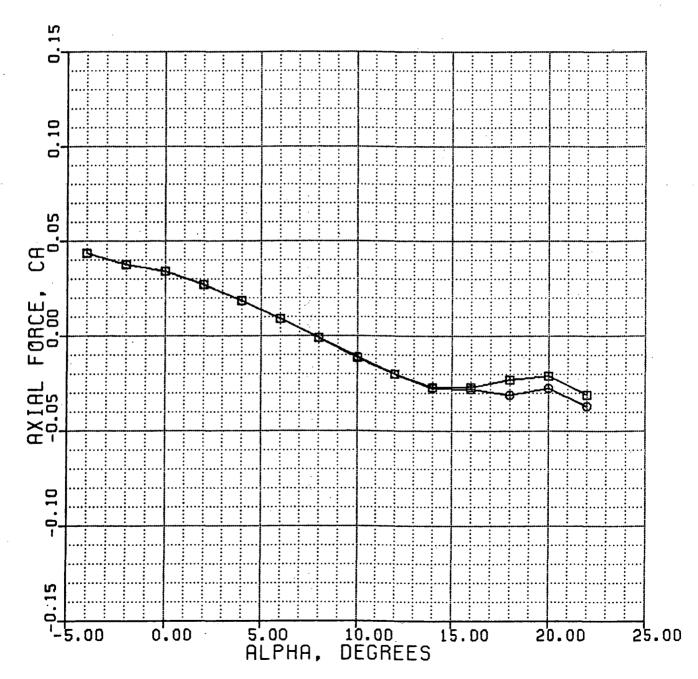
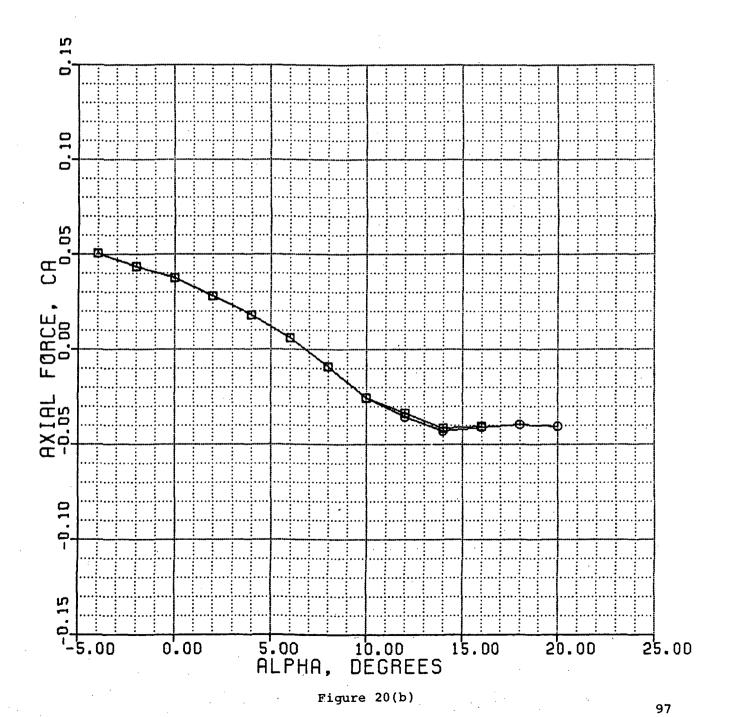


Figure 20(a)

CA VS ALPHA

6-16-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20



CA VS ALPHA

7-28-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

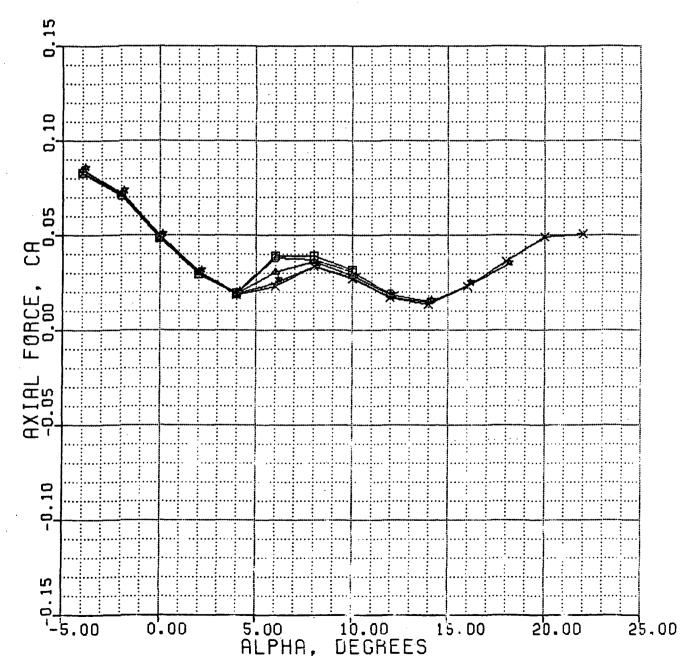
```
P ALT = 10K ALP: 0 T0 10

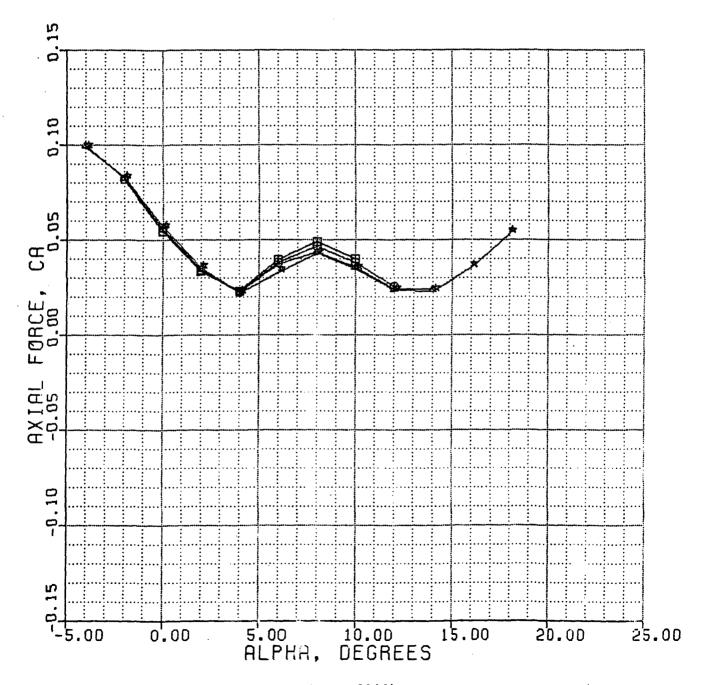
P ALT = 20K ALP: -4 T0 12

ALT = 30K ALP: -4 T0 14

ALT = 40K ALP: -4 T0 18

ALT = 50K ALP: -4 T0 22
```





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CA: VS ALPHA
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7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

D ALT = 20K ALP: -4 TO 8

D ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14

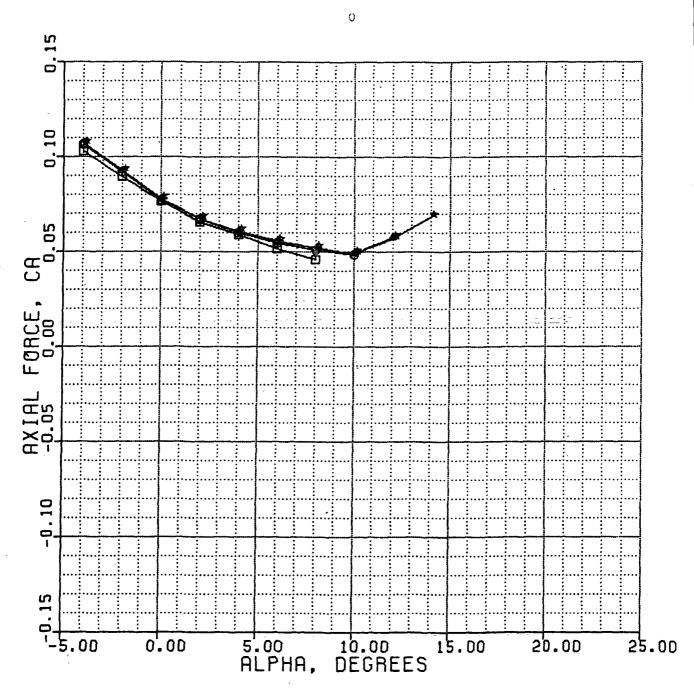


Figure 20(e)

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CA VS ALPHA

7-1-83 X-29A M# = 1.5 NØRMAL MØDE

XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8 9 ALT = 40K ALP: -4 TO 10 A ALT = 50K ALP: -4 TO 12

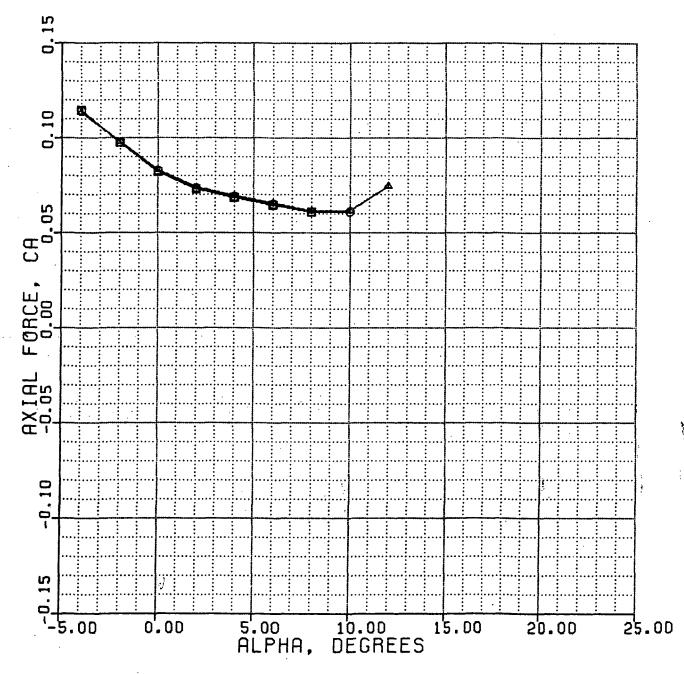
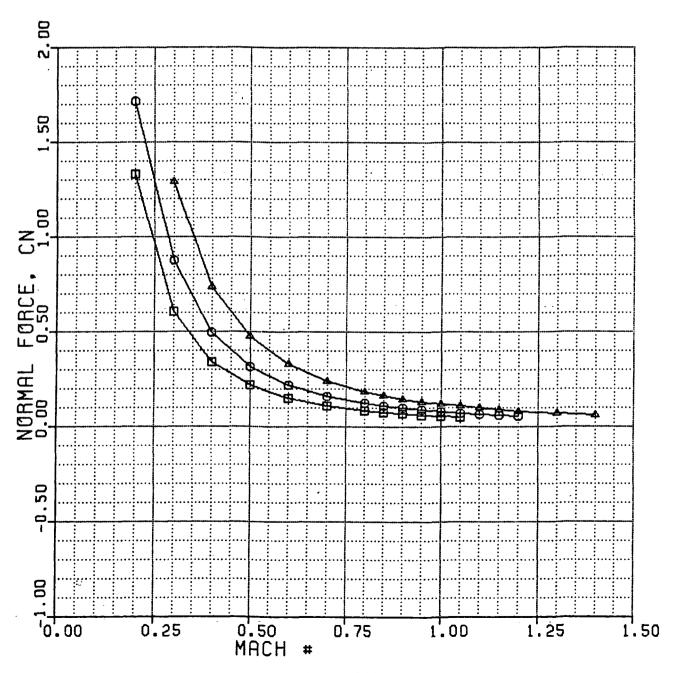
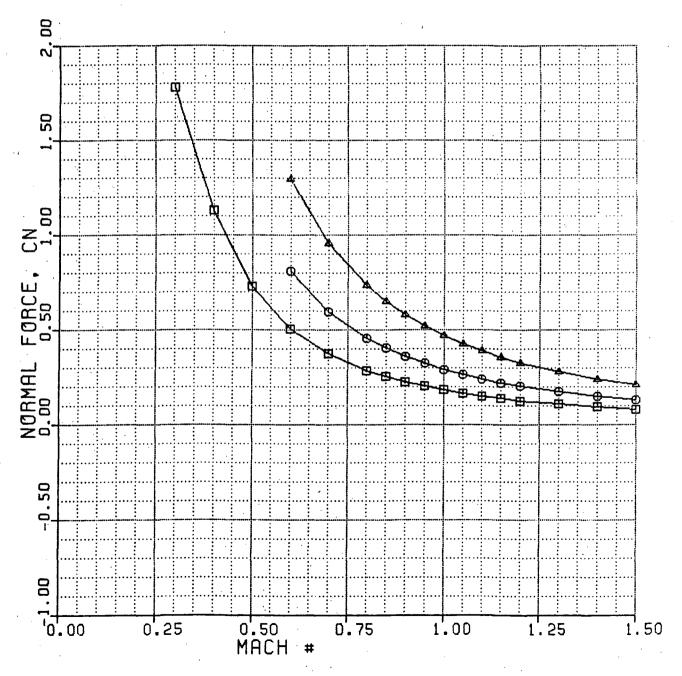


Figure 20(f)



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CN-NORMAL VS ALPHA
6-15-83 X-29A M# = 0.4 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM

B RLT = 5.L. ALP: -4 TO 22
B RLT = 10K ALP: -4 TO 22

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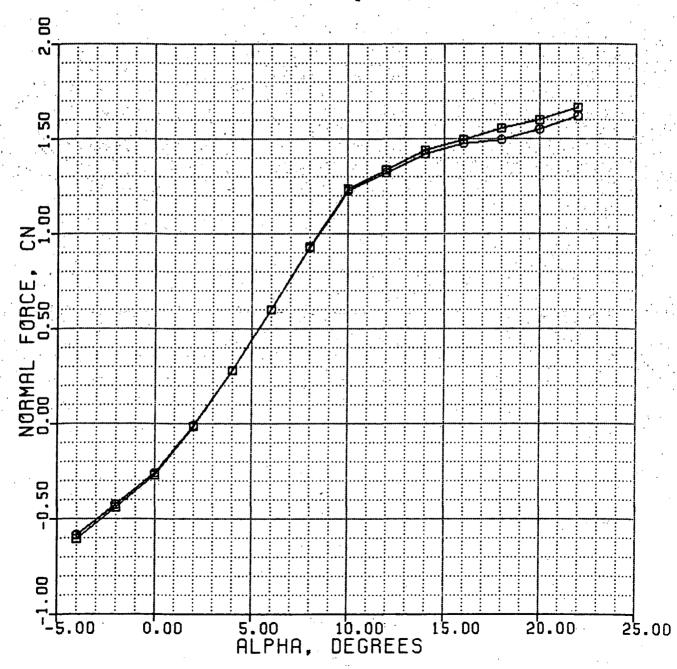
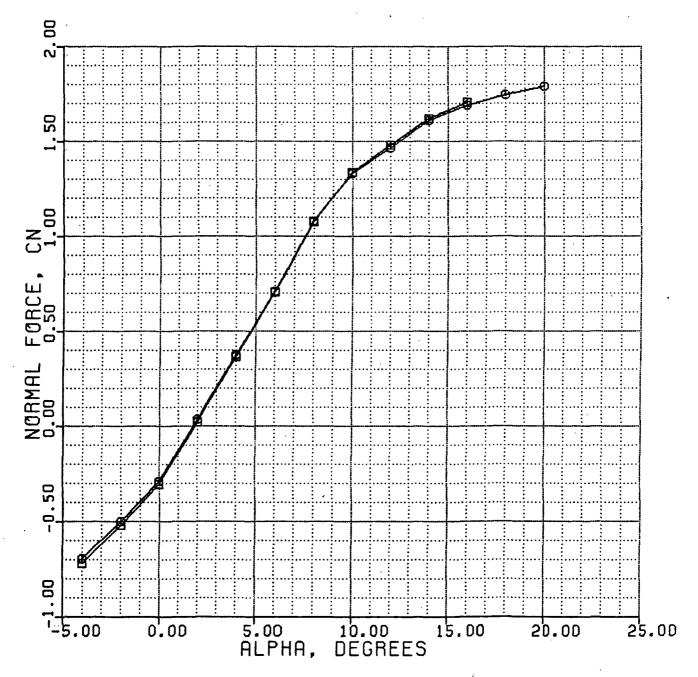


Figure 22(a)



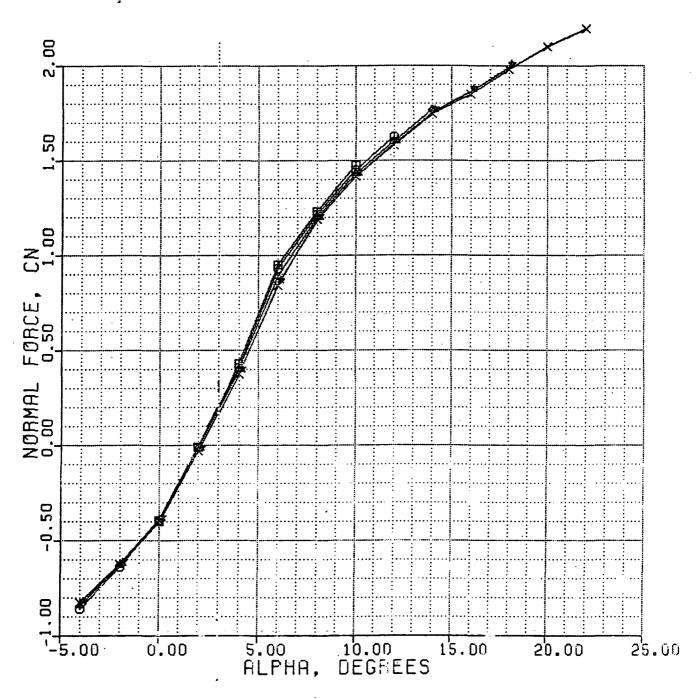
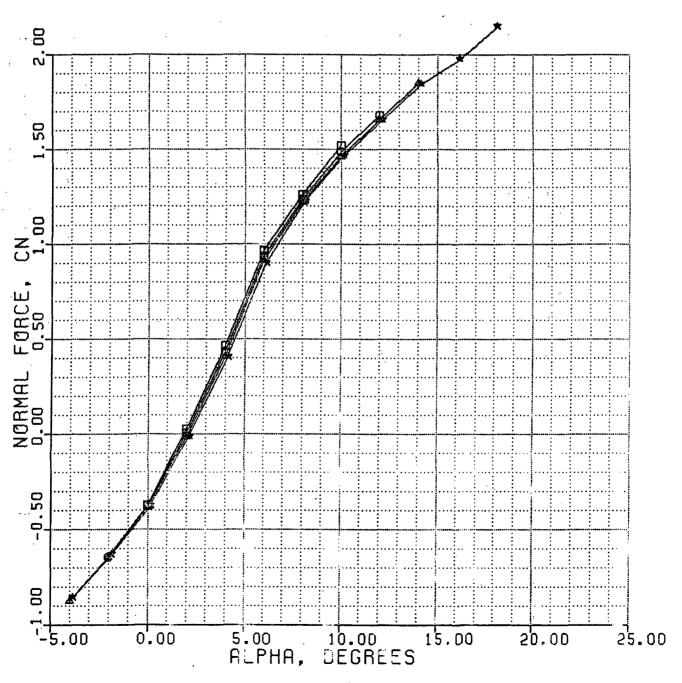


Figure 22(c)



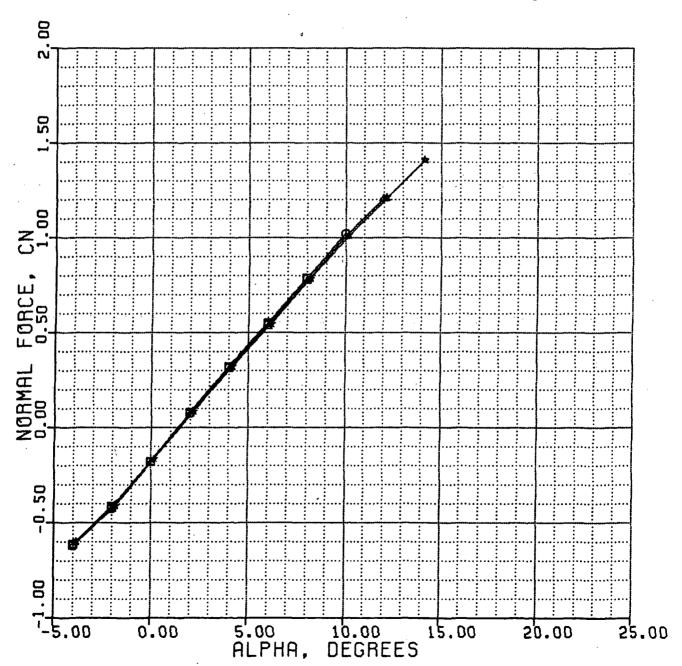


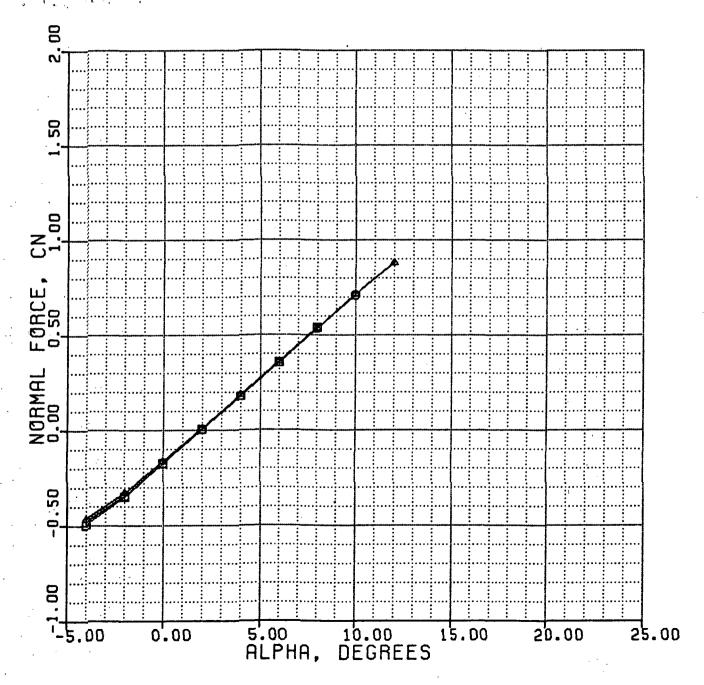
Figure 22(e)

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CN-NORMAL VS ALPHA

 $7-1-83 \cdot X-29A \cdot M# = 1.5 \cdot NORMAL MODE$

XCG = 451.0 WT = 15K ALPHA TRIM



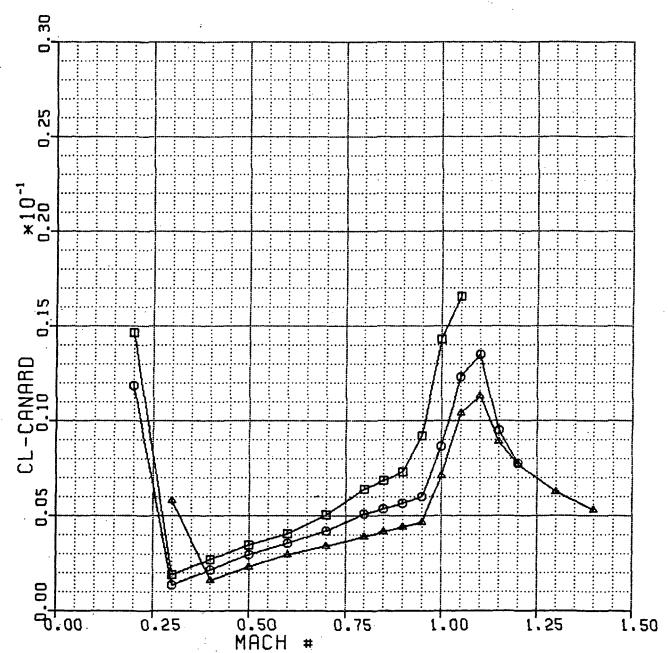


Figure 23(a)

```
CL-CANARD VS MACH #

7-7-83 X-29A 1-G TRIM NORMAL MODE

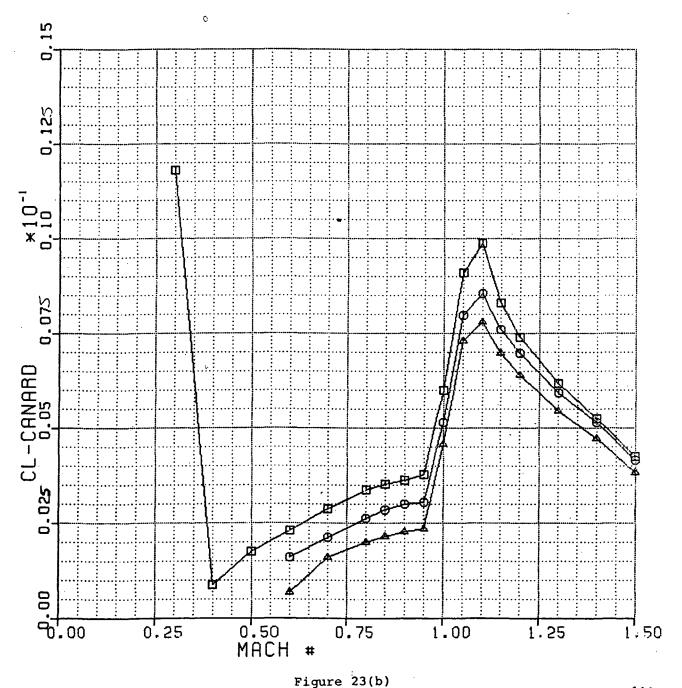
XCG = 451.0 WT = 15K

BALT = 30K M# = .3 TO 1.5

ALT = 40K M# = .6 TO 1.5

ALT = 50K M# = .6 TO 1.5

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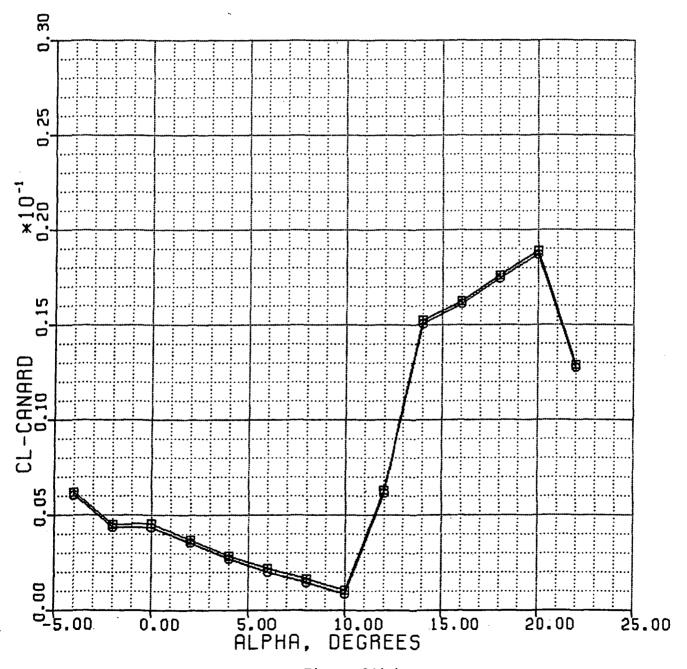


Figure 24(a)

ALP: -4 TO 20

-0 ALT = 20K

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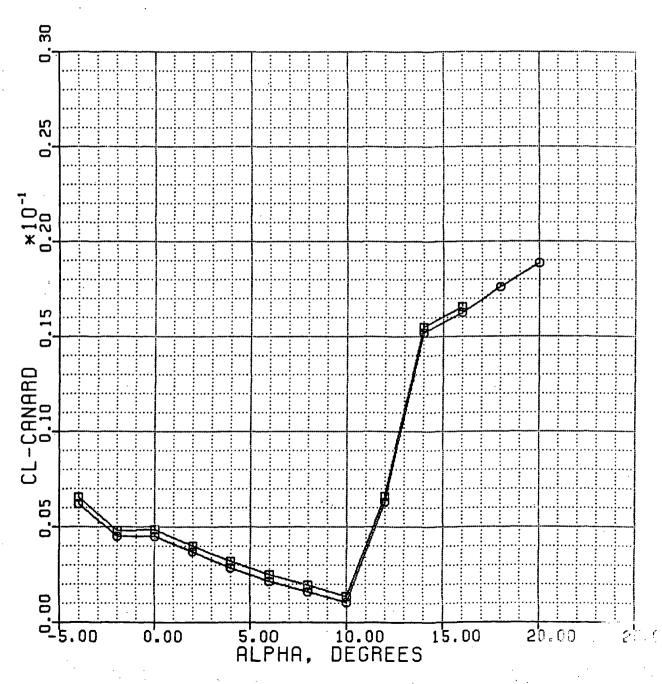


Figure 24(b)

```
CL-CANARD VS ALPHA
6-30-83 X-29A M# = 0.8
                                 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM
 P ALT = 10K
                  ALP:
                        O TO 10
     \underline{\underline{-}} ALT = 20K
                   ALP: -4 TO 12
    ____ ALP = 30K
                  ALP: -4 TO 14
                  ALP: -4 TO 18
     ____ * ALT = 40K
                                 ORIGINAL PAGE IS
      → ALT = 50K
                  -ALP: -4 TO 22
                                   OF POOR QUALITY
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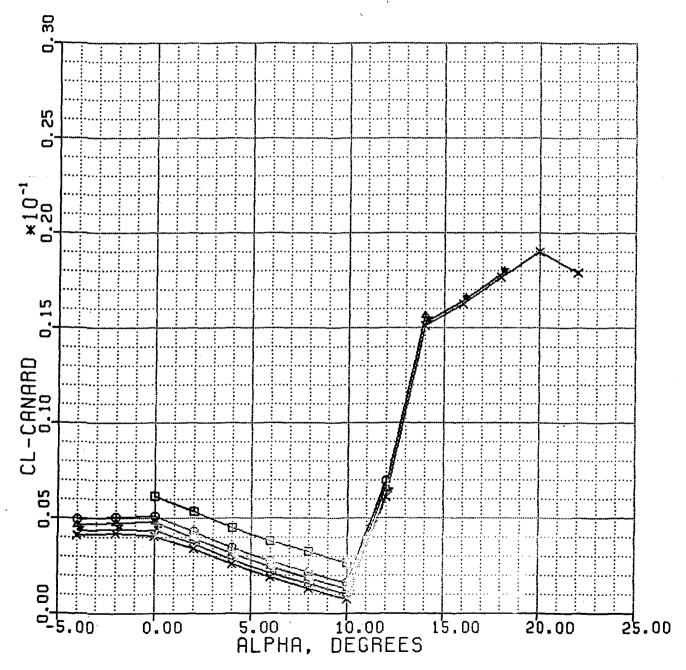
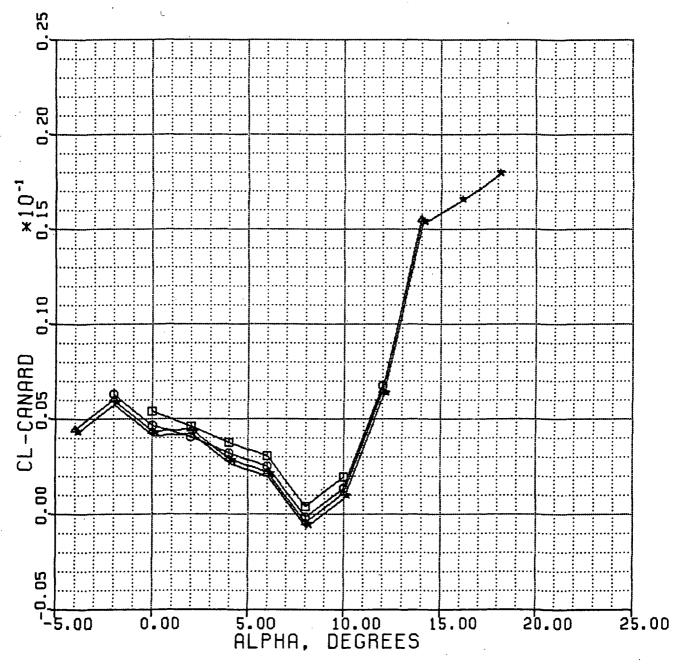


Figure 24(c)



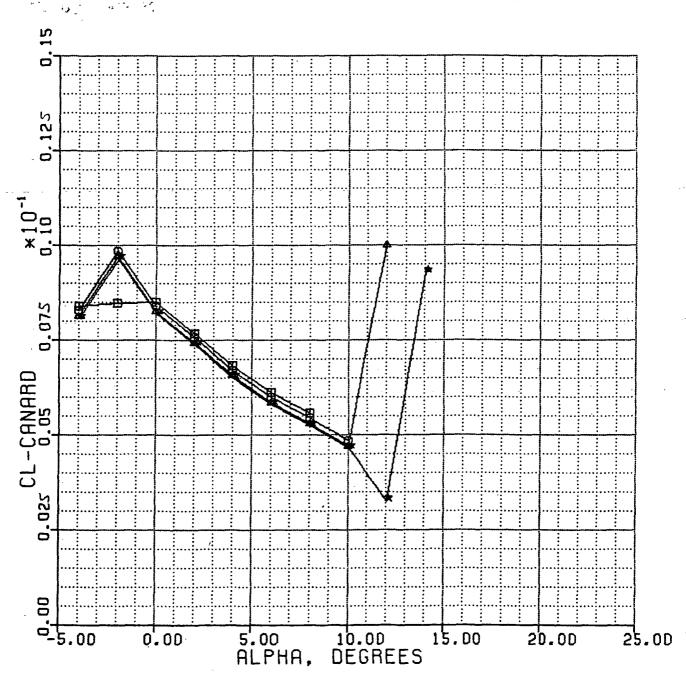


Figure 24(e)

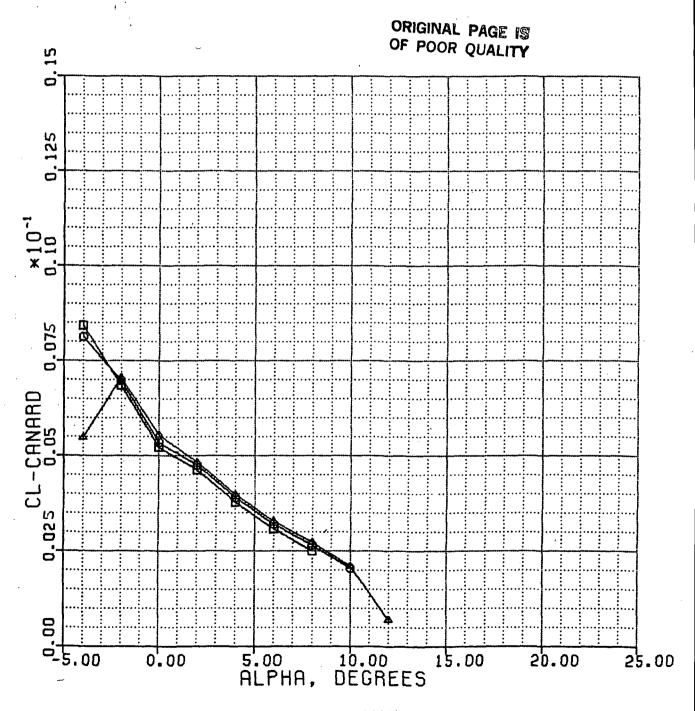


Figure 24(f)

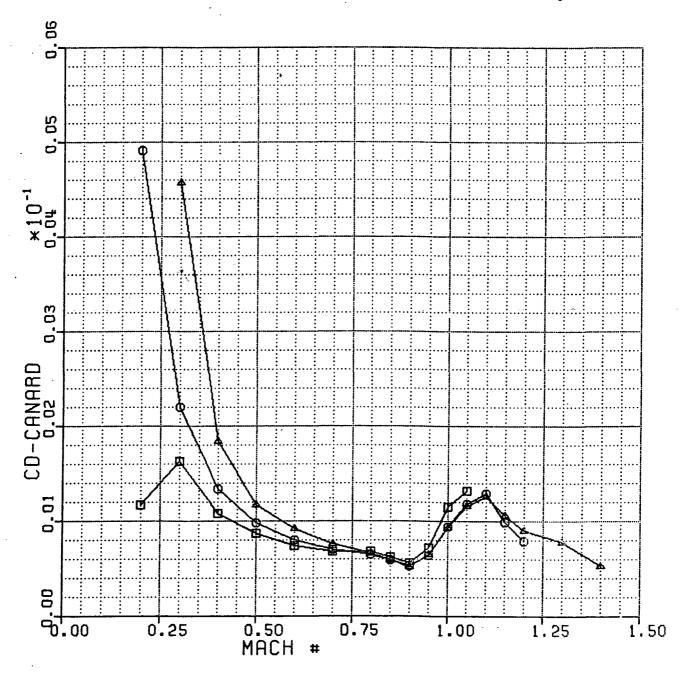
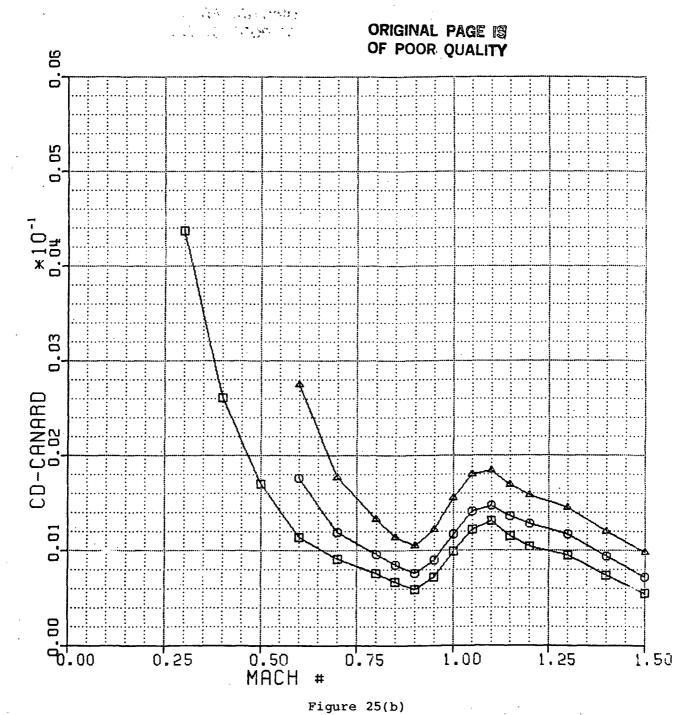


Figure 25(a)



CD-CANARD VS ALPHA 6-16-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM B ALT = S.L. ALP: -4 TO 22 B ALT = 10K ALP: -4 TO 22

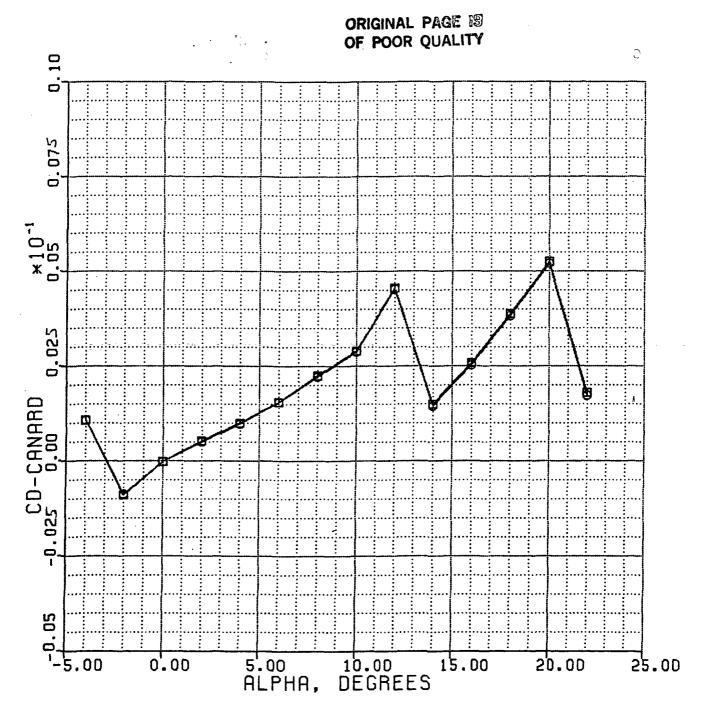


Figure 26(a)

MARKET SOFT

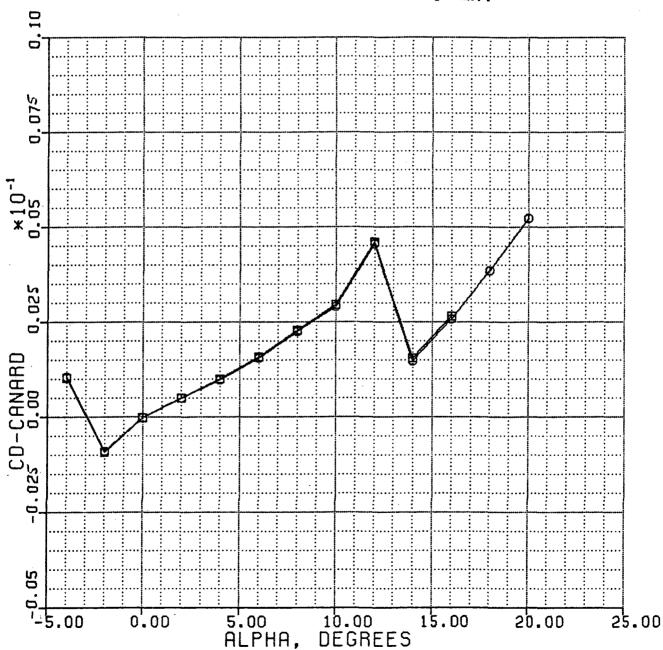


Figure 26(b)

```
CD-CANARD VS ALPHA
6-30-83 X-29A M# = 0.8 NORMAL MODE
XCG = 451.0 WT = 15K. ALPHA TRIM
     _pg ALT = 10K
                 ALP:
                      D TO 10
     ______ ALT = 20K
                 ALP: -4 TO 12
    __A RLP = 30K
                 ALP: -4 TO 14
                             ORIGINAL PAGE IS
                 ALP: -4 TO 18
     __★ ALT = 40K
                               OF POOR QUALITY
     __X ALT = 50K
                 ALP: -4 TO 22
```

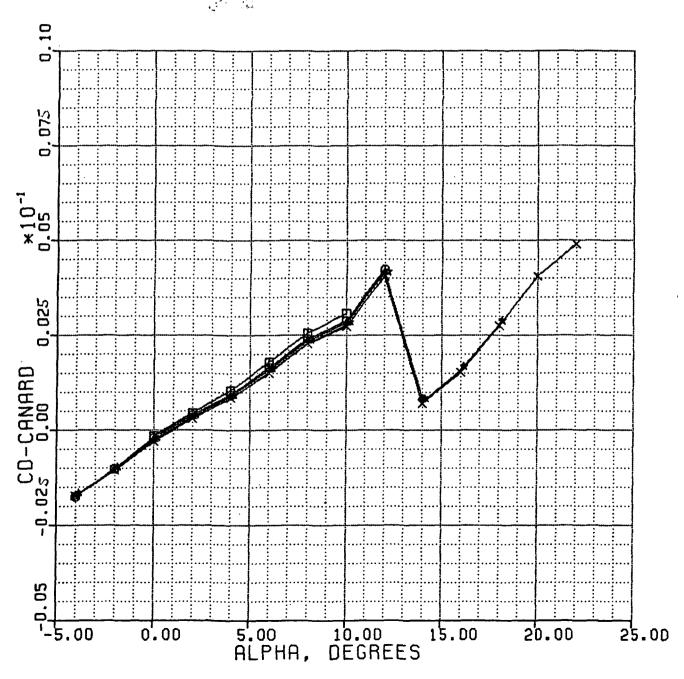
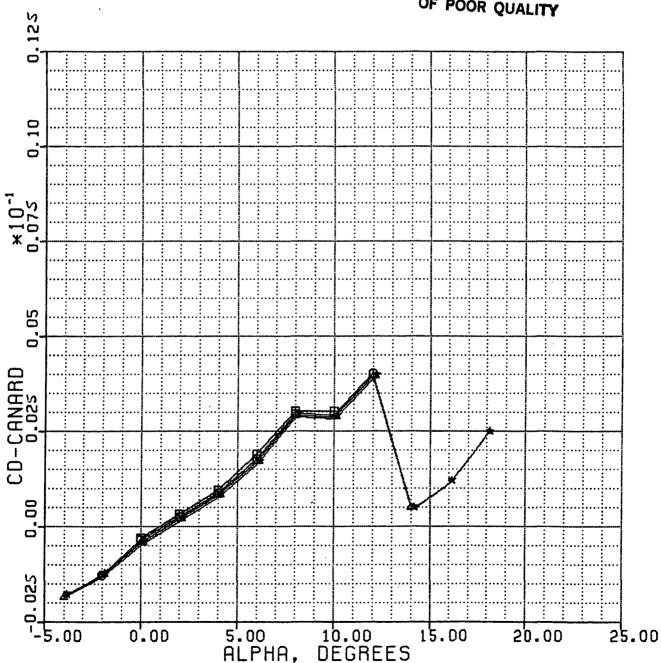
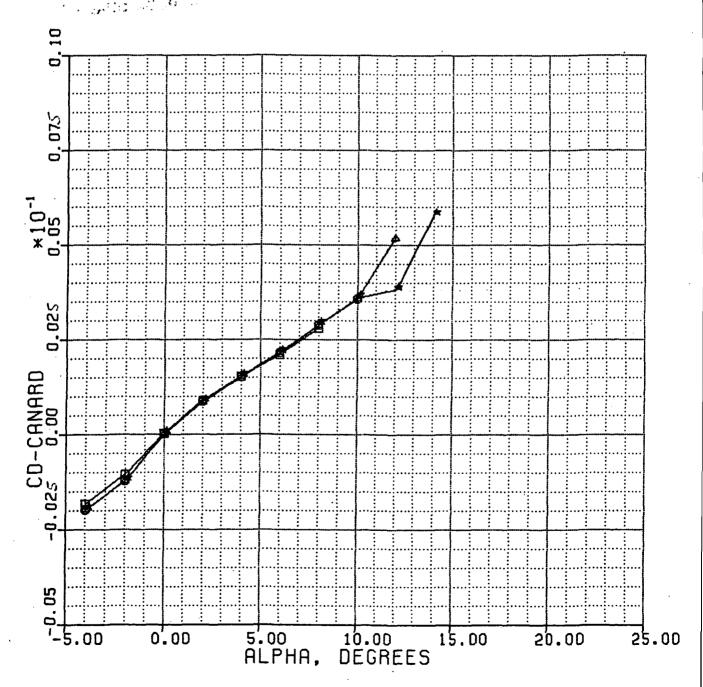


Figure 26(c)



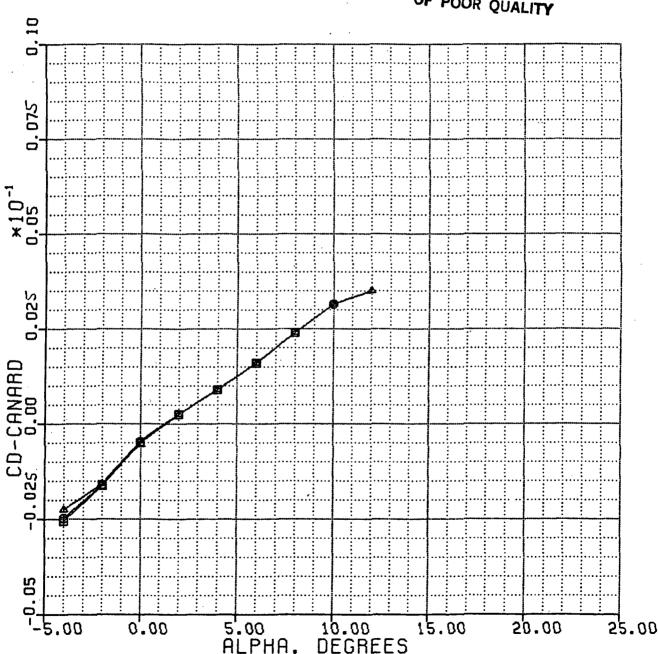


CD-CANARD VS ALPHA

7-1-83 X-29A M# = 1.5 NØRMAL MØDE

XCG = 451.0 WT = 15K ALPHA TRIM

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CM-CANARD VS MACH #1
7-5-83 X-29A 1-G TRIM NORMAL NOBE

XCG = 451.0 WT = 15K

B RLT = S.L. M# = .2 TG 1.05

B RLT = 10K M# = .2 TG 1.2

ARLT = 20K M# = .3 TG 1.4

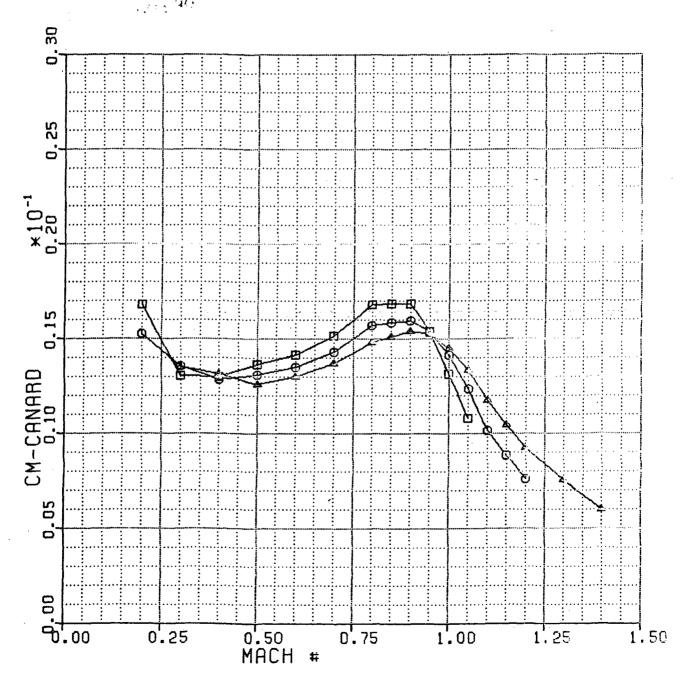


Figure 27(a)

The Congress of

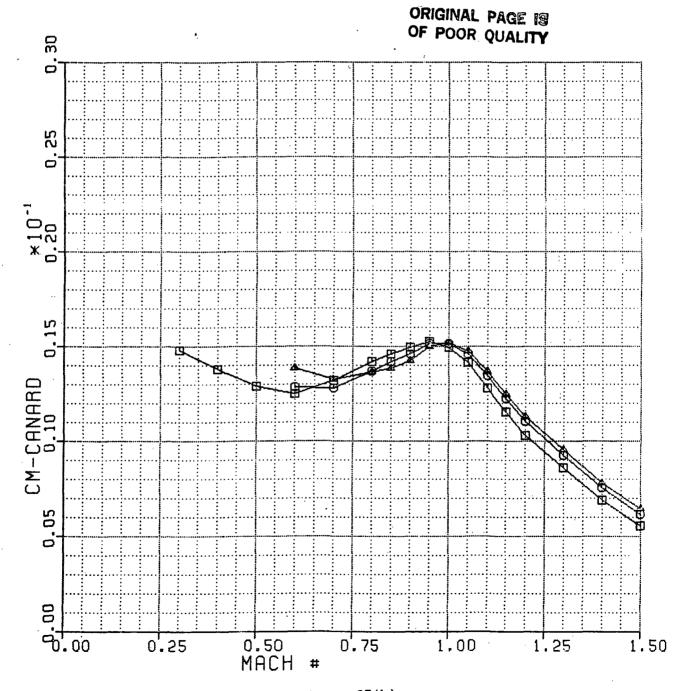
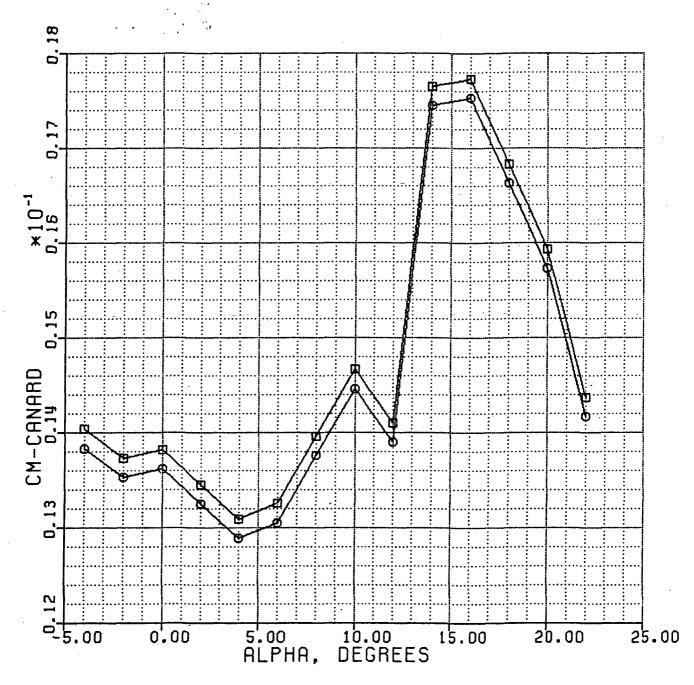


Figure 27(b)

CM-CANARD VS ALPHA
6-16-83 X-29A M# = 0.4 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = S.L. ALP: -4 TO 22
B ALT = 10K ALP: -4 TO 22



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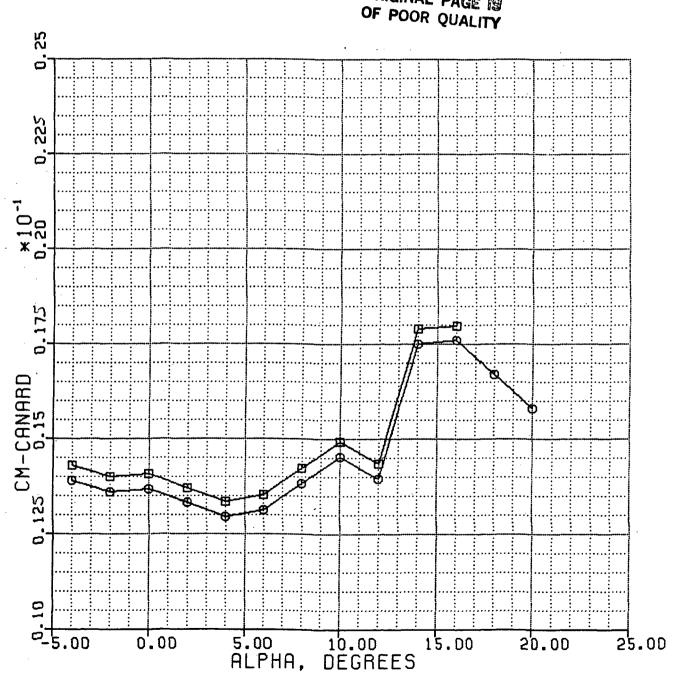


Figure 28(b)

```
CM-CANARD VS ALPHA

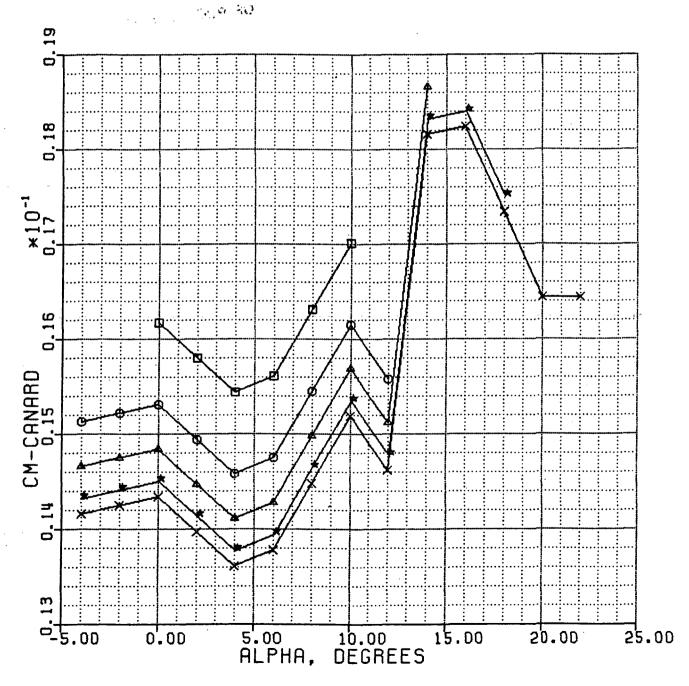
6-30-83 X-29A M# = 0.8 NØRMAL MØDE

XCG = 451.0 WT = 15K ALPHA TRIM

B RLT = 10K ALP: 0 TØ 10

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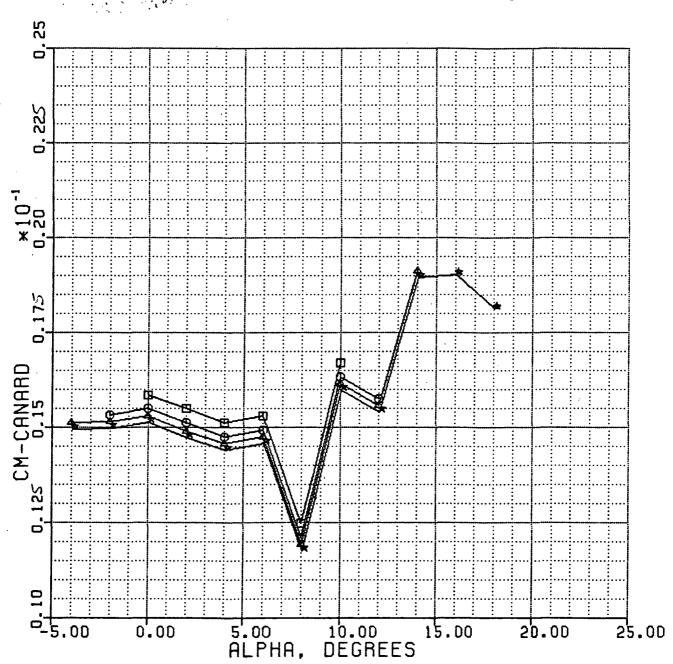


Figure 28(d)

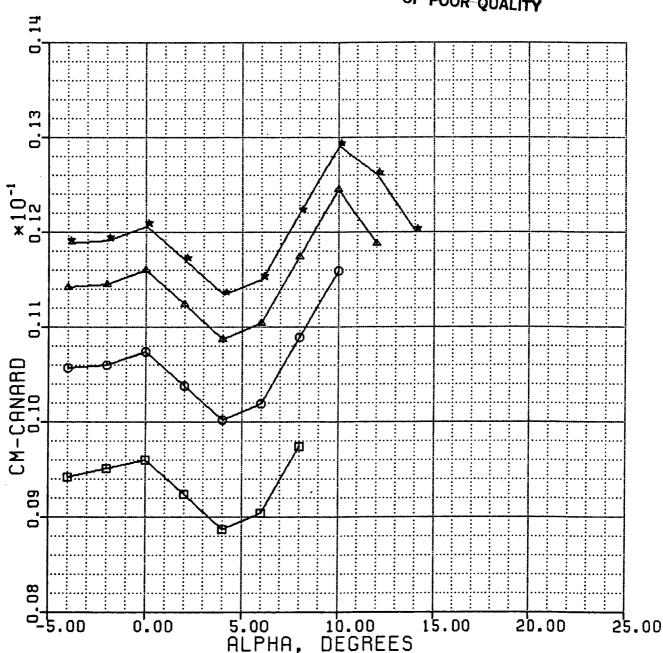


Figure 28(e)

CM-CANARD VS ALPHA
7-1-83 X-29A M# = 1.5 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

B RLT = 30K ALP: -4 TØ 8

B RLT = 40K ALP: -4 TØ 10
ALT = 50K ALP: -4 TØ 12

The Angles

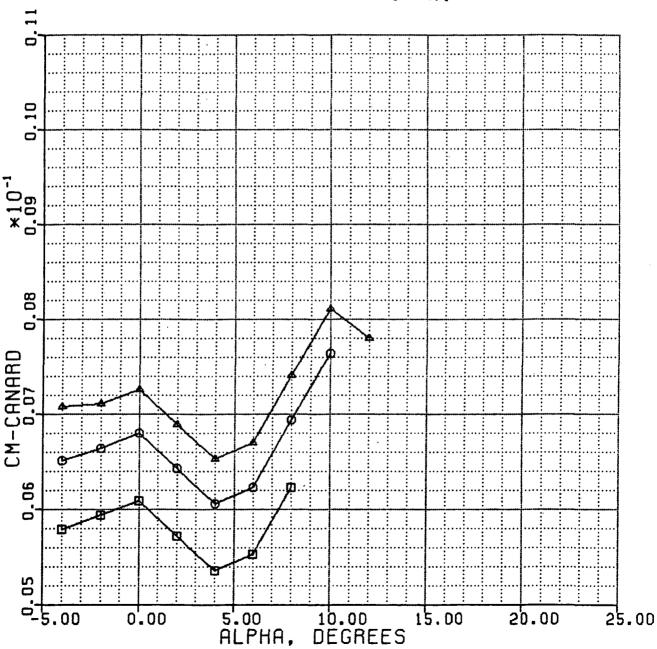


Figure 28(f)

```
CA-CANARD VS MACH #

7-6-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B RLT = 5.L. M# = .2 TO 1.05

P RLT = 10K M# = .2 TO 1.2

A RLT = 20K M# = .3 TO 1.4
```

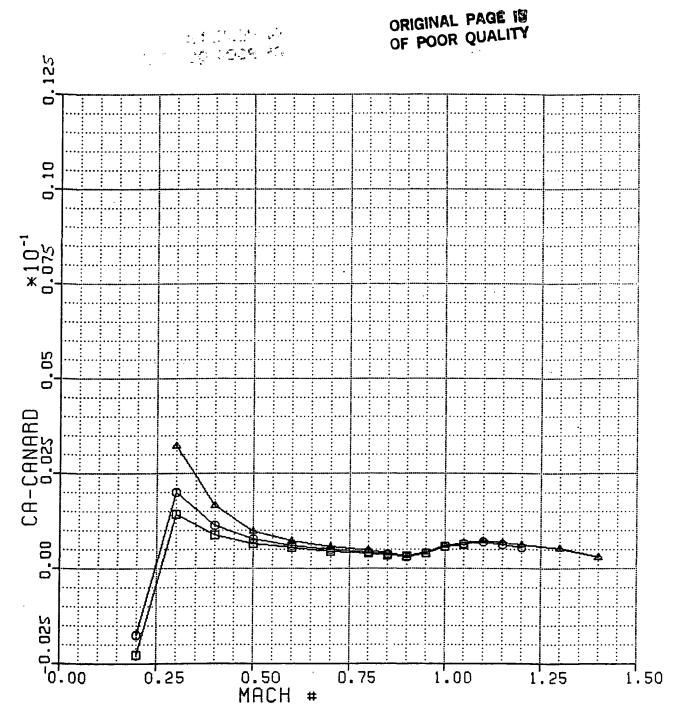


Figure 29(a)

CA-CANARD VS MACH # 7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

O ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

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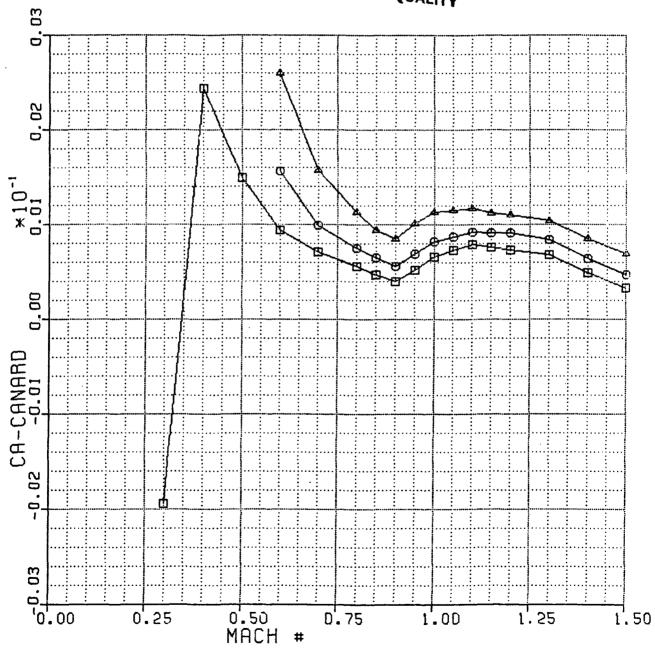


Figure 29(b)

CA-CANARD VS ALPHA
6-16-83 X-29A M# = 0.4 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

B RLT = S.L. ALP: -4 TØ 22
B RLT = 10K ALP: -4 TØ 22

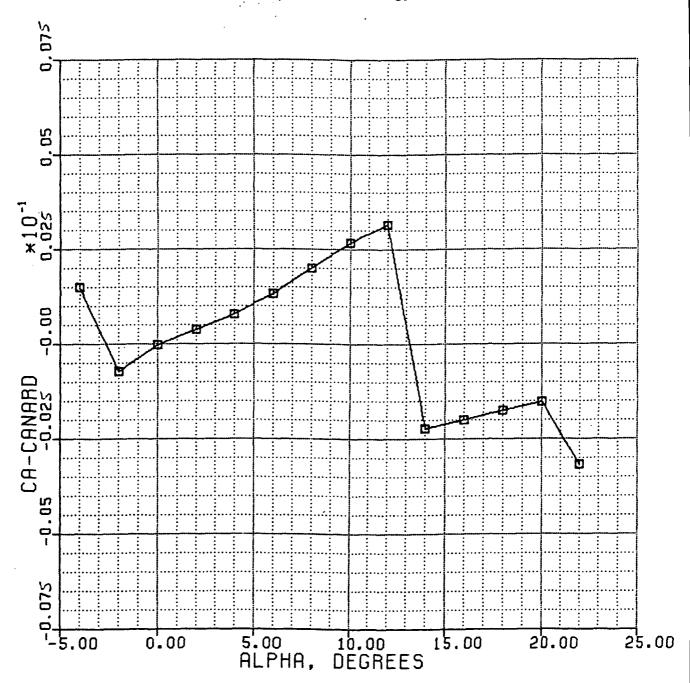
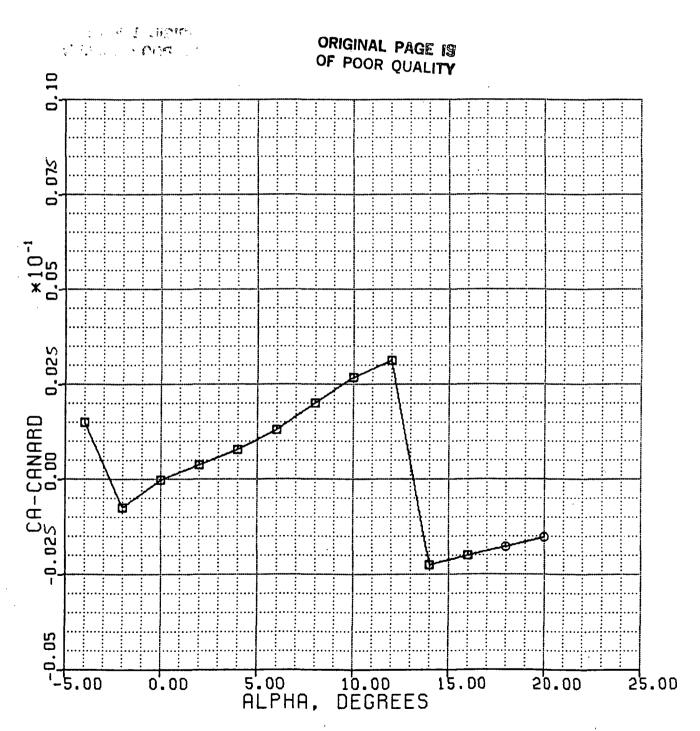


Figure 30(a)



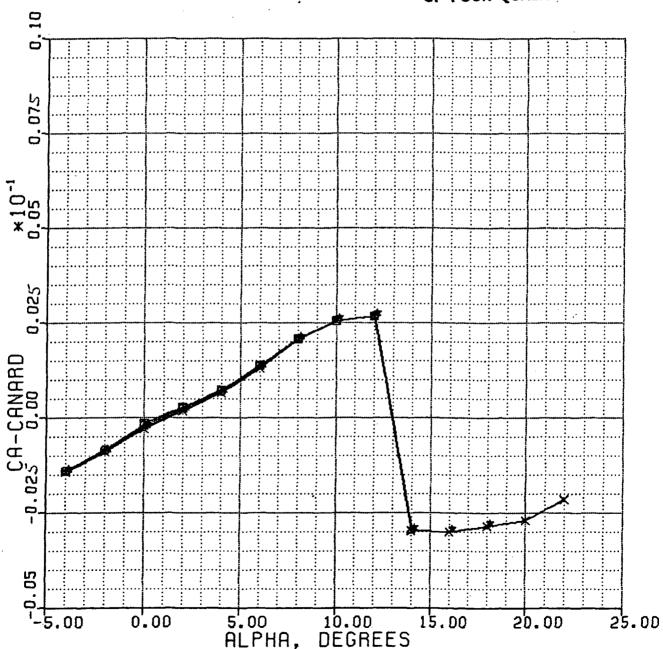
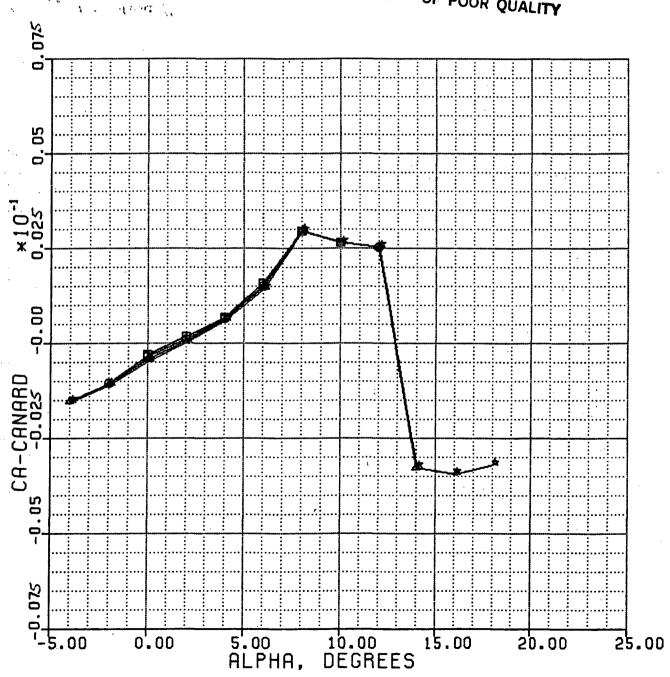


Figure 30(c)

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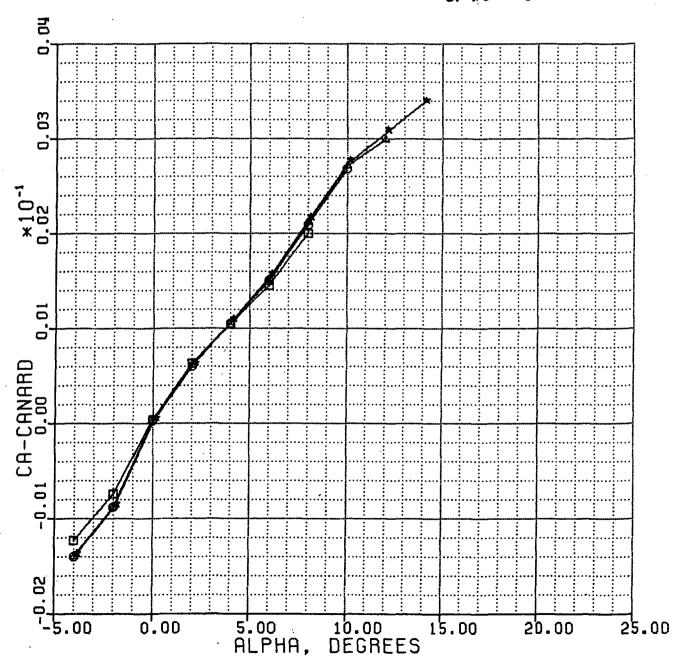
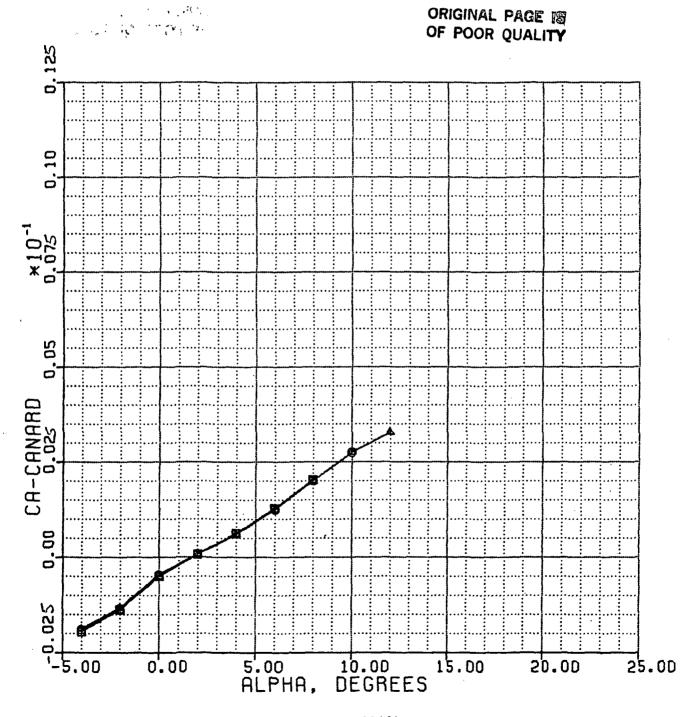


Figure 30(e)



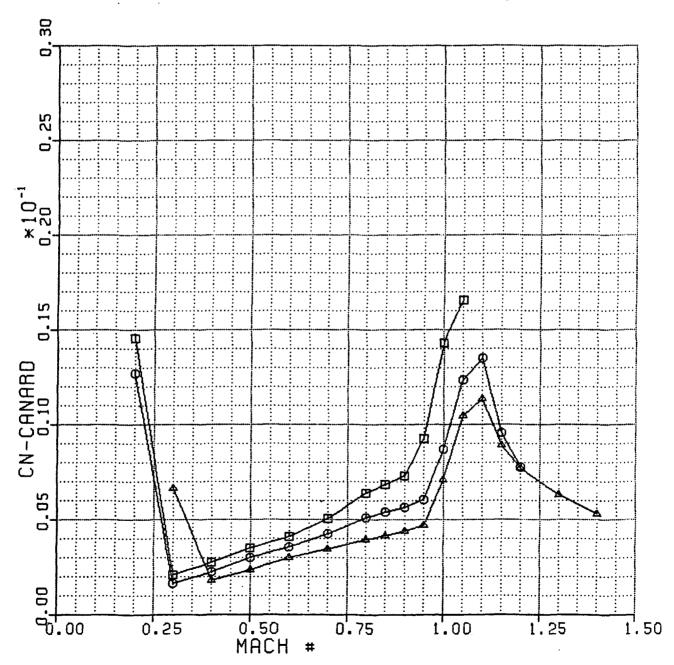


Figure 31(a)

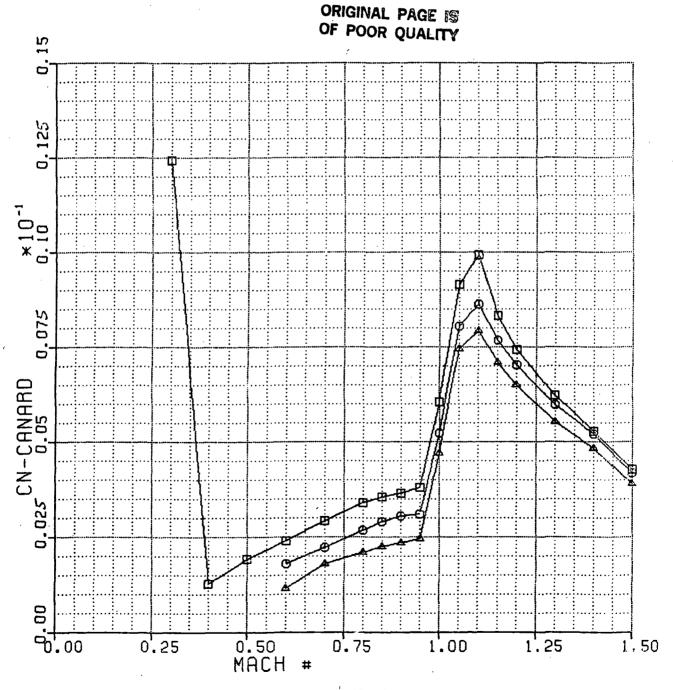


Figure 31(b)

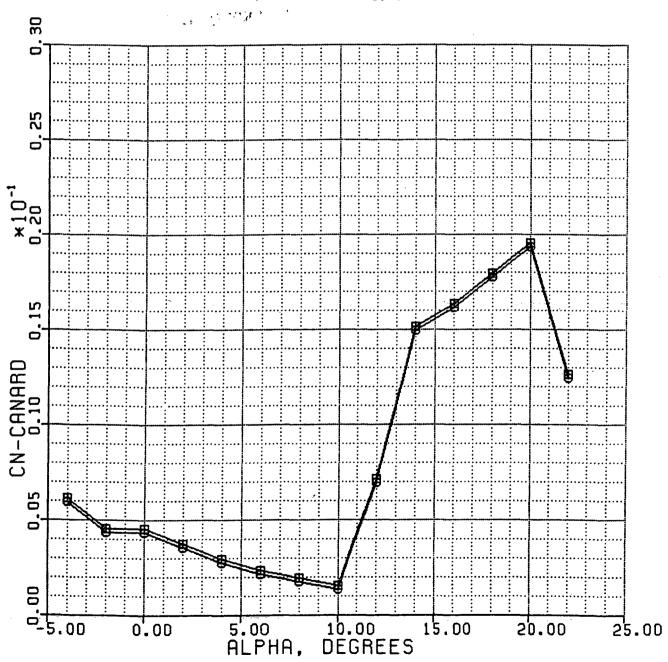
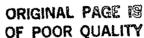


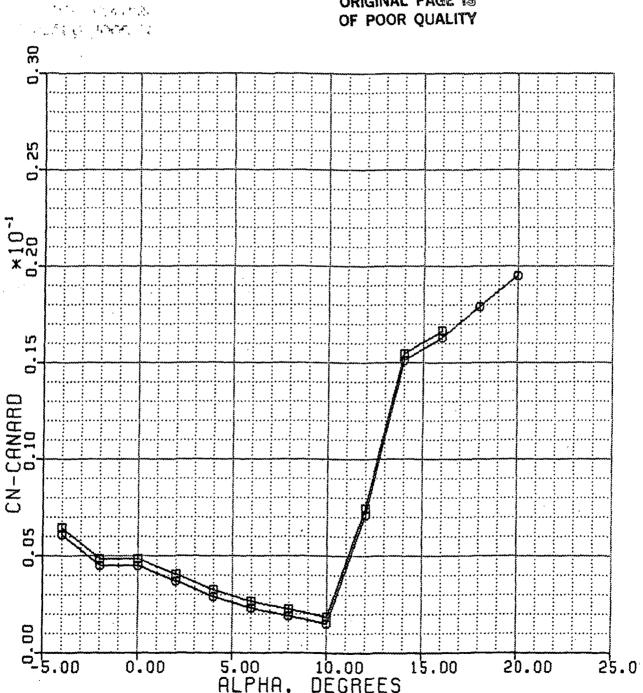
Figure 32(a)

CN-CANARD VS ALPHA

6-17-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 10K ALP: -4 TO 16





CN-CANARD VS ALPHA 6-30-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM PALT = 10K ALP: 0 TØ 10 PALT = 20K ALP: -4 TØ 12 ALP = 30K ALP: -4 TØ 14 ALT = 40K ALP: -4 TØ 18 X ALT = 50K ALP: -4 TØ 22

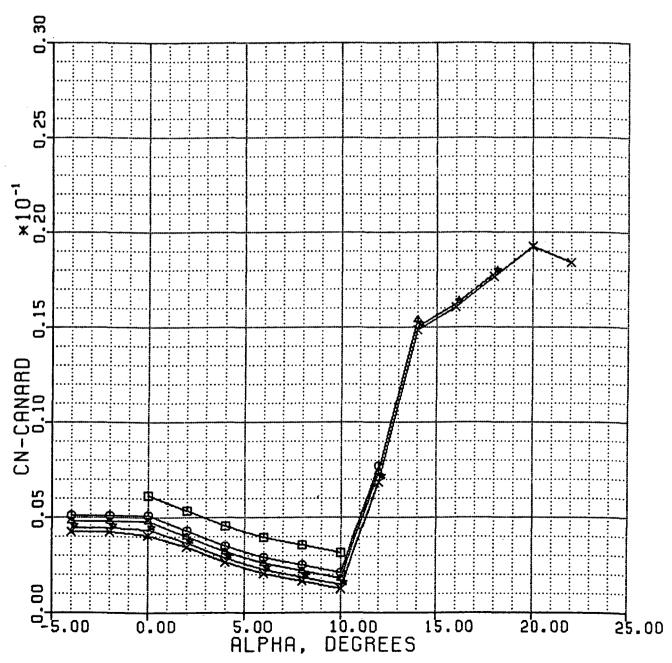


Figure 32(c)

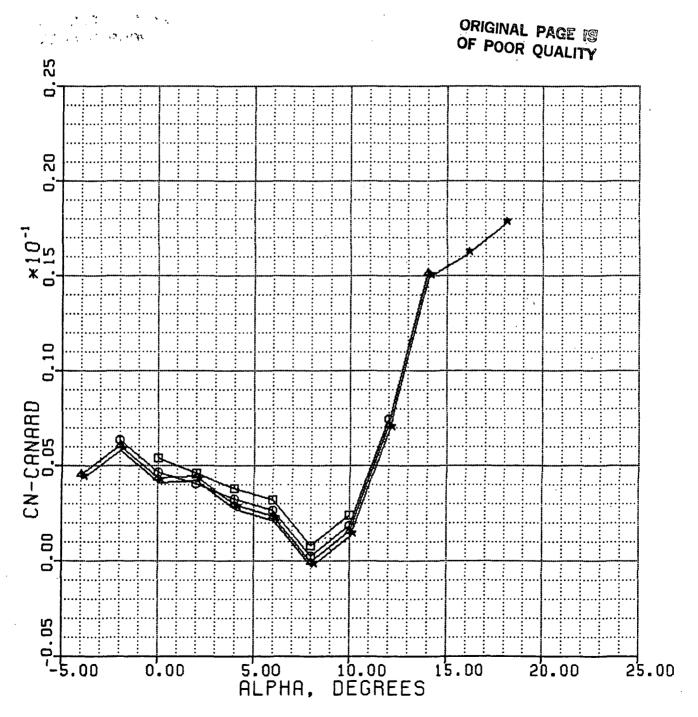


Figure 32(d)

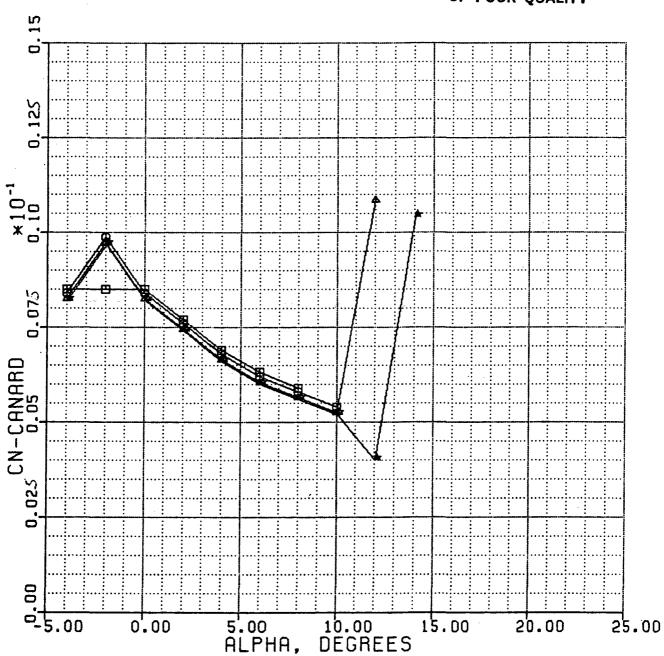
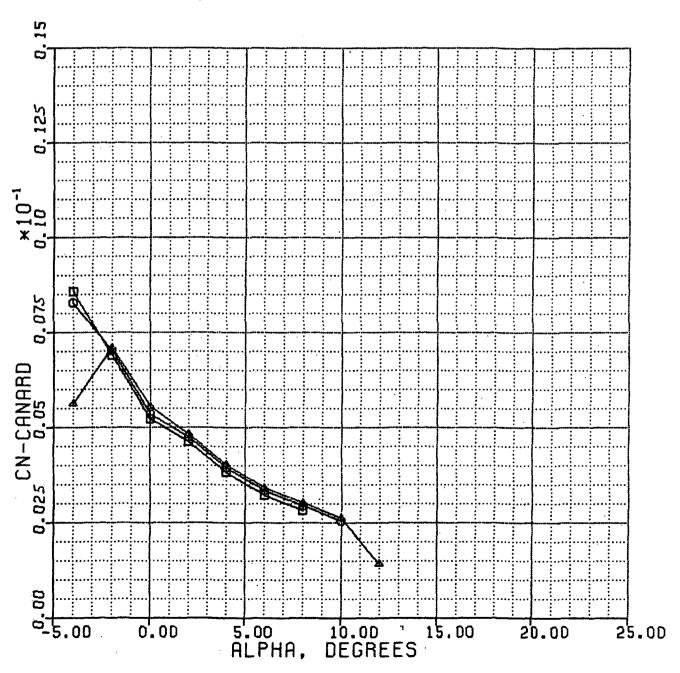


Figure 32(e)

____ ALT = 50K ALP: -4 TO 12

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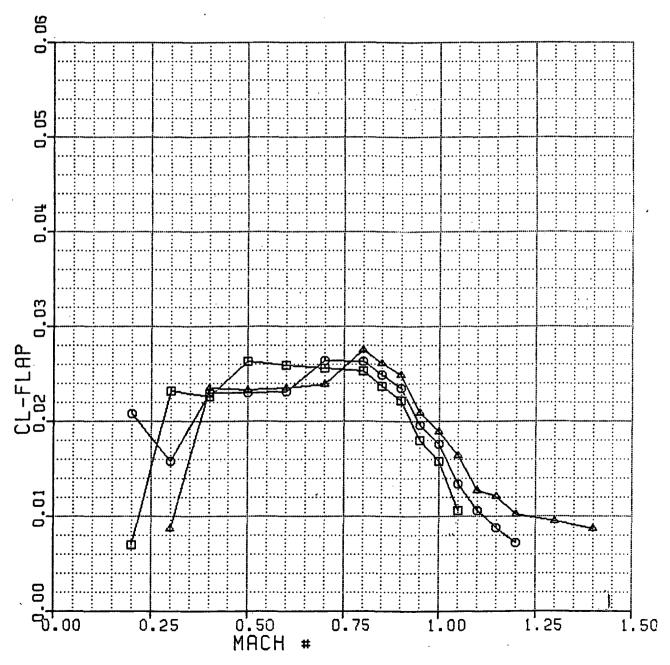


Figure 33(a)

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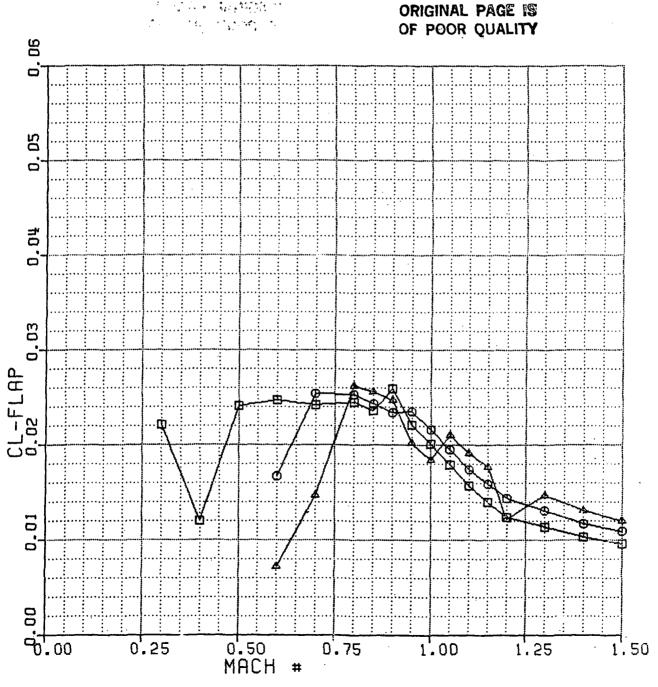
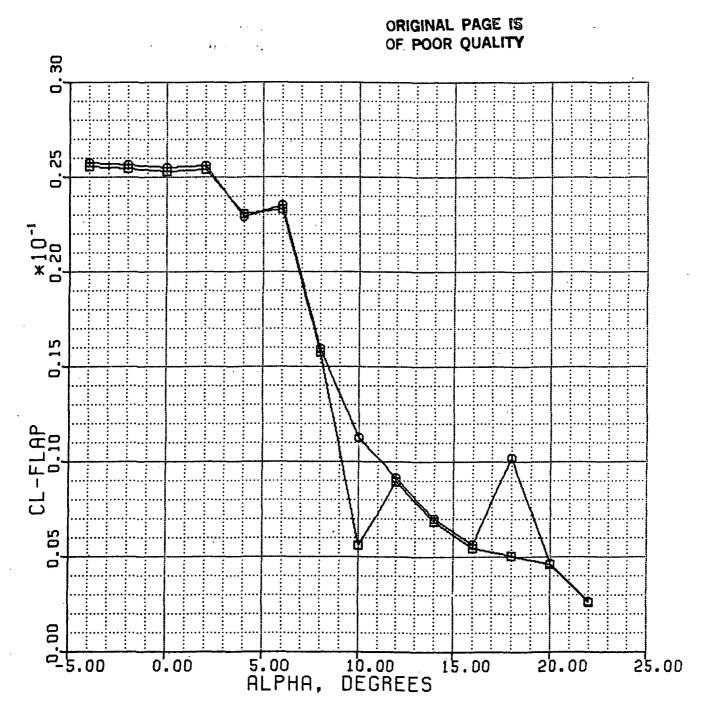
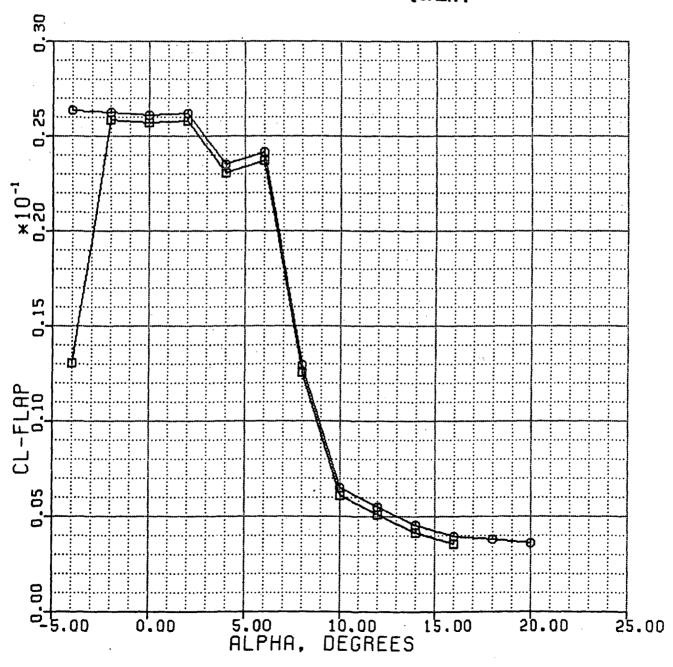


Figure 33(b)





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CL-FLAP VS ALPHA

6-30-83 X-29A M# = 0.8 NØRMAL MØDE

XCG = 451.0 WT = 15K ALPHA TRIM

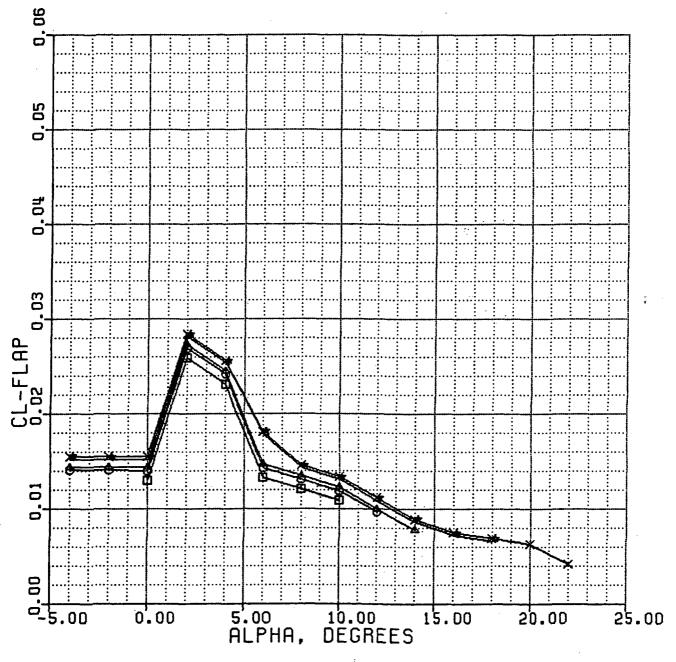
B ALT = 10K ALP: 0 TO 10

C ALT = 20K ALP: -4 TO 12

ALP = 30K ALP: -4 TO 14

ALP = 40K ALP: -4 TO 18

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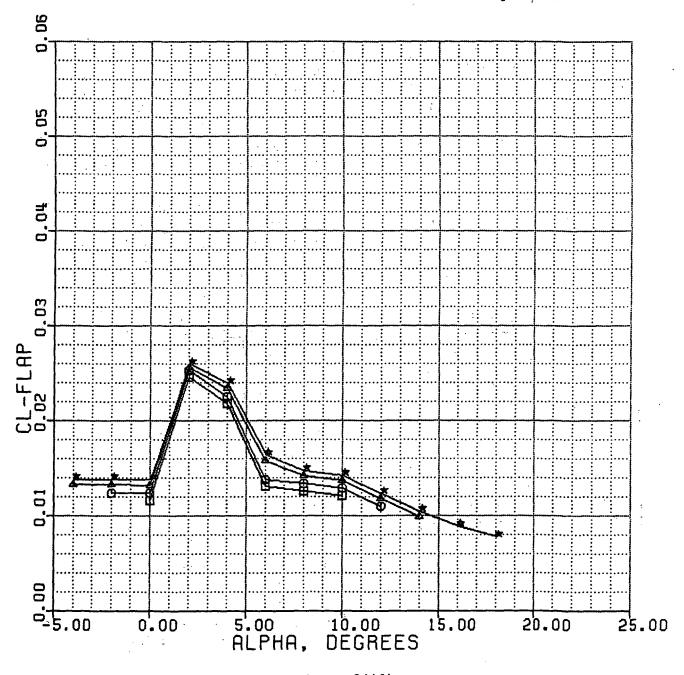


Figure 34(d)

CL-FLAP VS ALPHA

7-27-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
9 ALT = 20K ALP: -4 TO 8

9 ALT = 30K ALP: -4 TO 10

ALT = 40K ALP: -4 TO 12

ALT = 50K ALP: -4 TO 14
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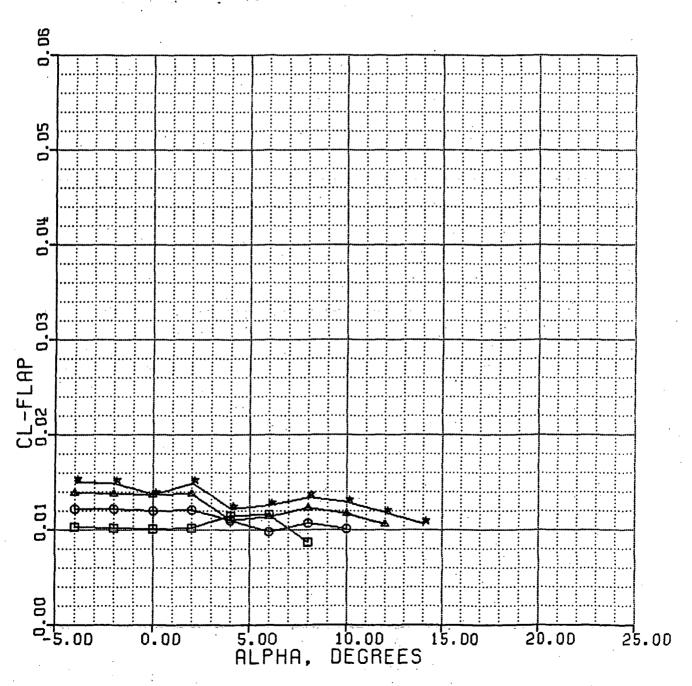


Figure 34(e)

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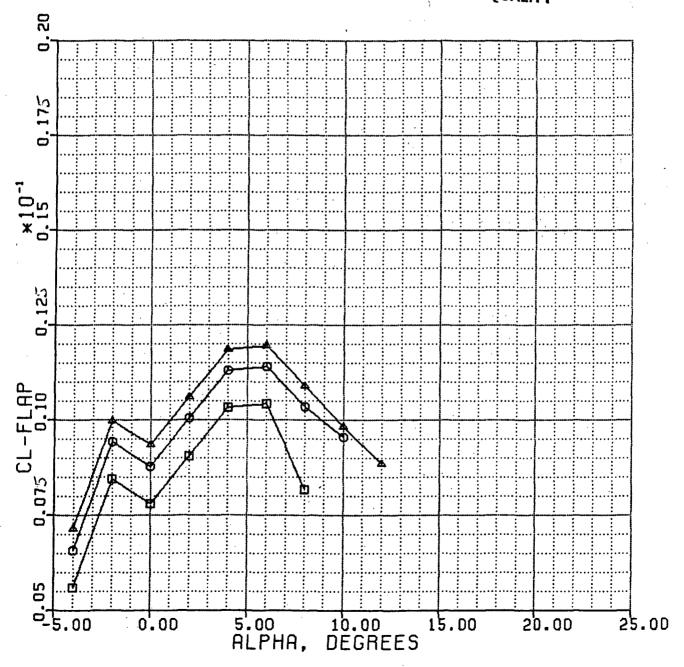


Figure 34(f)

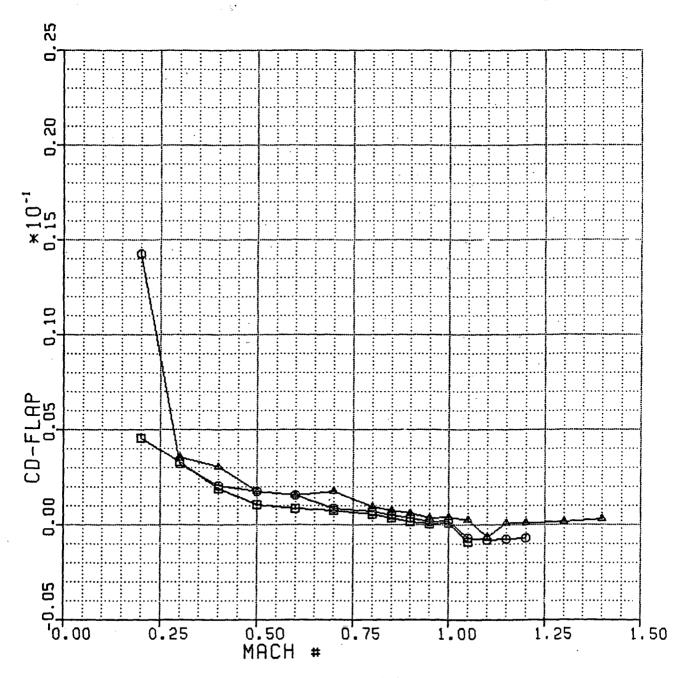


Figure 35(a)

STANCE BUTTONS

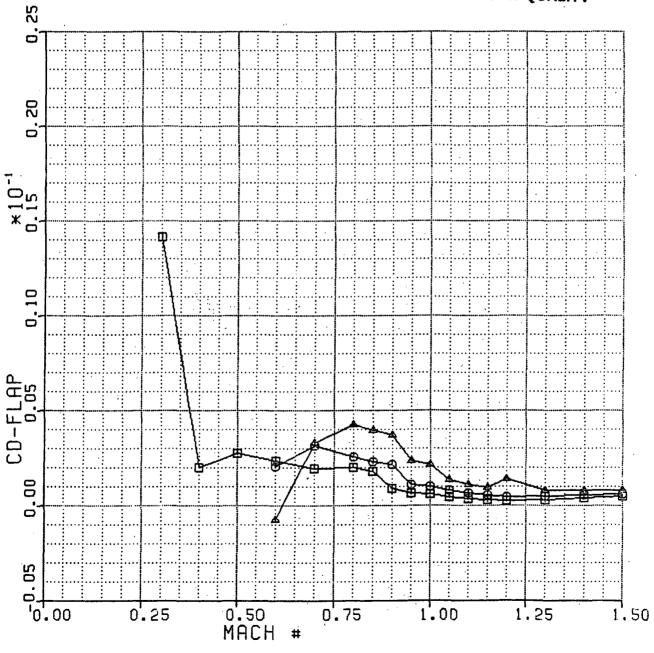


Figure 35(b)

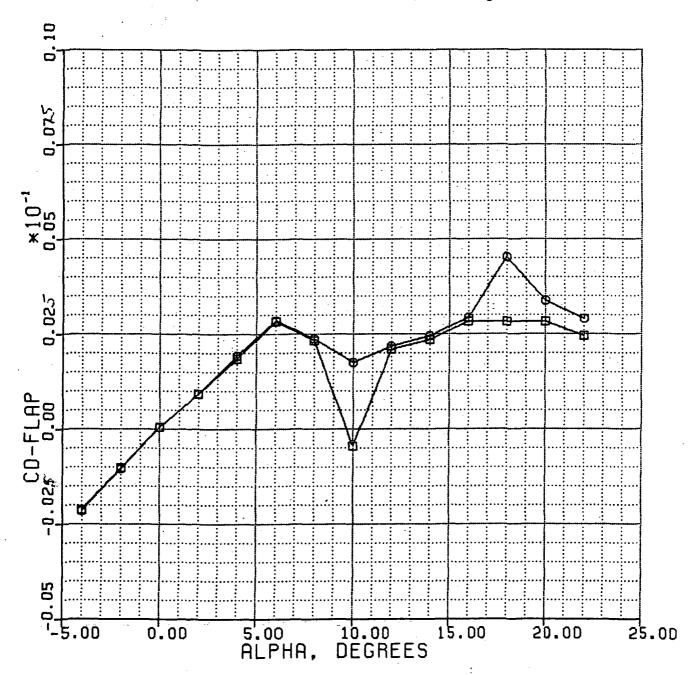
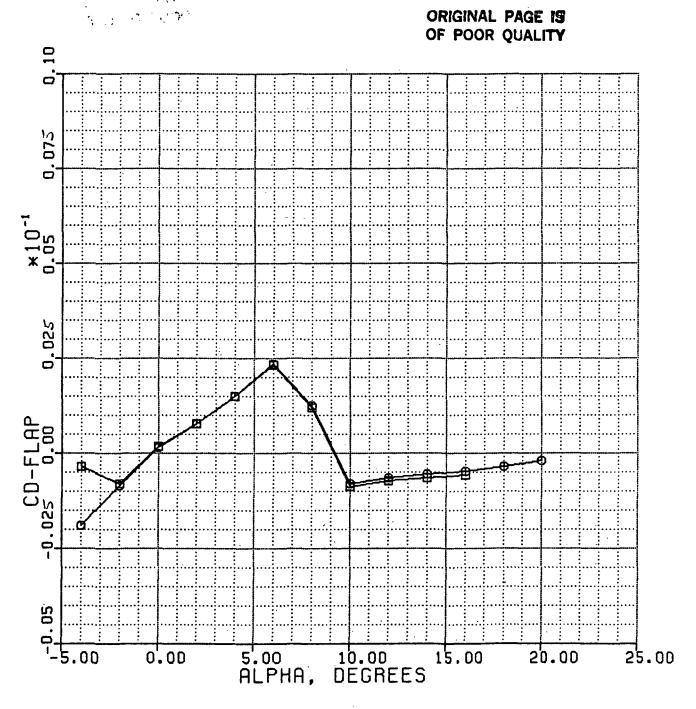
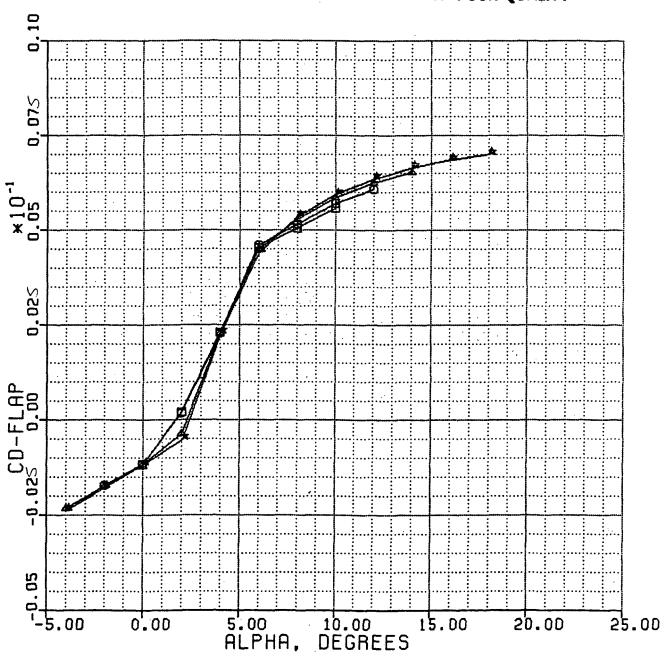


Figure 36(a)



CD-FLAP VS ALPHA 6-30-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM 9 RLT = 20K ALP: -4 TO 12 ____ ALP = 30K ALP: -4 TO 14 _★ ALT = 40K ALP: -4 TO 18 → ALT = 50K ALP: -4 TØ 22 ORIGINAL PAGE IS OF POOR QUALITY * 5 1 1 1 1 1 1 1 1 1 1 1 1 0.10 270 05 0'.00 10.00 5.00 5.00 20.00 15.DO 25.00 ALPHA, DEGREES



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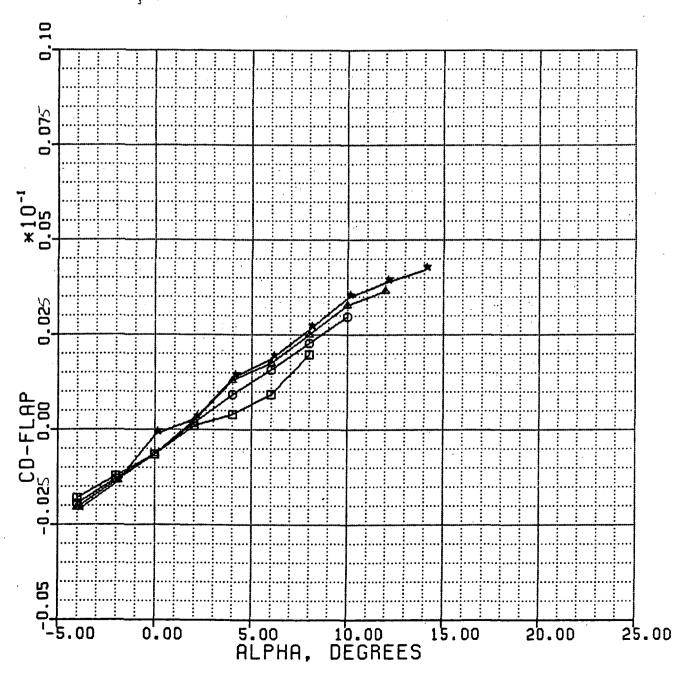
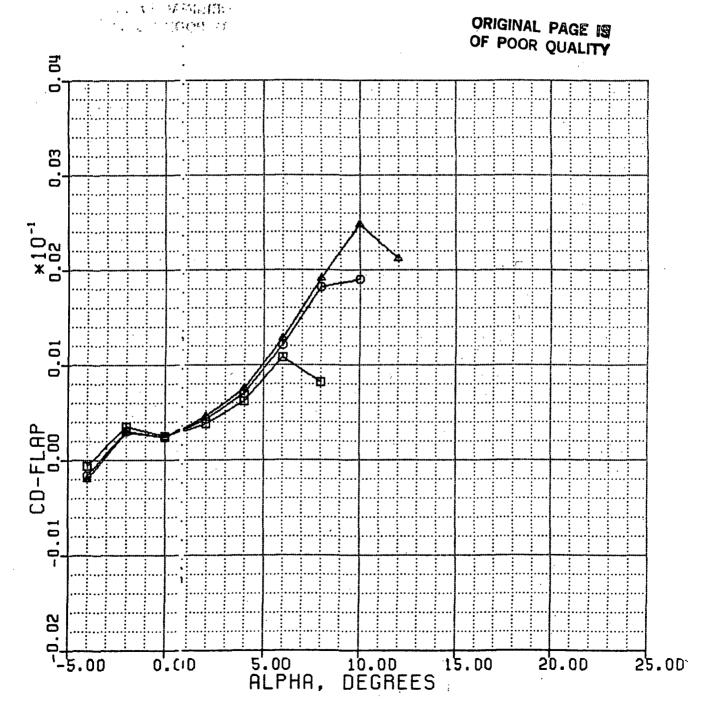


Figure 36(e)



CM-FLAP VS MACH #

7-6-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B PLT = 5.L. M# = .2 TO 1.05

B PLT = 10K M# = .2 TO 1.2

A PLT = 20K M# = .3 TO 1.4

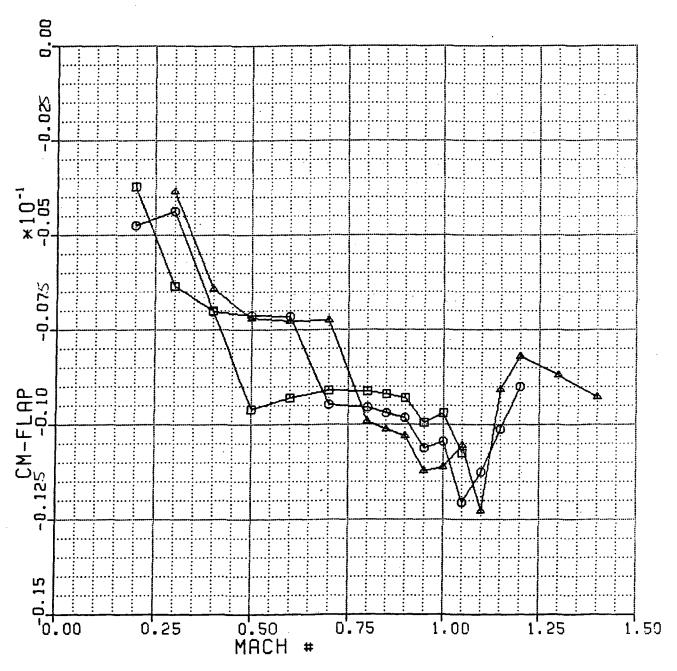


Figure 37(a)

CM-FLAP VS MACH #
7-7-83 X-29A 1-G TRIM NORMAL MODE
XCG = 451.0 WT = 15K

9 ALT = 30K M# = .3 TO 1.5 9 ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

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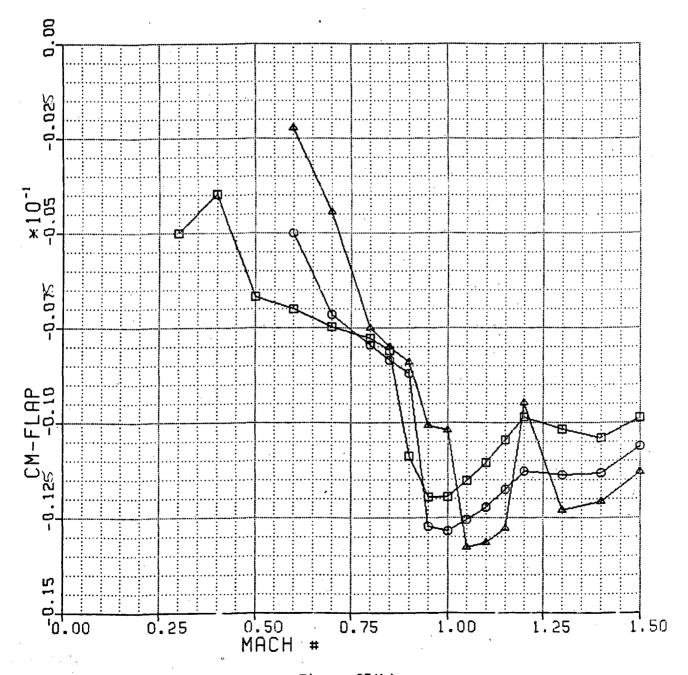


Figure 37(b)

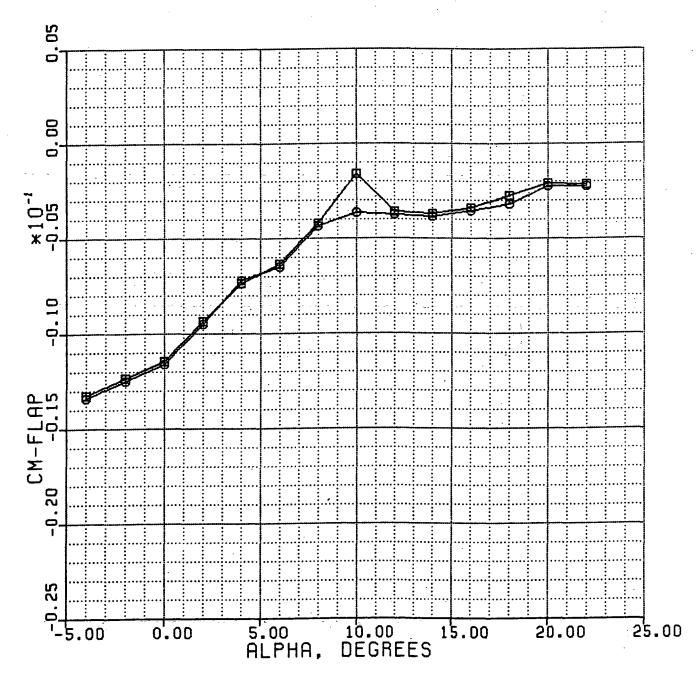
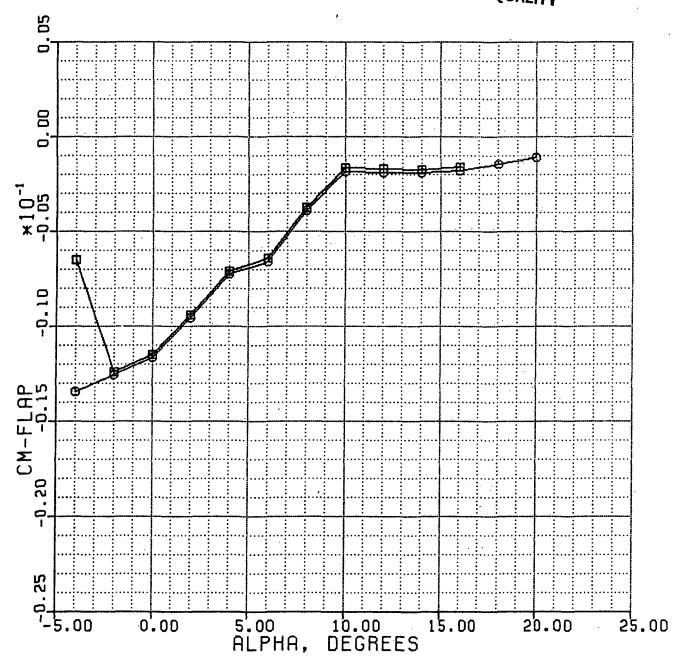


Figure 38(a)



```
CM-FLAP VS ALPHA
  6-30-83 X-29A M# = 0.8 NORMAL MODE
   XCG = 451.0 WT = 15K ALPHA TRIM
                          O TO 10
                     ALP:
           ALT = 10K
                     ALP: -4 TO 12
           ALT = 20K
                     ALP: -4 TO 14
         _ ALP = 30K
         ♣ ALT = 40K
                   ALP: -4 TO 18
         -X ALT = 50K. ALP: -4 TO 22
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 8
 -0.05
CM-FLAP
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Figure 38(c)

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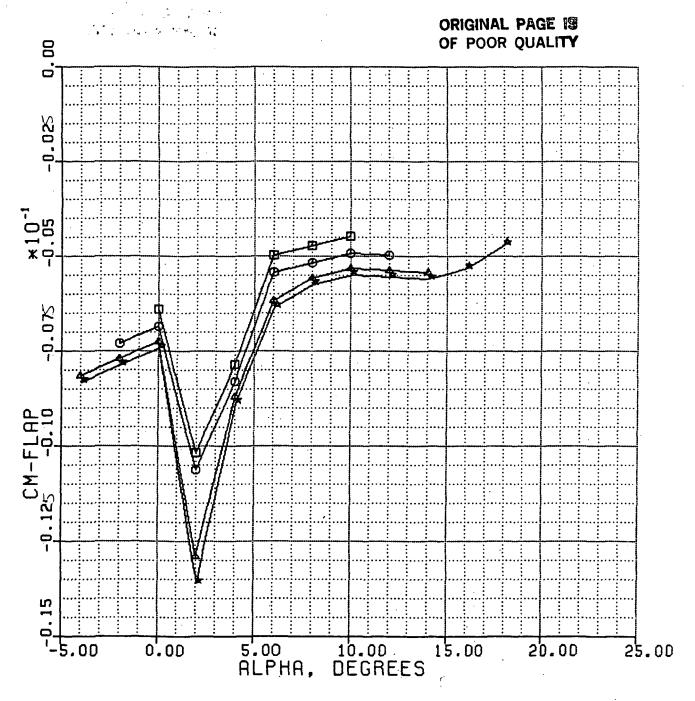
15.00

25.00

5'.00 10.00 ALPHA, DEGREES

0'.00

5.00



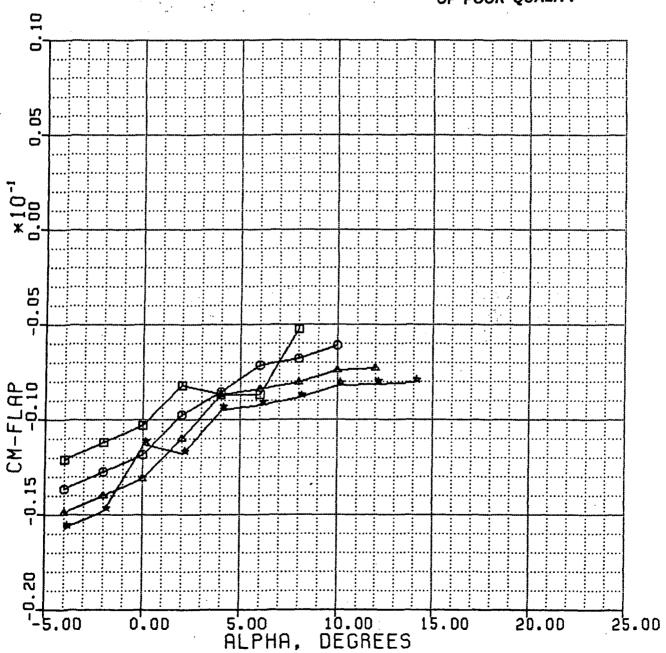


Figure 38(e)

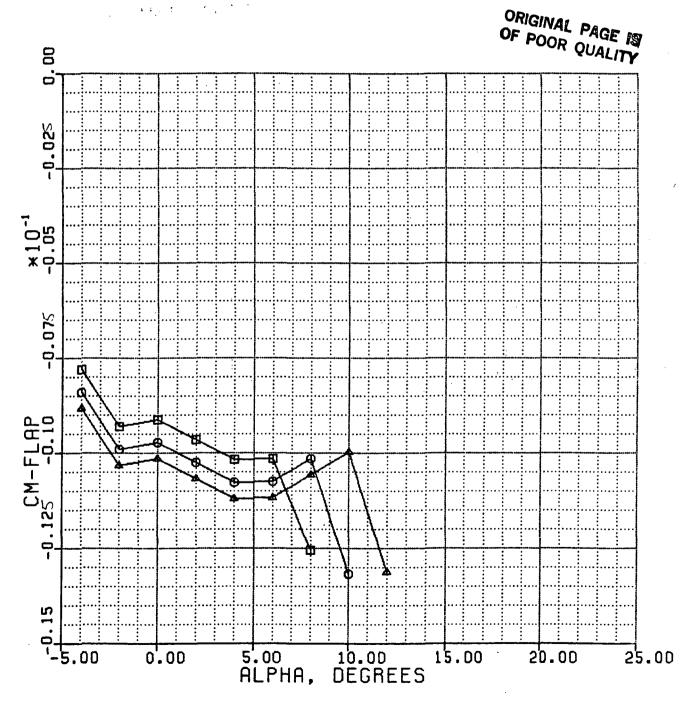


Figure 38(f)

CA-FLAP VS MACH #

7-6-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B ALT = S.L. M# = .2 TO 1.05

B ALT = 10K M# = .2 TO 1.2

ALT = 20K M# = .3 TO 1.4

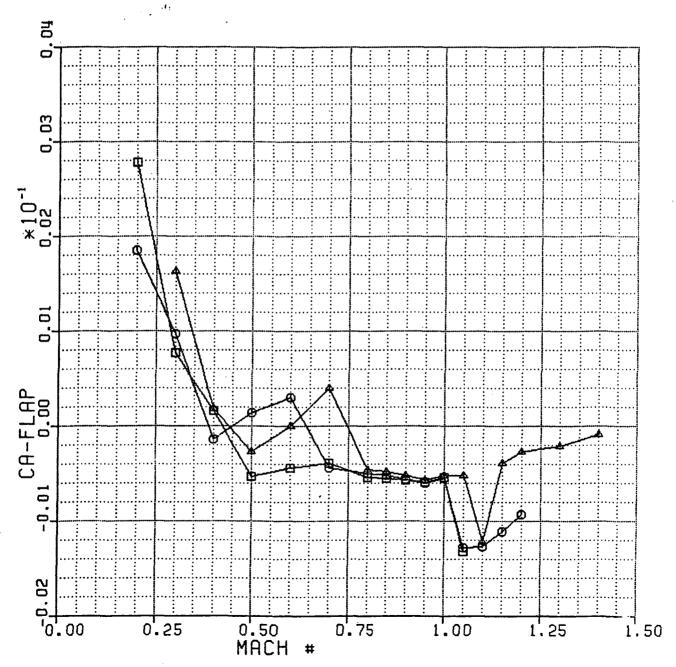
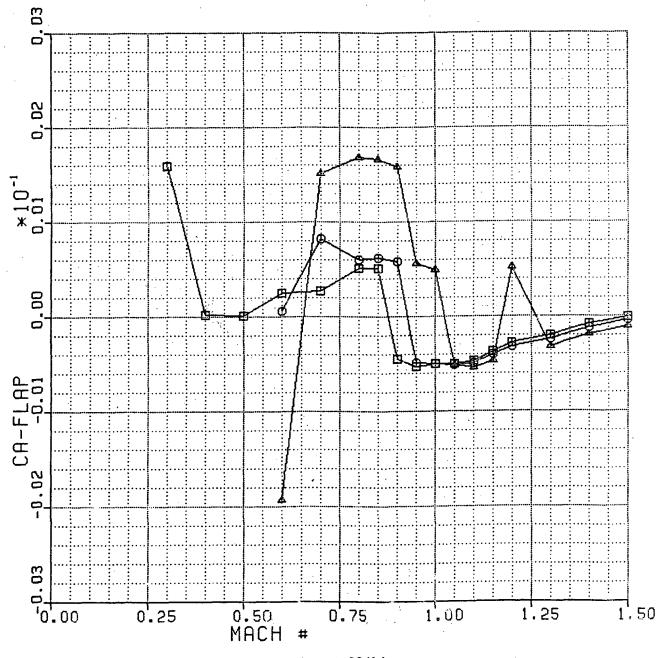


Figure 39(a)



CA-FLAP VS ALPHA

6-16-83 X-29A M# = 0.4 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

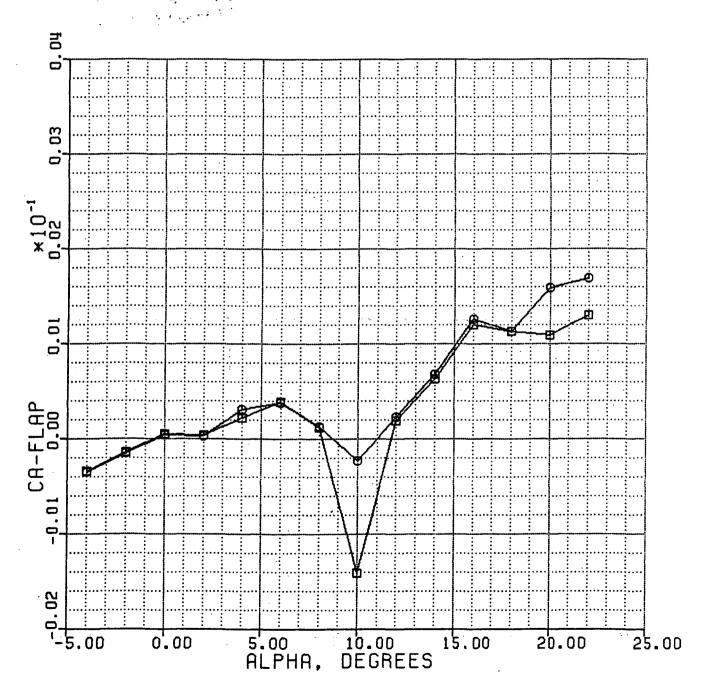


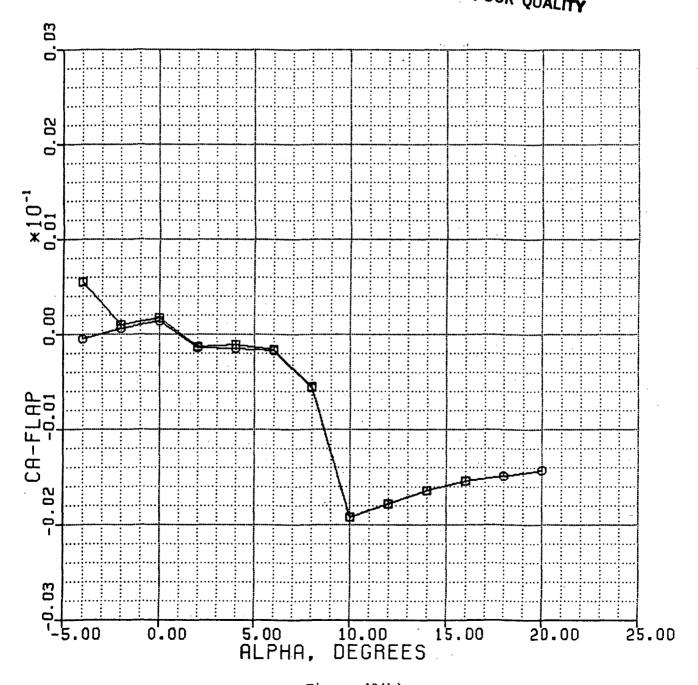
Figure 40(a)

CA-FLAP VS ALPHA 6-17-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

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CA-FLAP VS ALPHA
6-30-83 X^{-}29A M# = 0.8 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM
                  ALP:
                      D TO 10
     -P ALT = 10K
   ______ ALT = 20K
                  ALP: -4 TO 12
                  ALP: -4 TO 14
     _A ALP = 30K
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    ____ * ALT = 40K
                  ALP: -4 TO 18
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     X ALT = 50K
                RLP: -4 TO 22
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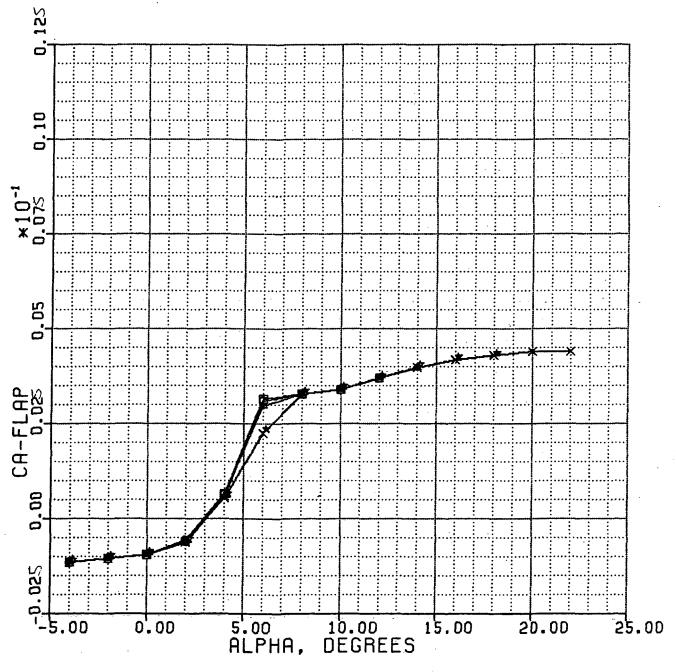


Figure 40(c)

```
CA-FLAP VS ALPHA
7-1-83 X-29A M# = 0.9
                              NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM
 rg --- P3 ALT = 20K
                 ALP:
                      O TO 10
    \overline{RLT} = 30K
                 ALP: -2 TO 12
     __ ALT = 40K
                 ALP: -4 TO 14.
      ¥ ALT = 50K
                 ALP: -4 TO 18
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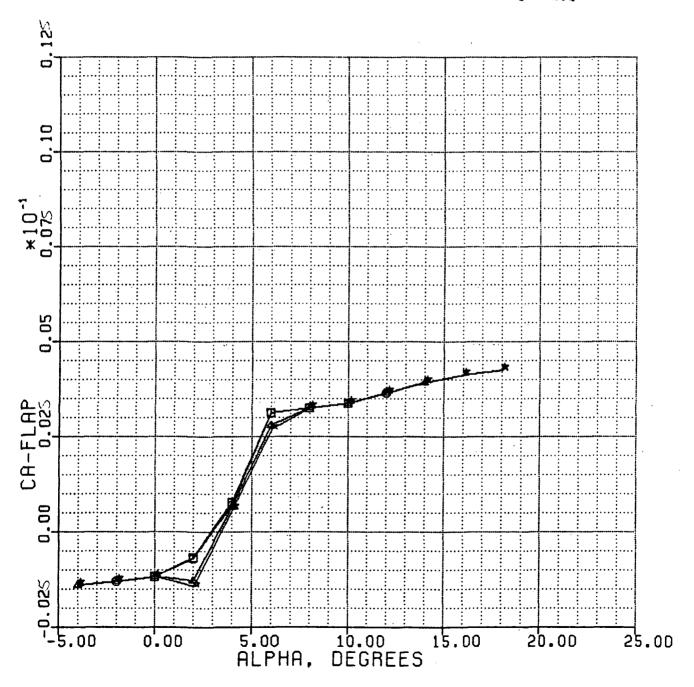
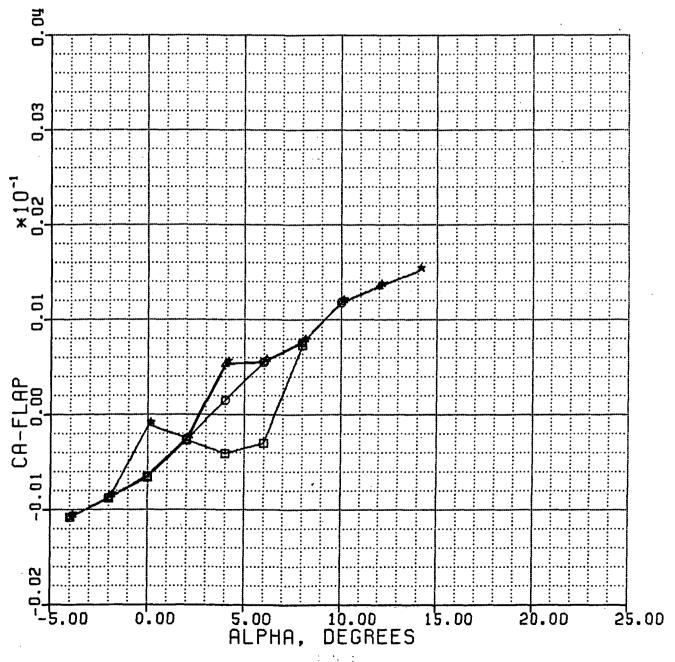
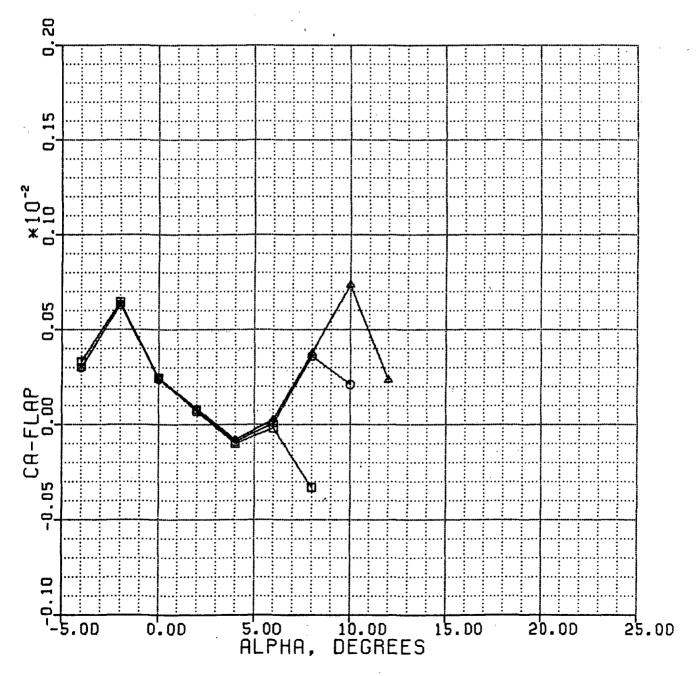


Figure 40(d)



CA-FLAP VS ALPHA
7-1-83 X-29A M# = 1.5 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 30K ALP: -4 TØ 8
O ALT = 40K ALP: -4 TØ 10
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CN-FLAP VS MACH #

7-6-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B RLT = S.L. M# = .2 TO 1.05

B RLT = 10K M# = .2 TO 1.2

A RLT = 20K M# = .3 TO 1.4

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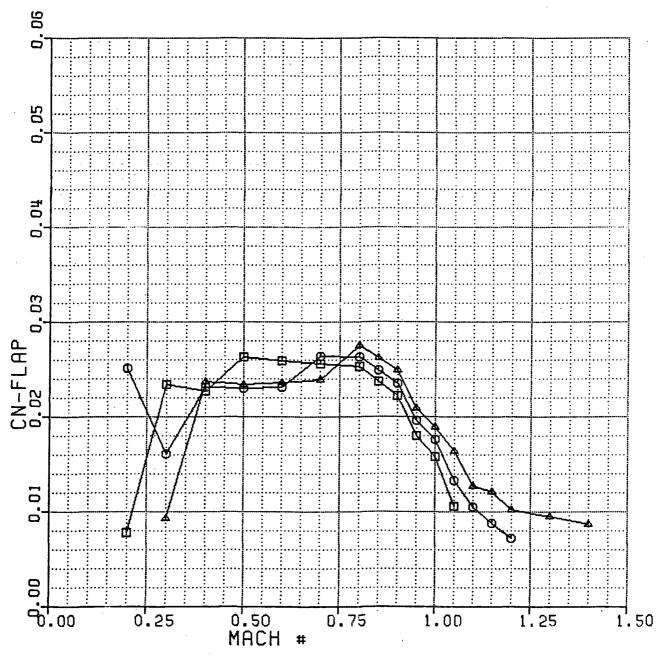


Figure 41(a)

CN-FLAP VS MACH #
7-7-83 X-29A 1-G TRIM NORMAL MODE
XCG = 451.0 WT = 15K

BLT = 30K M# = .3 TO 1.5 BLT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

PROPERTY STATES

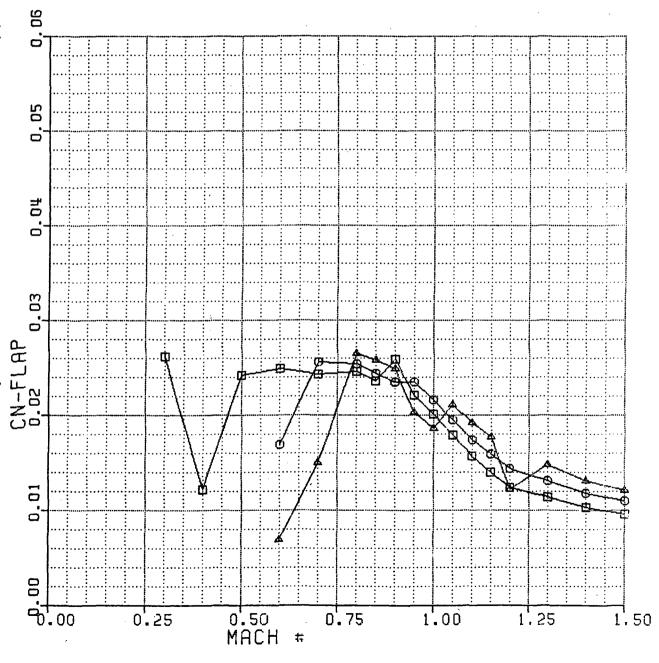


Figure 41(b)

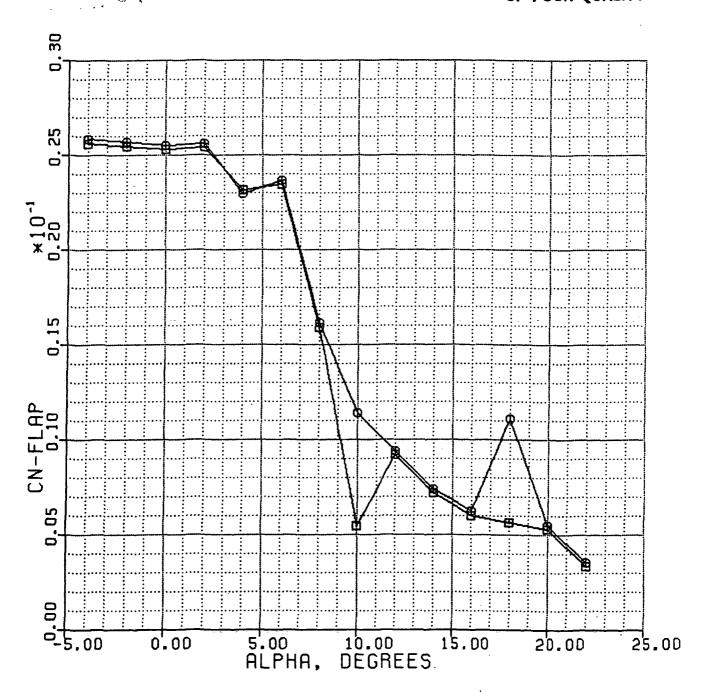


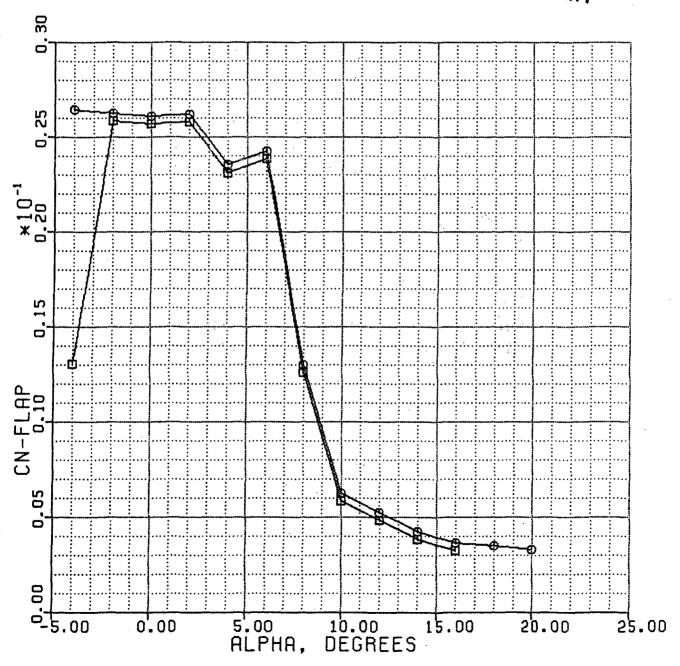
Figure 42(a)

CN-FLAP VS ALPHA
6-17-83 X-29A M# = 0.6 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 10K ALP: -4 TO 16 B ALT = 20K ALP: -4 TO 20

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CN-FLAP VS ALPHA

6-30-83 X-29A M# = 0.8 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 10K ALP: 0 TO 10

C ALT = 20K ALP: -4 TO 12

ALP = 30K ALP: -4 TO 14

*** ALT = 40K ALP: -4 TO 18

X ALT = 50K ALP: -4 TO 22

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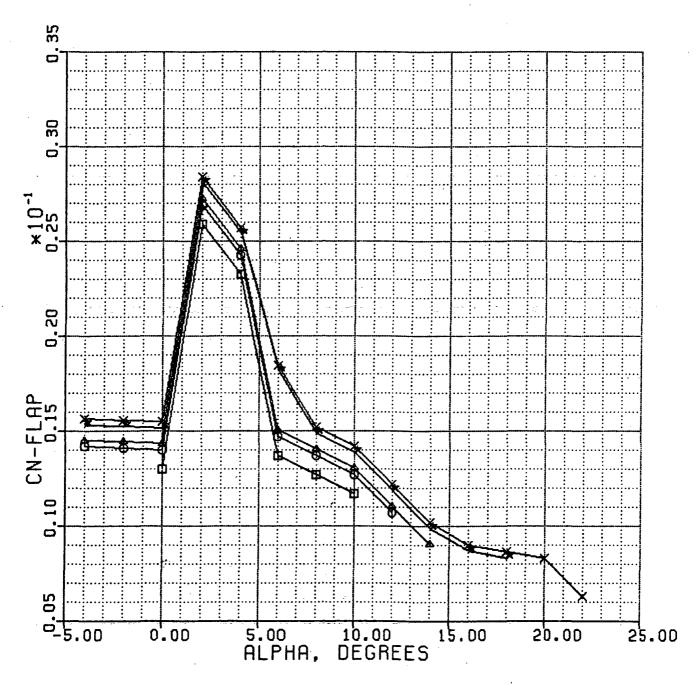


Figure 42(c)

CN-FLAP VS ALPHA
7-1-83 X-29A M# = 0.9 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

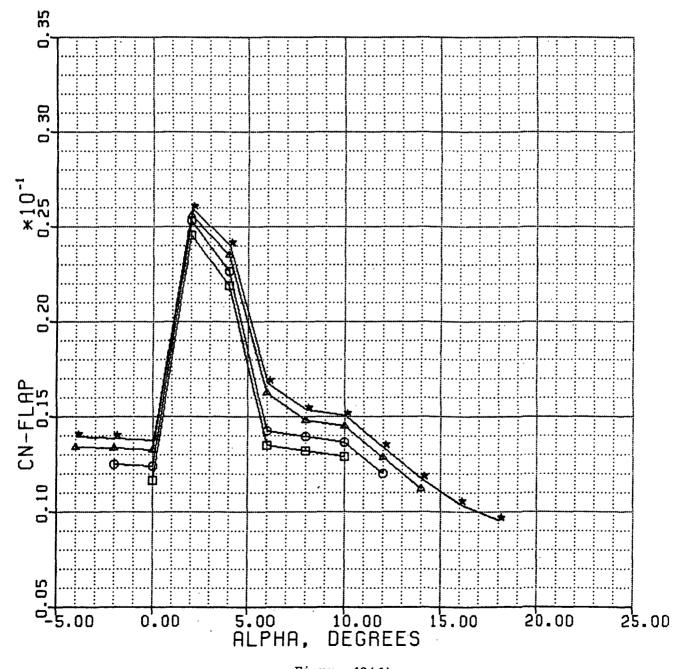
B ALT = 20K ALP: 0 TO 10

C ALT = 30K ALP: -2 TO 12

ALT = 40K ALP: -4 TO 14

ALT = 50K ALP: -4 TO 18

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CN-FLAP VS ALPHA 7-28-83 X-29A M# = NORMAL MODE 1.2 WT = 15KALPHA TRIM XCG = 451.0_m ALT = 20K ALP: -4 TO 8 ALT = 30K ALT = 40K ALP: -4 TO 12 ALP: -4 TO 14 ★ ALT = 50K ORIGINAL PAGE IS

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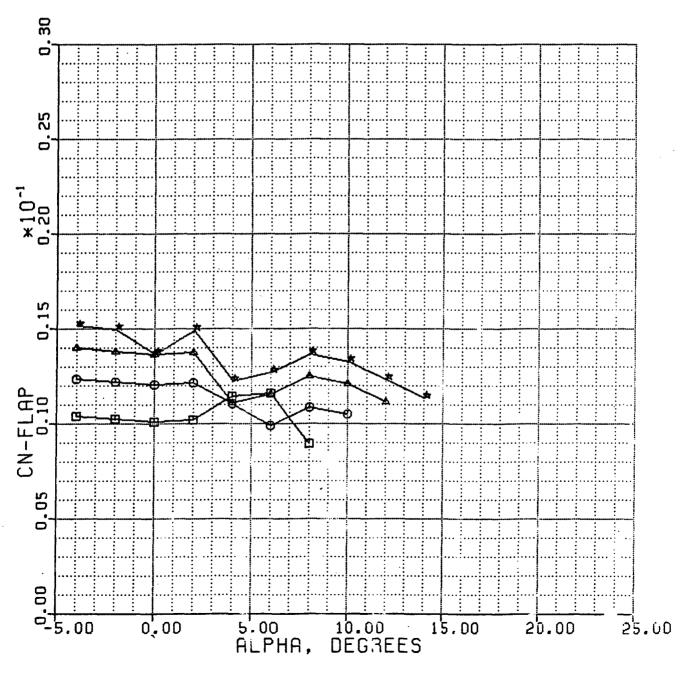


Figure 42(e)

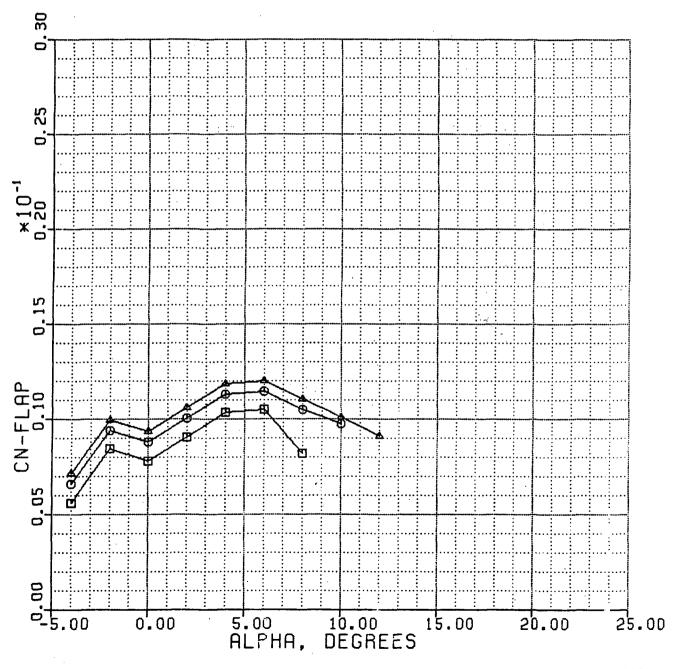
CN-FLAP VS ALPHA7-28-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

PALT = 30K ALP: -4 TO 8

PALT = 40K ALP: -4 TO 10

ALT = 50K ALP: -4 TO 12

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CL-STRAKE VS MACH #

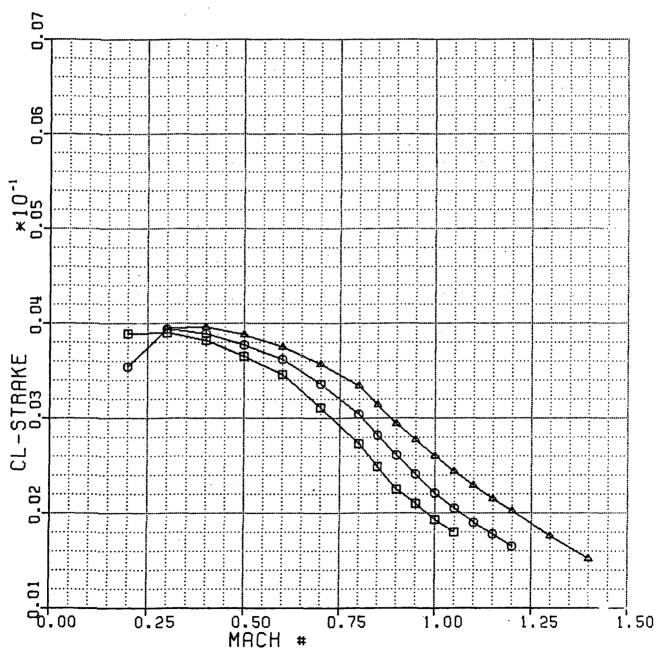
7-6-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B ALT = 5.L. M# = .2 TO 1.05

A ALT = 20K M# = .3 TO 1.4

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CL-STRAKE VS MACH # 7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

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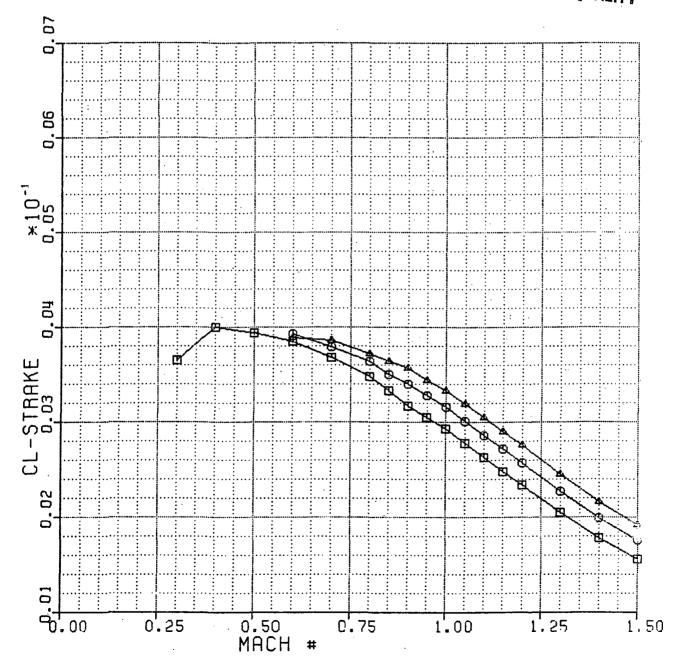




Figure 43(b)

CL-STRAKE VS ALPHA 6-16-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM B ALT = S.L. ALP: -4 TØ 22 C ALT = 10K ALP: -4 TØ 22

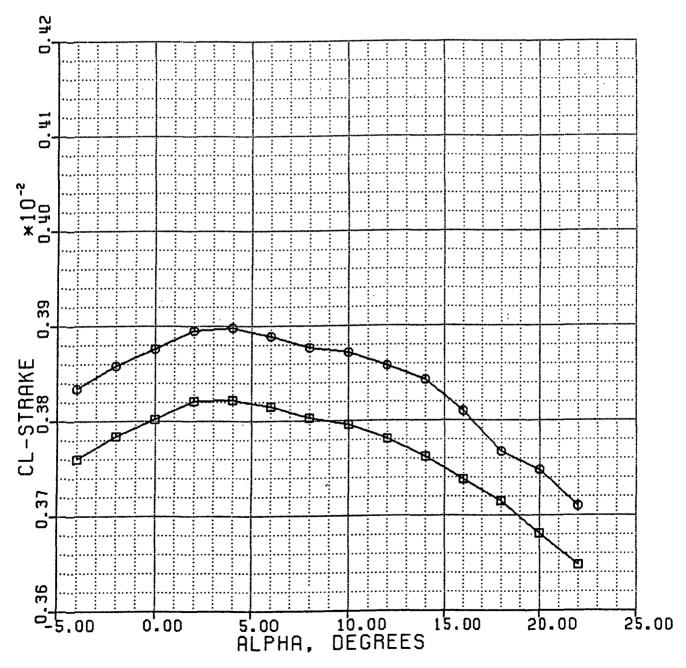
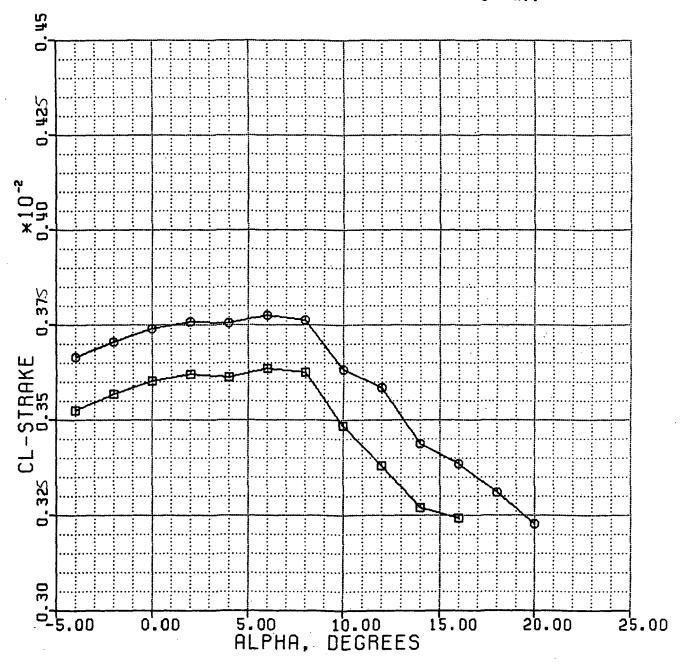
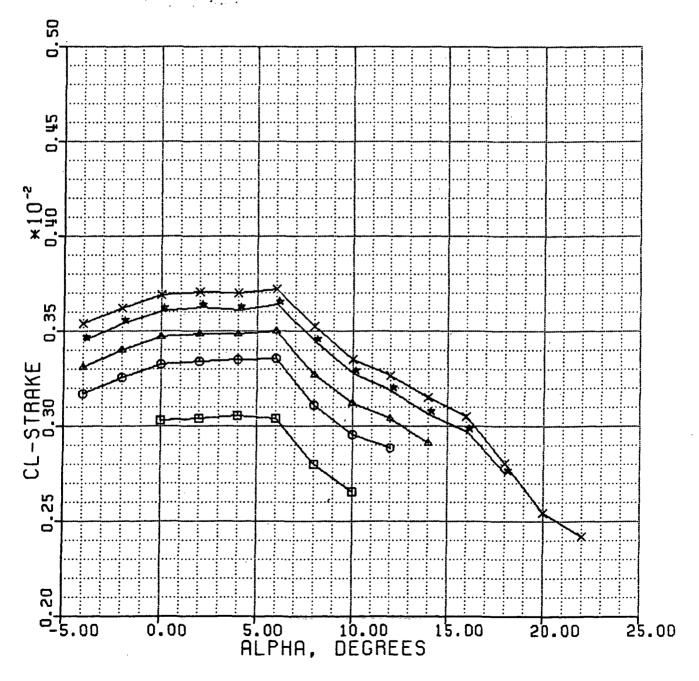


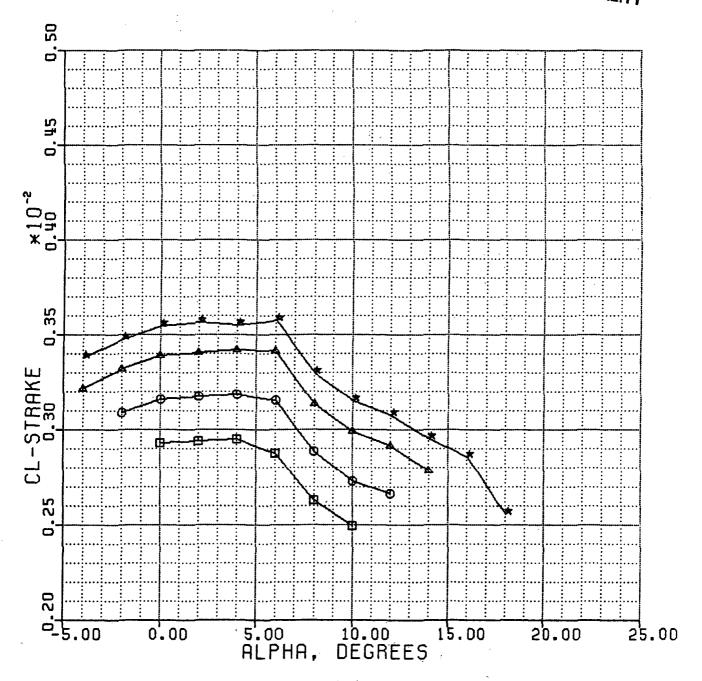
Figure 44(a)



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CL-STRAKE VS ALPHA
6-30-83 X-29A M# = 0.8 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM
     _ ALT = 10K
                 ALP:
                     0 TO 10
       ALT = 20K
                 ALP: -4 TO 12
       ALP = 30K
                 ALP: -4 TO 14
      _★ ALT = 40K
                 ALP: -4 TO 18
                               ORIGINAL PAGE 18
     → ALT = 50K
                 ALP: -4 TO 22
                               OF POOR QUALITY
```



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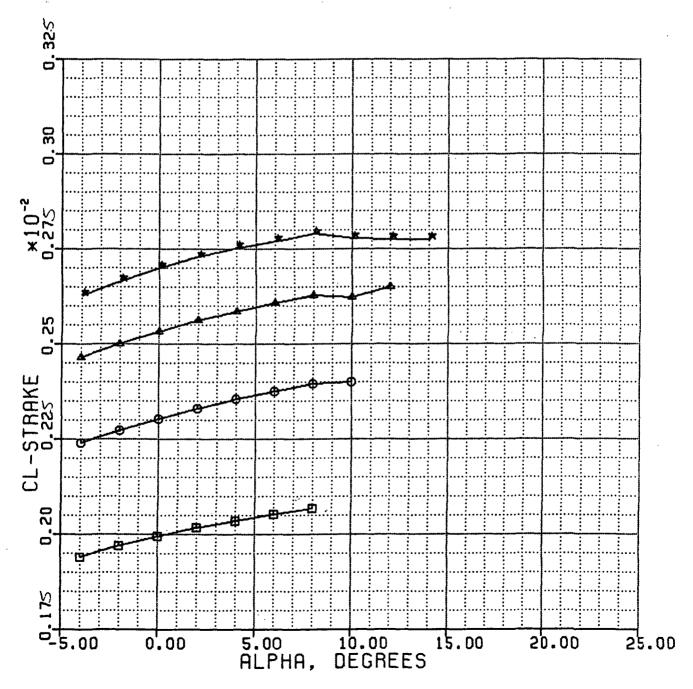
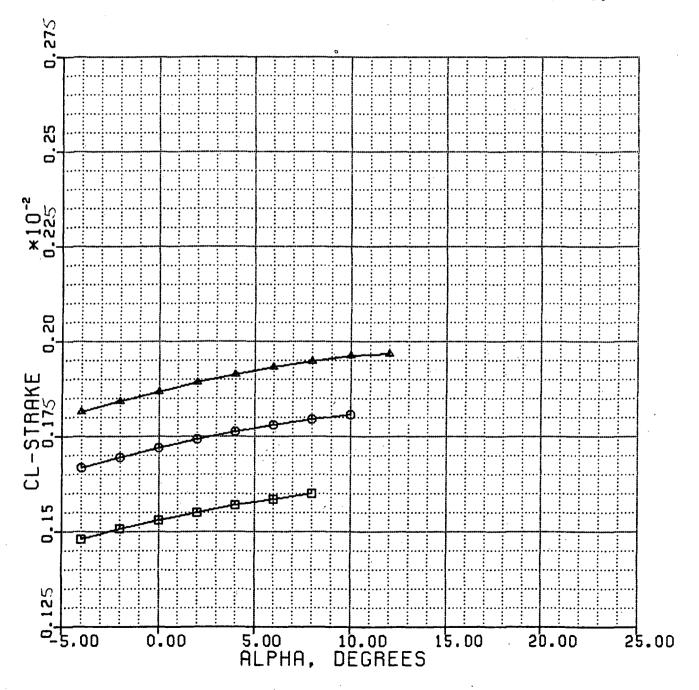


Figure 44(e)



```
CD-STRAKE VS MACH #

7-6-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

BRIT = S.L. M# = .2 TO 1.05

BRIT = 10K M# = .2 TO 1.2

ARIT = 20K M# = .3 TO 1.4

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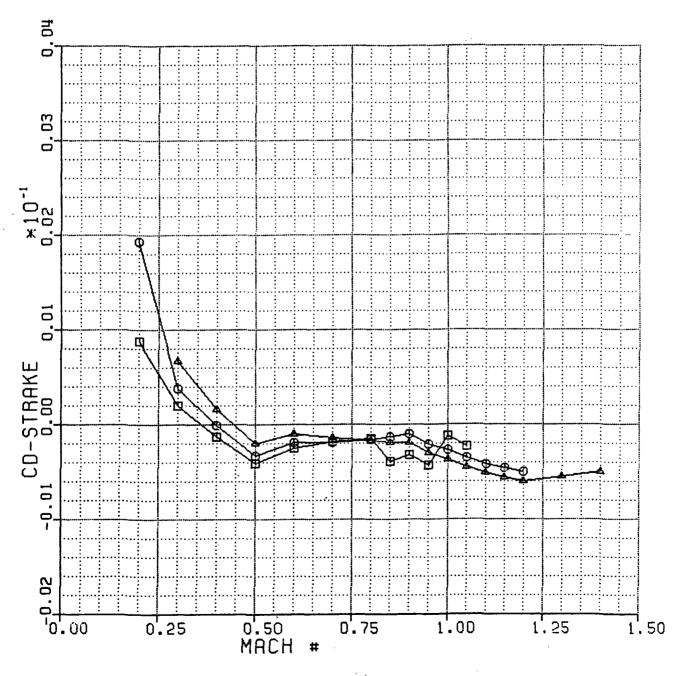


Figure 45(a)

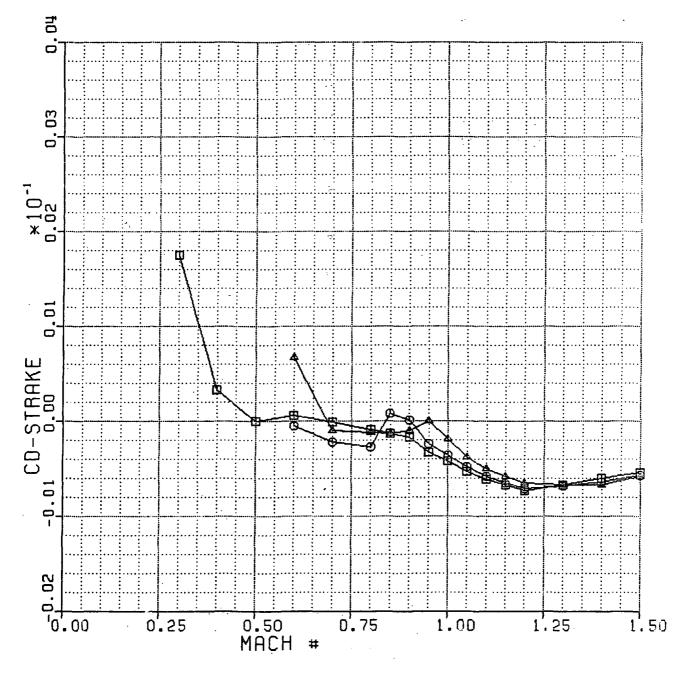


Figure 45(b)

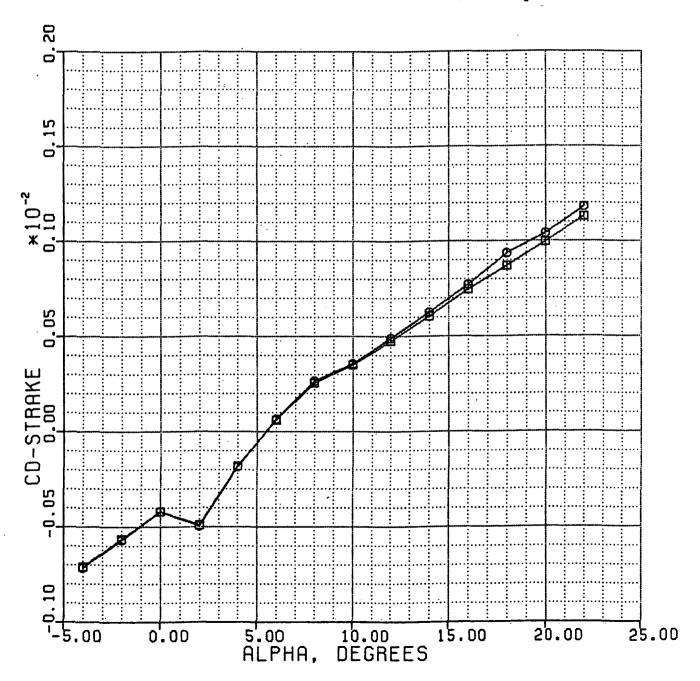
CD-STRAKE VS ALPHA

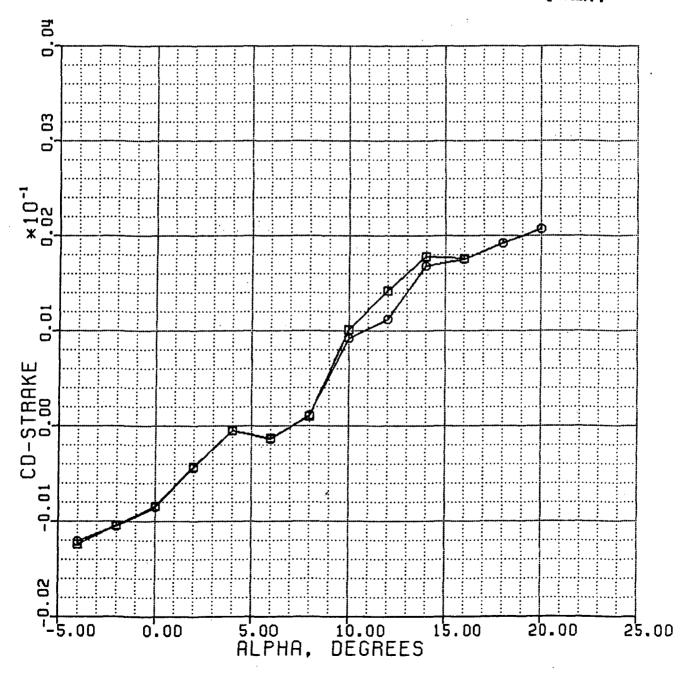
6-16-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = S.L. ALP: -4 TO 22

P ALT = 10K ALP: -4 TO 22

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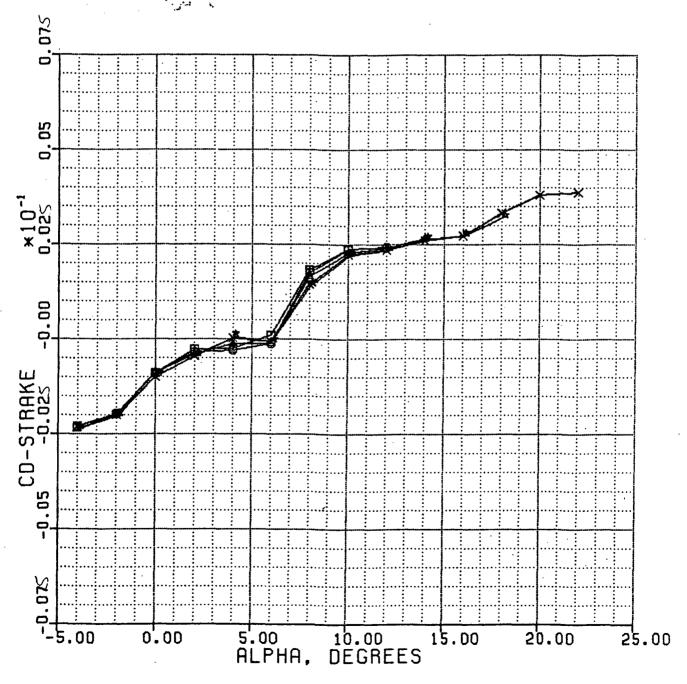
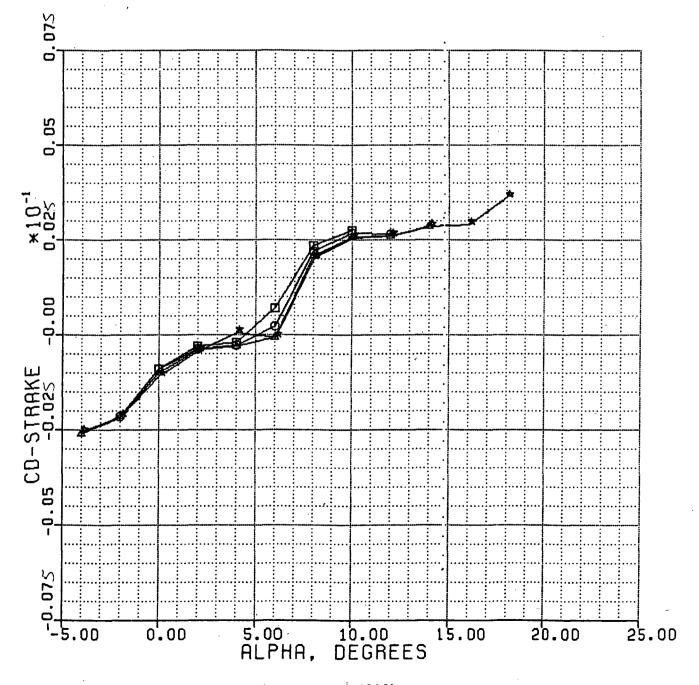


Figure 46(c)



CD-STRAKE VS ALPHA 7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM ALP: -4 TO 8 _m ALT = 20K ALT = 30KALP: -4 TO 10 ALT = 40K ALP: -4 TO 12 ★ ALT = 50K ALP: -4 TO 14

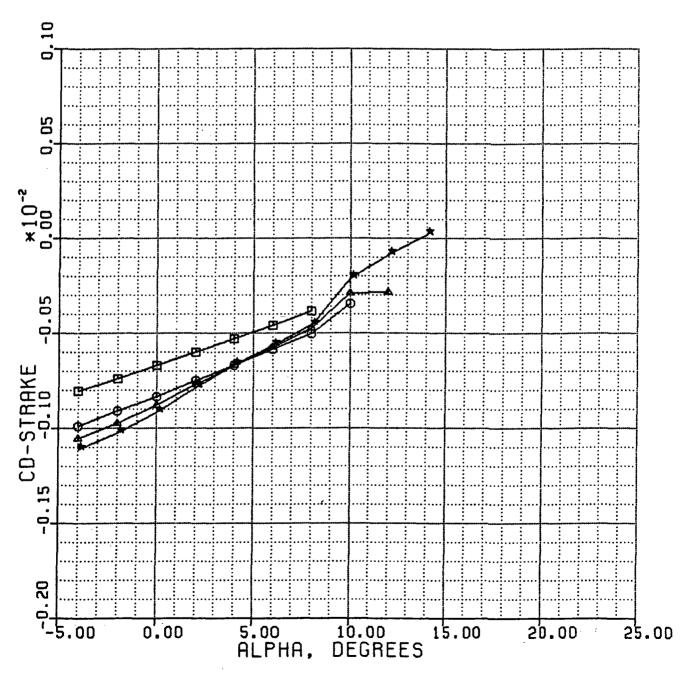


Figure 46(e)

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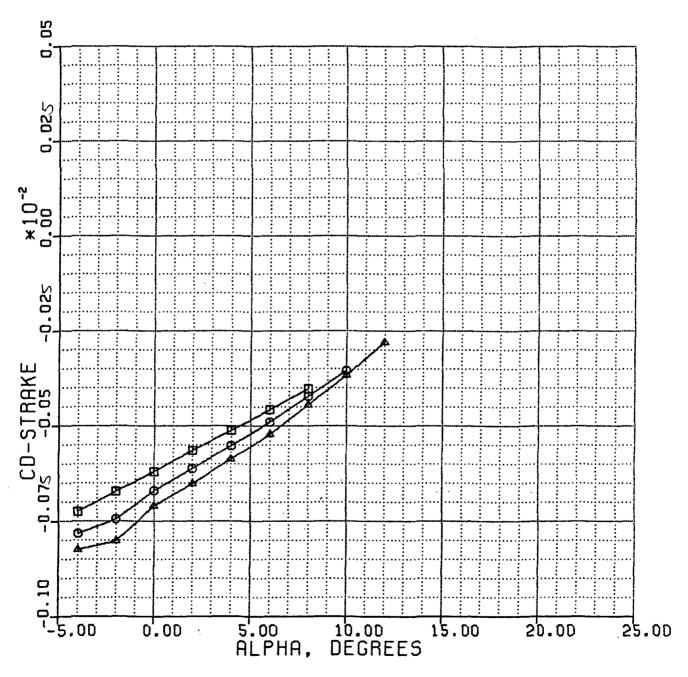


Figure 46(f)

CM-STRAKE VS MACH # 7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = S.L. M# = .2 TO 1.05 P ALT = 10K M# = .2 TO 1.2 ALT = 20K M# = .3 TO 1.4

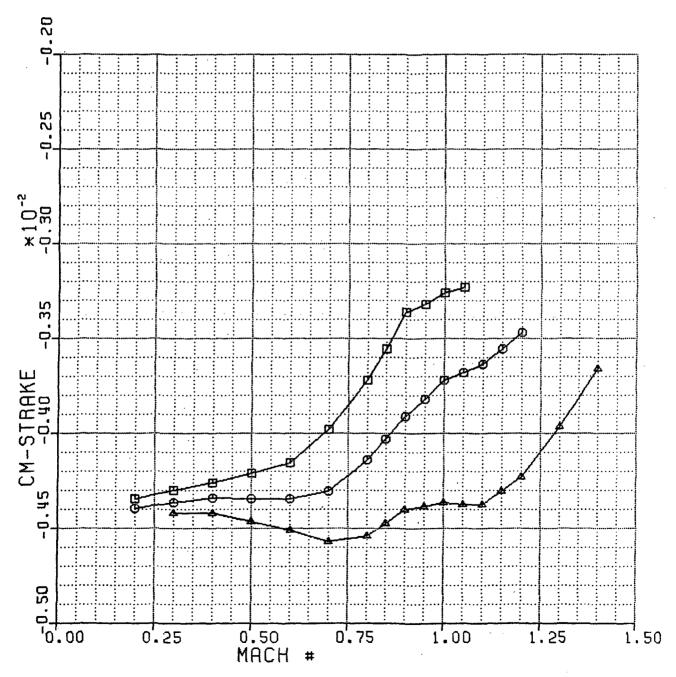


Figure 47(a)

CM-STRAKE VS MACH #
7-7-83 X-29A 1-G TRIM NORMAL MODE
XCG = 451.0 WT = 15K

PRIT = 30K M# = .3 TO 1.5
PRIT = 40K M# = .6 TO 1.5
PRIT = 50K M# = .6 TO 1.5
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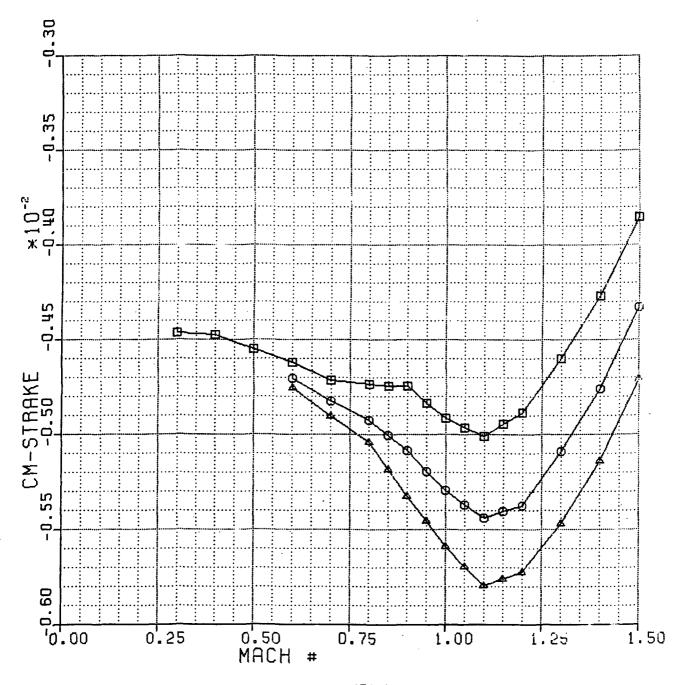


Figure 47(b)

CM-STRAKE VS ALPHA 7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 5.L. ALP: -4 TO 22 0 ALT = 10K ALP: -4 TO 22

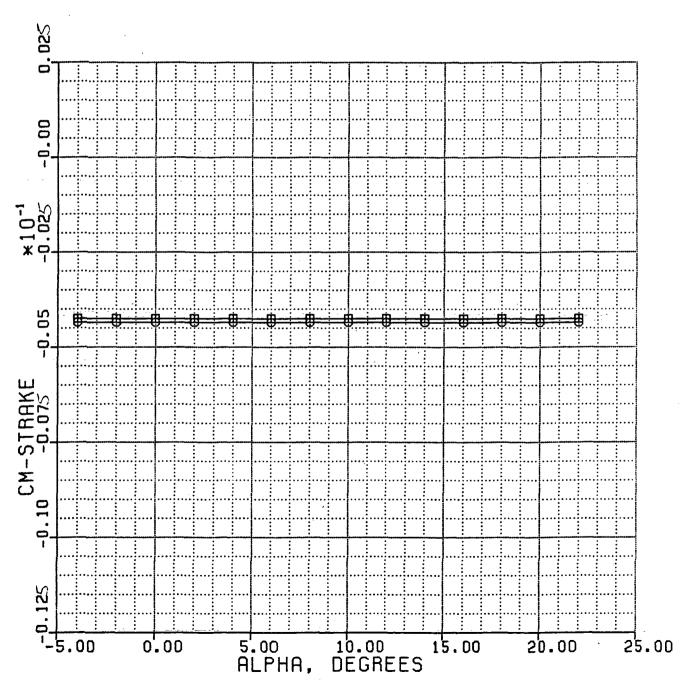
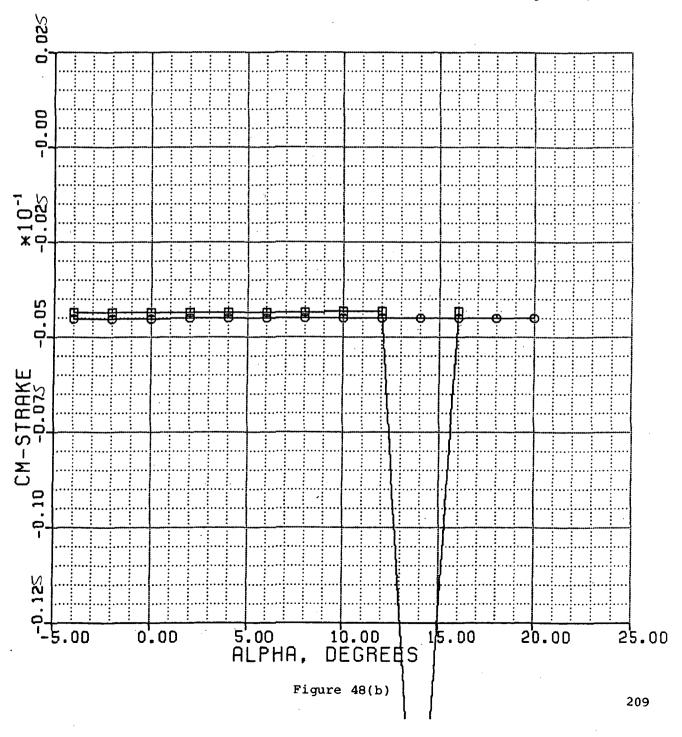


Figure 48(a)

0 ALT = 10K ALP: -4 TO 16 0 ALT = 20K ALP: -4 TO 20



CM-STRAKE VS ALPHA 6-30-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM _m ALT = 10K ALP: O TO 10 ALP: -4 TO 12 - ALT = 20K ALP = 30KALP: -4 TO 14 ALP: -4 TO 18 _★ ALT = 4DK ORIGINAL PAGE 18 → ALT = 50K ALP: -4 TO 22 OF POOR QUALITY

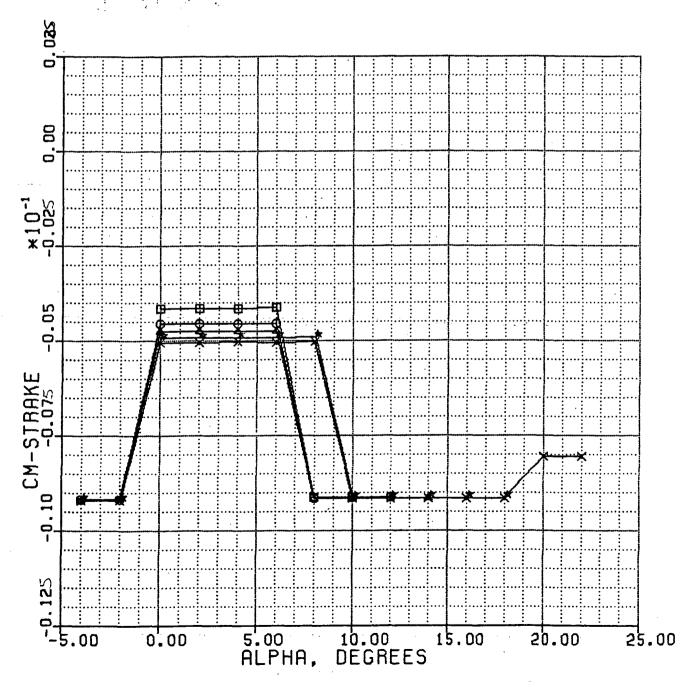


Figure 48(c)

CM-STRAKE VS ALPHA
7-1-83 X-29A M# = 0.9 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

PALT = 20K ALP: 0 TØ 10
O ALT = 30K ALP: -2 TØ 12
ALT = 40K ALP: -4 TØ 14
ALT = 50K ALP: -4 TØ 18

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OF POOR QUALITY

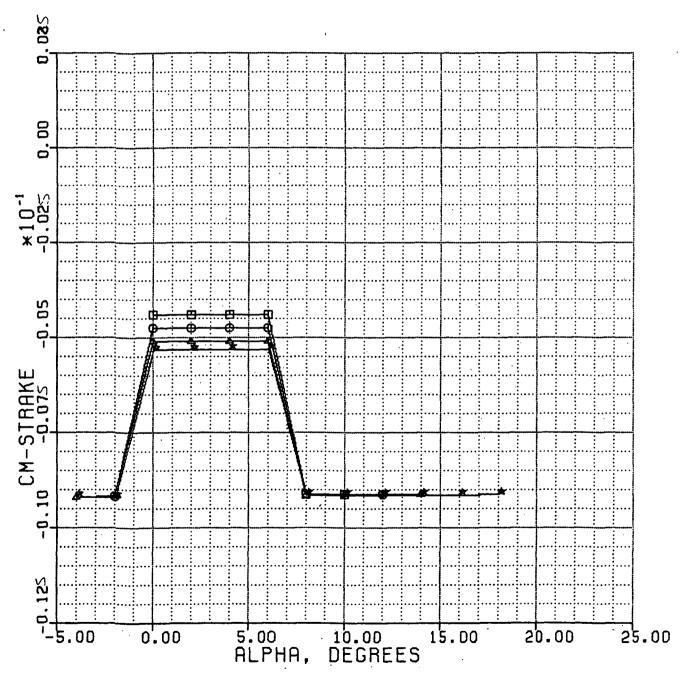


Figure 48(d)

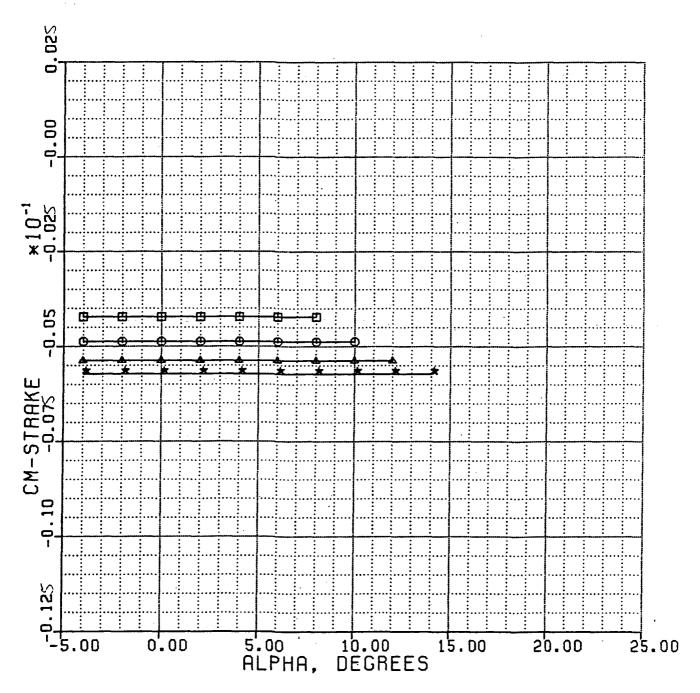


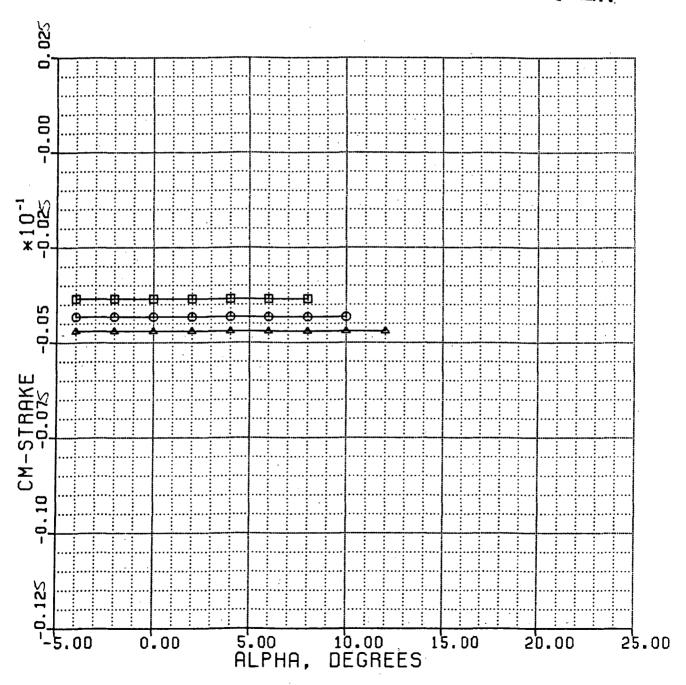
Figure 48(e)

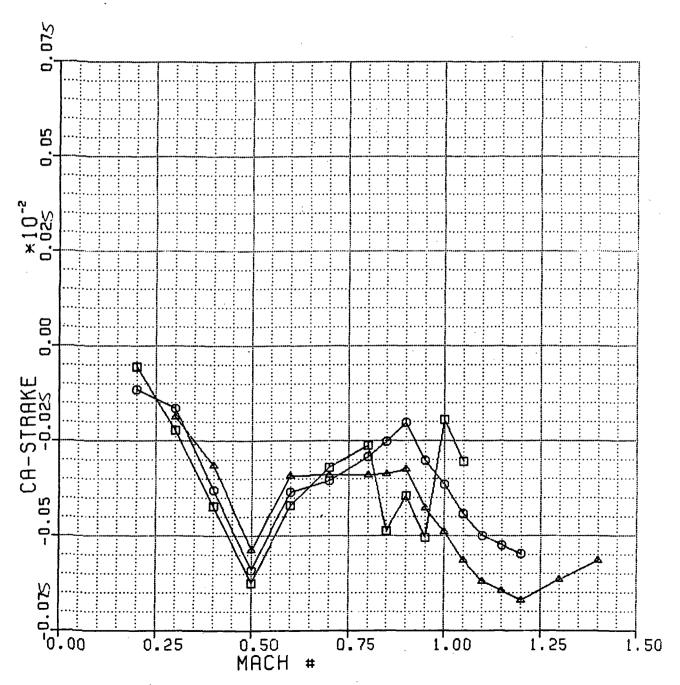
CM-STRAKE VS ALPHA
7-27-83 X-29A M# = 1.5 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

D P ALT = 30K ALP: -4 TO 8

O P ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12





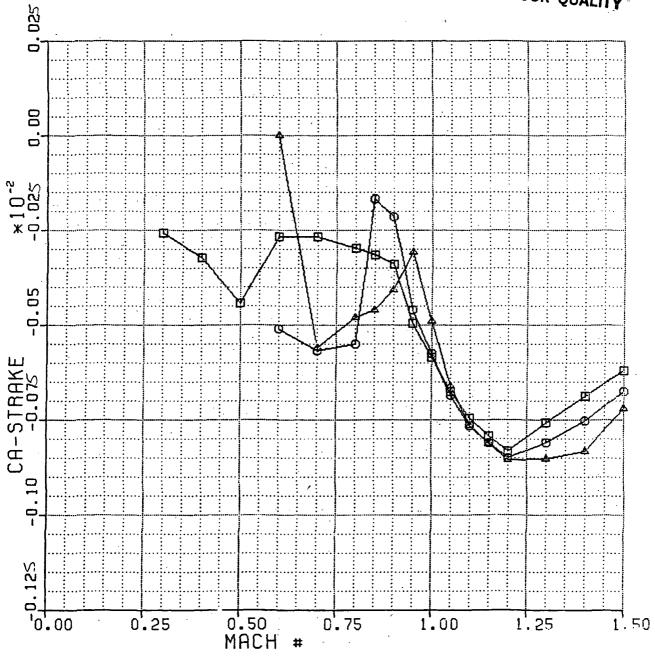


Figure 49(b)

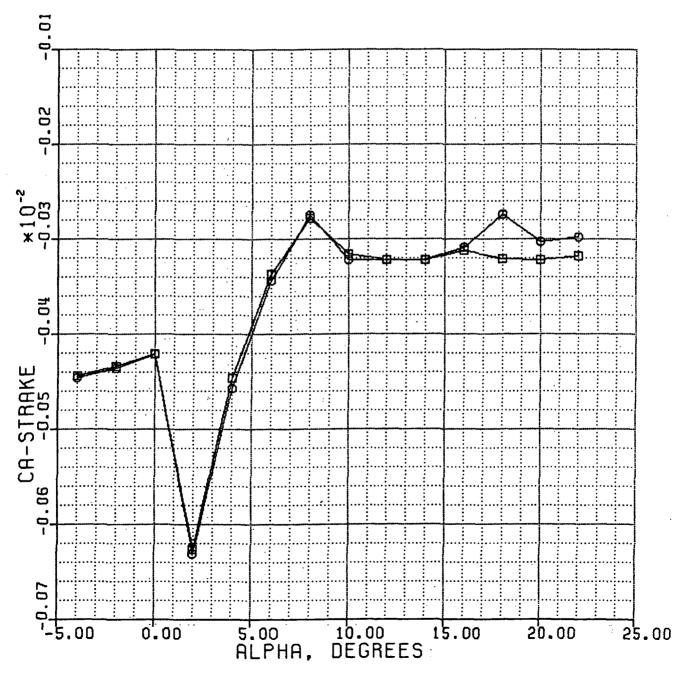
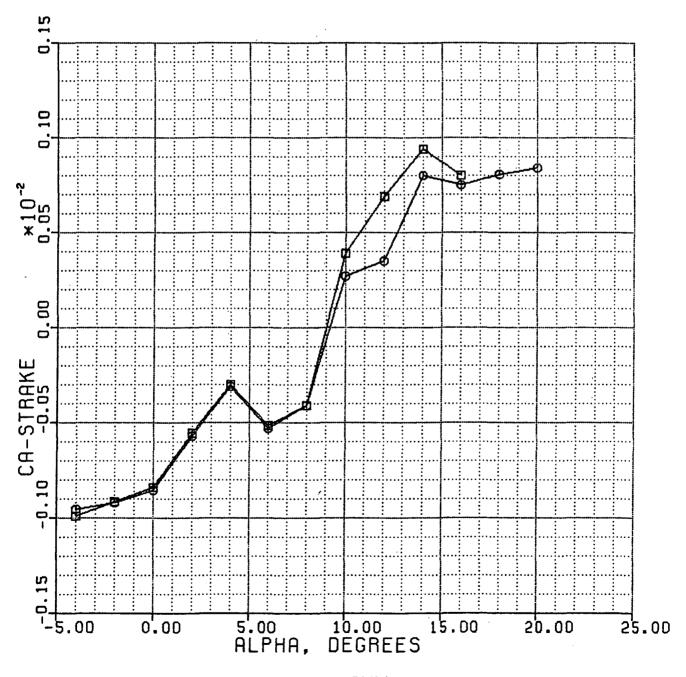


Figure 50(a)

CA-STRAKE VS ALPHA 6-17-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

O O ALT = 10K ALP: -4 TO 16
O O ALT = 20K ALP: -4 TO 20



```
CA-STRAKE VS ALPHA

6-30-83 X-29A M# = 0.8 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 10K ALP: 0 TO 10

O ALT = 20K ALP: -4 TO 12

ALP = 30K ALP: -4 TO 14

ALP = 30K ALP: -4 TO 18

ALT = 40K ALP: -4 TO 18

ALT = 50K ALP: -4 TO 22
```

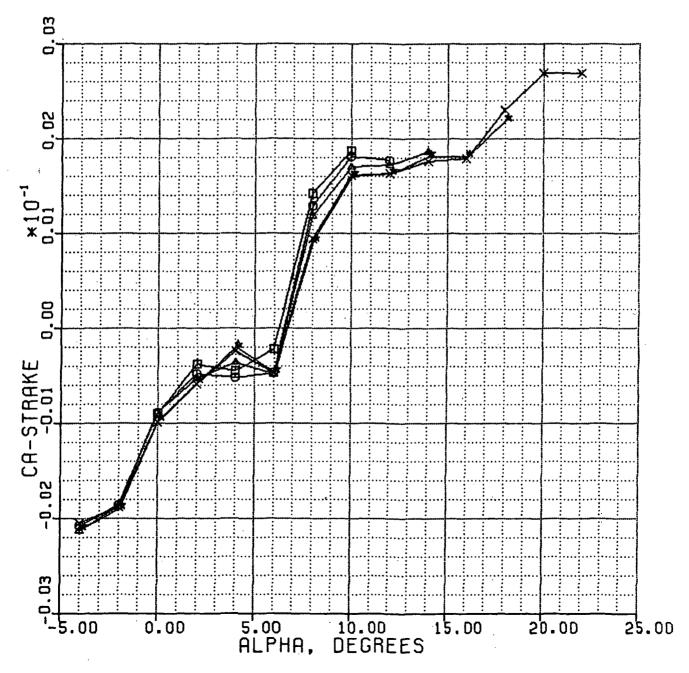
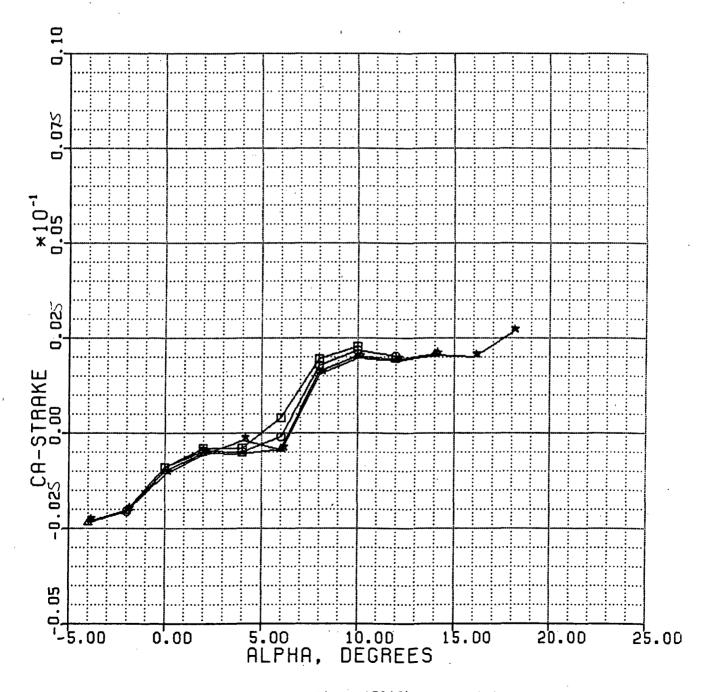


Figure 50(c)



CA-STRAKE VS ALPHA

7-27-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

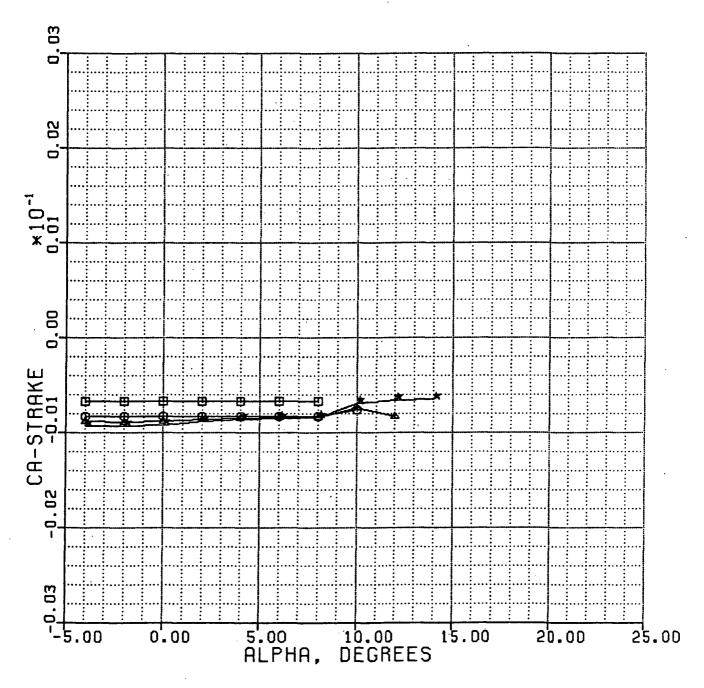


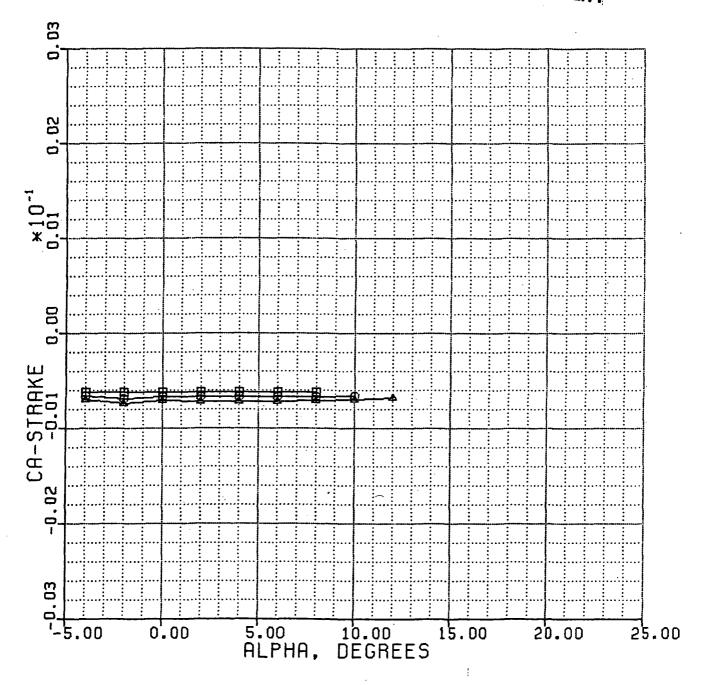
Figure 50(e)

CA-STRAKE VS ALPHA
7-27-83 X-29A M# = 1.5 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM

BLT = 30K ALP: -4 TO 8

O ALT = 40K ALP: -4 TO 10

ALT = 50K ALP: -4 TO 12



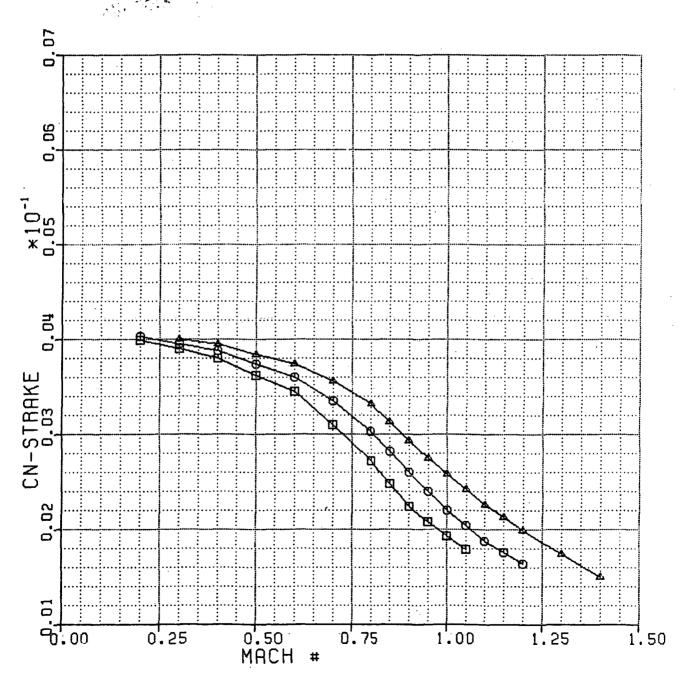


Figure 51(a)

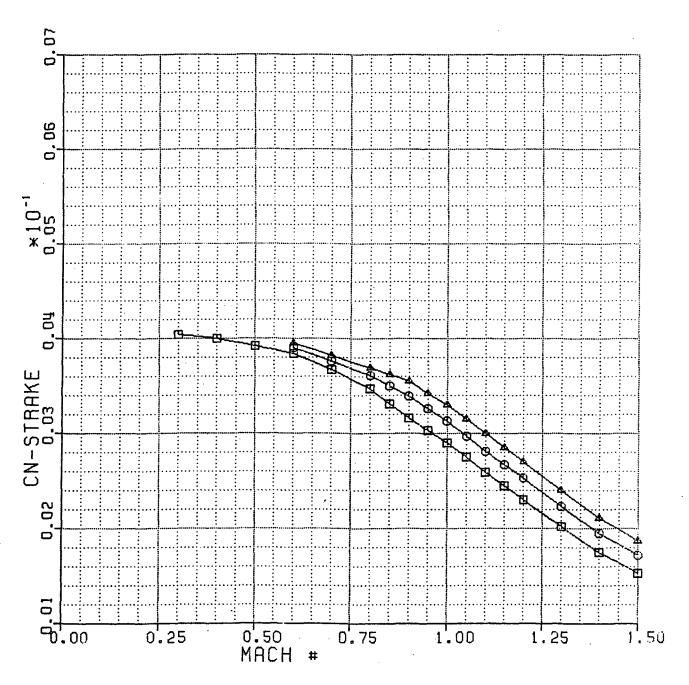


Figure 51(b)

CN-STRAKE VS ALPHA

7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

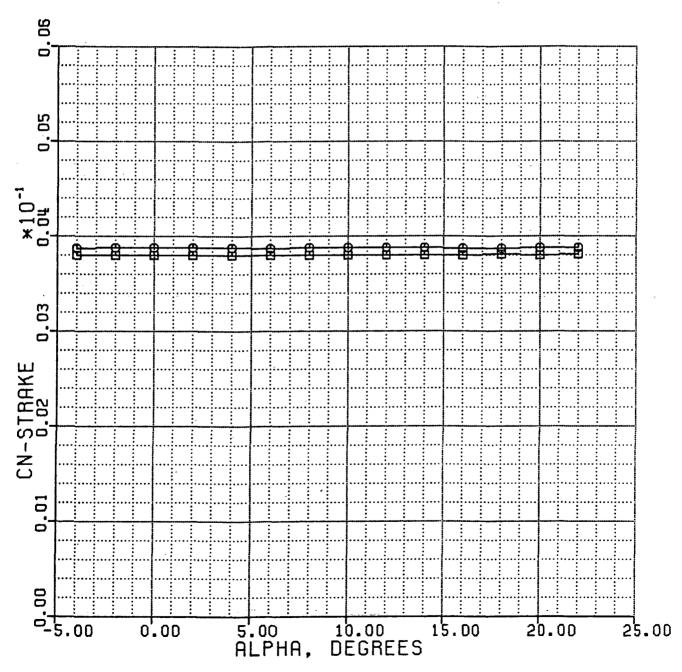


Figure 52(a)

CN-STRAKE VS ALPHA 7-26-83 X-29A M# = 0.6 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 10K ALP: -4 TO 16

B ALT = 20K ALP: -4 TO 20

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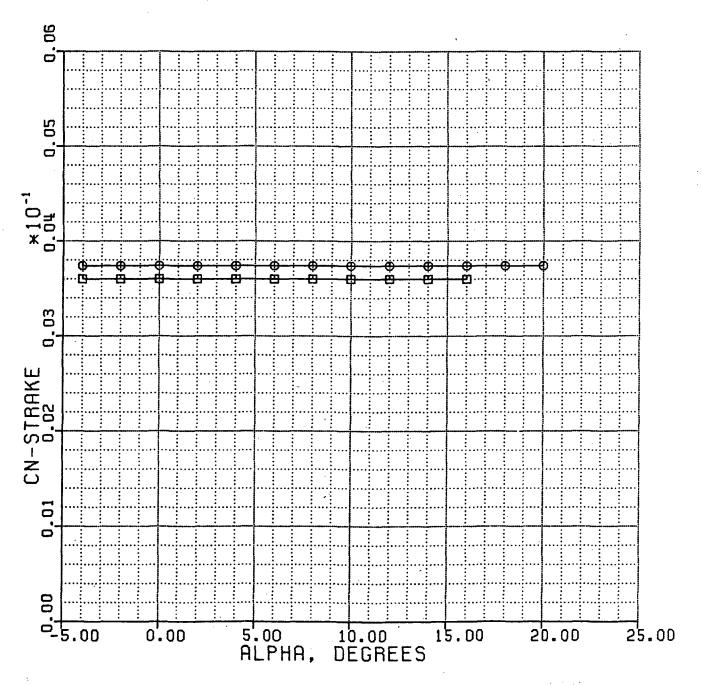


Figure 52(b)

CN-STRAKE VS ALPHA 6-30-83 X-29A M# = 0.8NORMAL MODE XCG = 451.0 WT = 15KALPHA TRIM ALT = 10K ALP: 0 TO 10 -4 TO 12 ALT = 20KORIGINAL PAGE IS ALP = 30K-4 TO 14 ALP: OF POOR QUALITY _★ ALT = 40K / -4 TO 18 ALP: ALT = 50K ALP: -4 TO 22

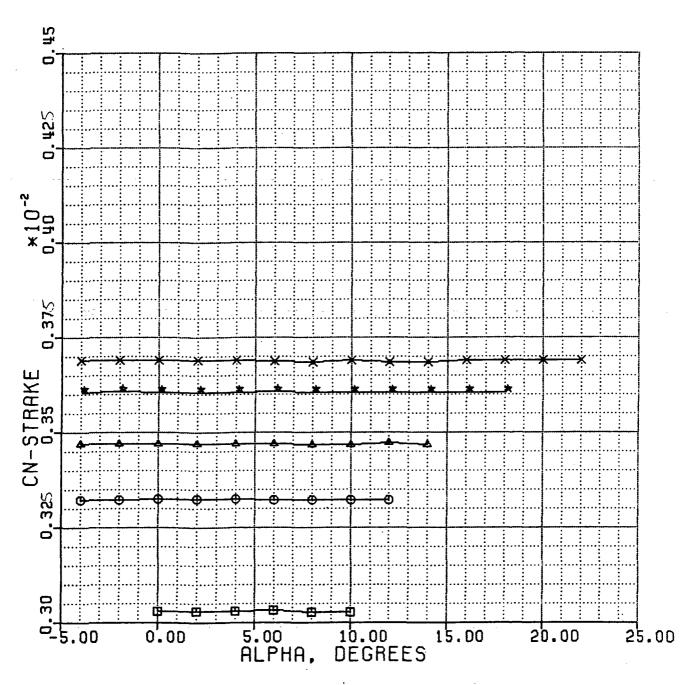
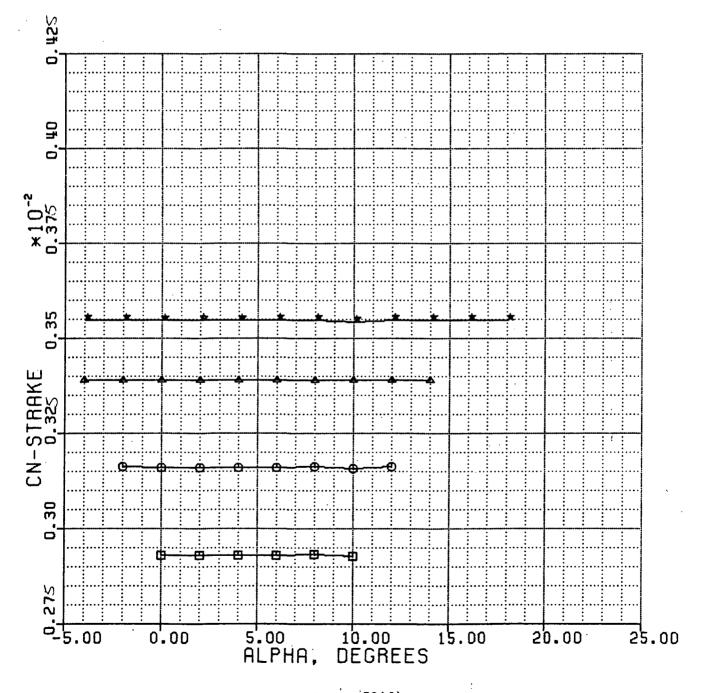
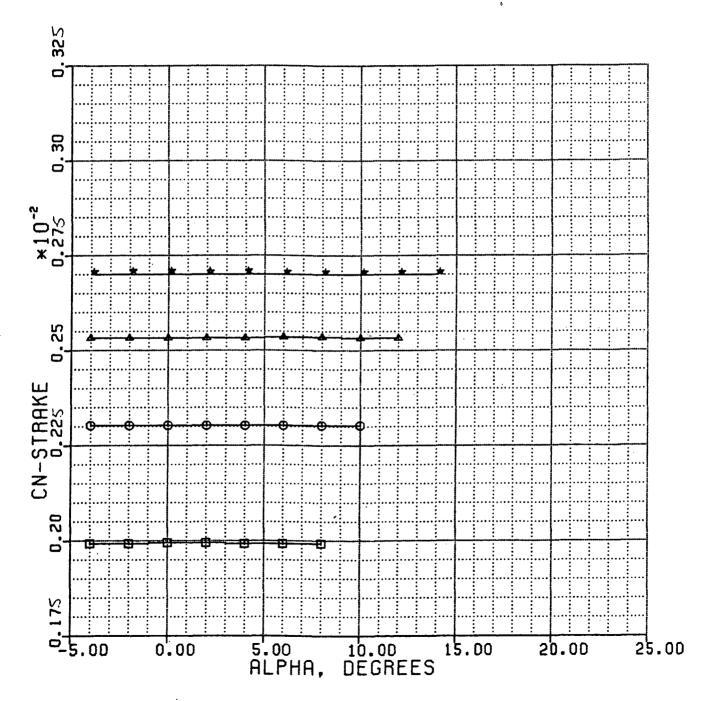


Figure 52(c)

CN-STRAKE VS ALPHA 7-1-83 X-29A M# = 0.9NORMAL MODE ALPHA TRIM XCG = 451.0 WT = 15K-M ALT = 20K ALP: O TO 10 ALT = 30K ALP: ALT = 40K ALP: -4 TO 14 ORIGINAL PAGE IS ★ ALT = 50K ALP: -4 TO 18 OF POOR QUALITY



CN-STRAKE VS ALPHA 7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15KALPHA TRIM _____ ALT = 20K ALP: -4 TO 8 -A) ALT = 30K ALP: -4 TO 10 ALT = 40KALP: -4 TO 12 ORIGINAL PAGE 19 ★ ALT = 50K ALP: -4 TO 14 OF POOR QUALITY 1 5 A 18



CN-STRAKE VS ALPHA

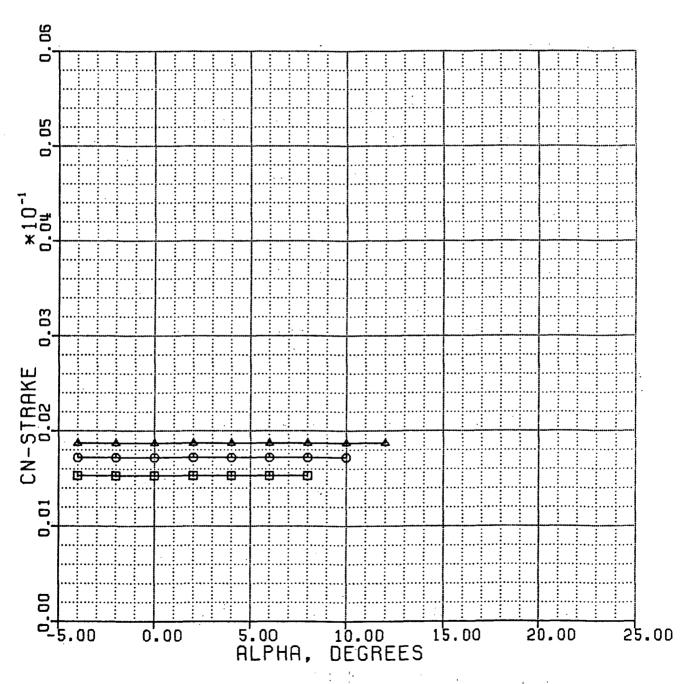
7-27-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
9 ALT = 30K ALP: -4 TO 8

9 PLT = 40K ALP: -4 TO 10

ALT = 50K ALP: -4 TO 12
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Cy - AILERON VS MACH

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

9 ALT = S.L. M# = .2 TO 1.05 9 ALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4

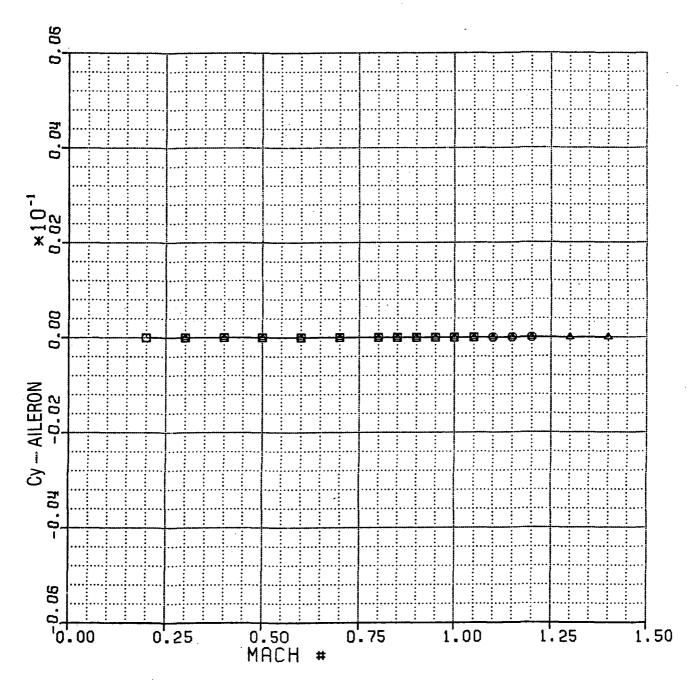
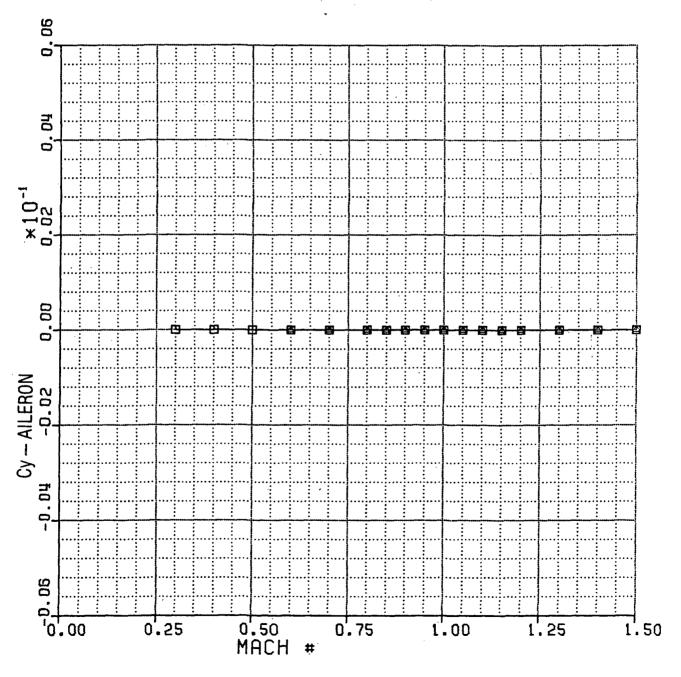


Figure 53(a)

Cy - AILERON VS MACH

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

9 ALT = 30K M# = .3 TO 1.5 9 ALT = 40K M# = .6 TO 1.5 A ALT = 50K M# = .6 TO 1.5



7-26-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 5.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22

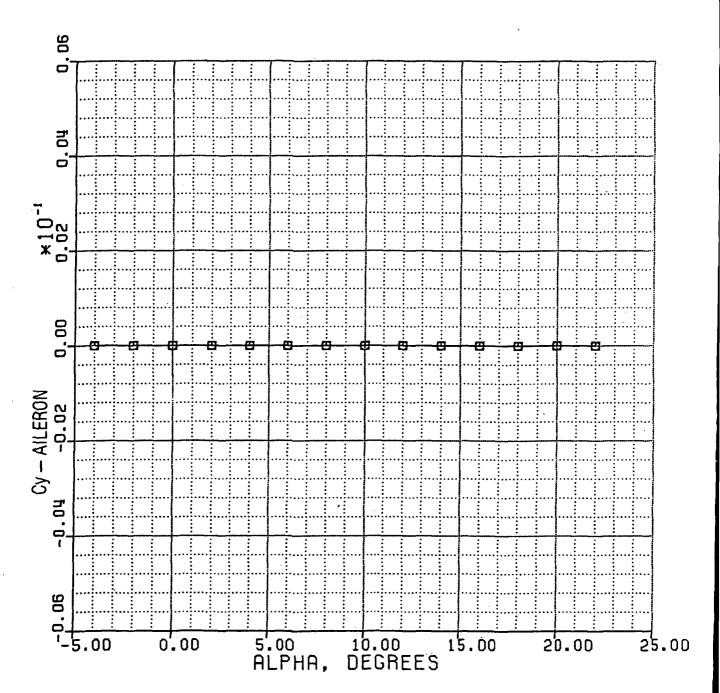
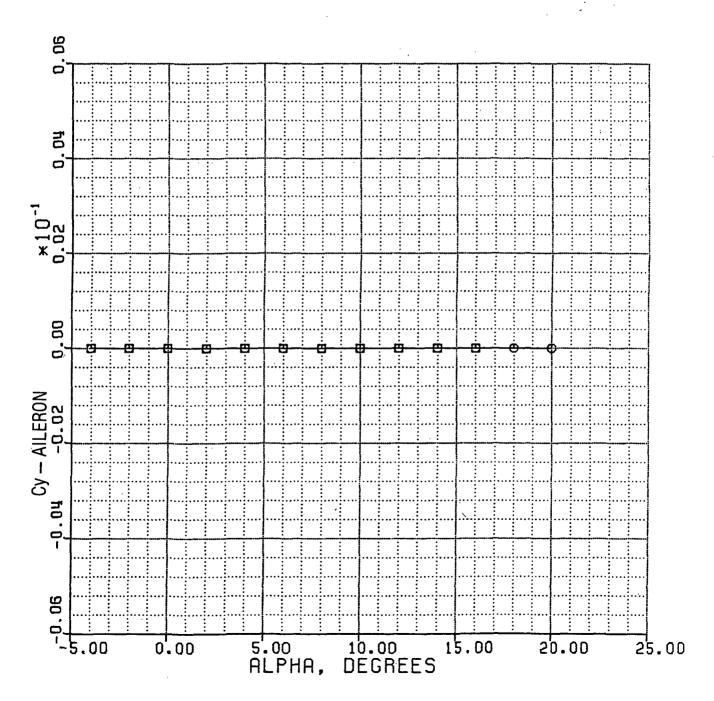


Figure 54(a)

7-26-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 10K ALP: -4 TO 16 0 ALT = 20K ALP: -4 TO 20



7-26-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

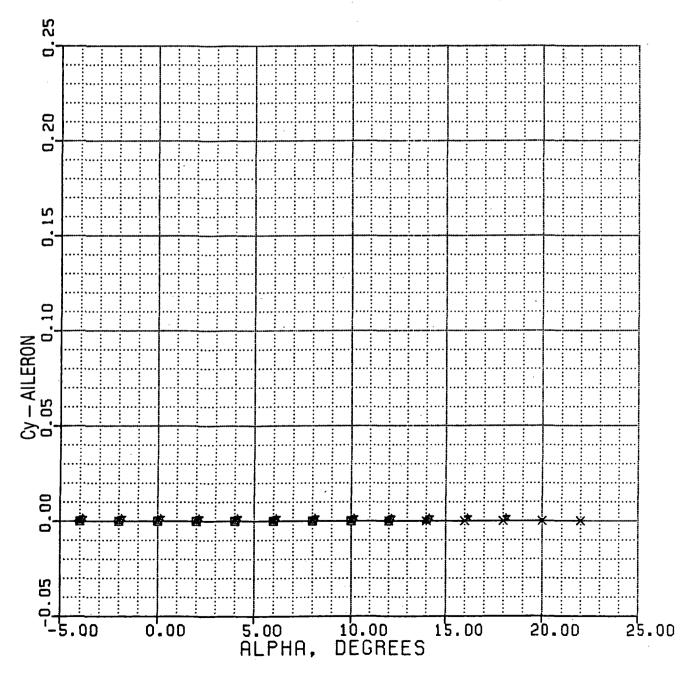
```
P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALT = 30K ALP: -4 TO 14

A ALT = 40K ALP: -4 TO 18

A ALT = 50K ALP: -4 TO 22
```



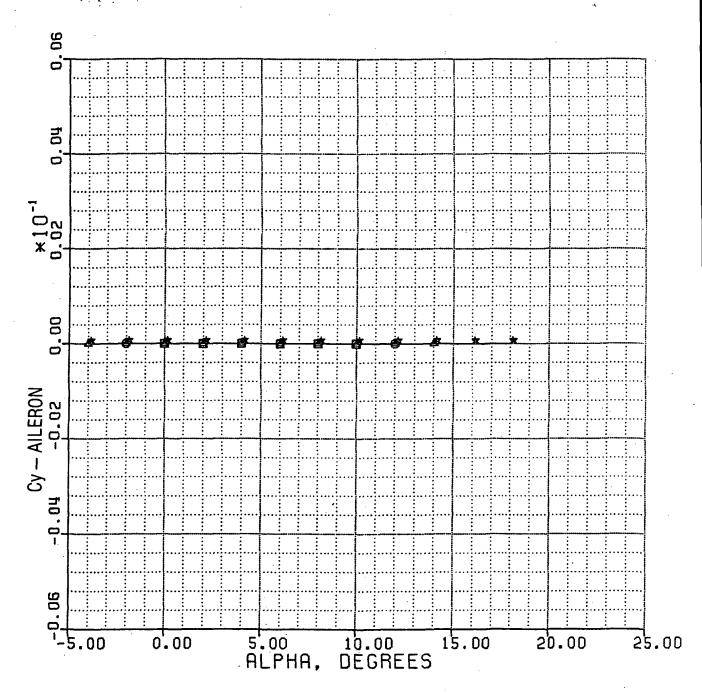
7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: 0 TO 10

P ALT = 30K ALP: -2 TO 12

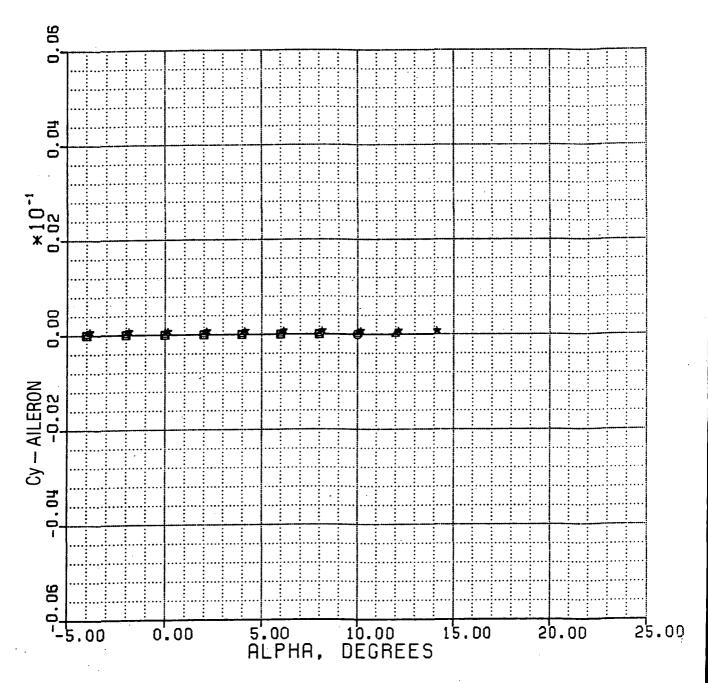
A ALT = 40K ALP: -4 TO 14

A ALT = 50K ALP: -4 TO 18



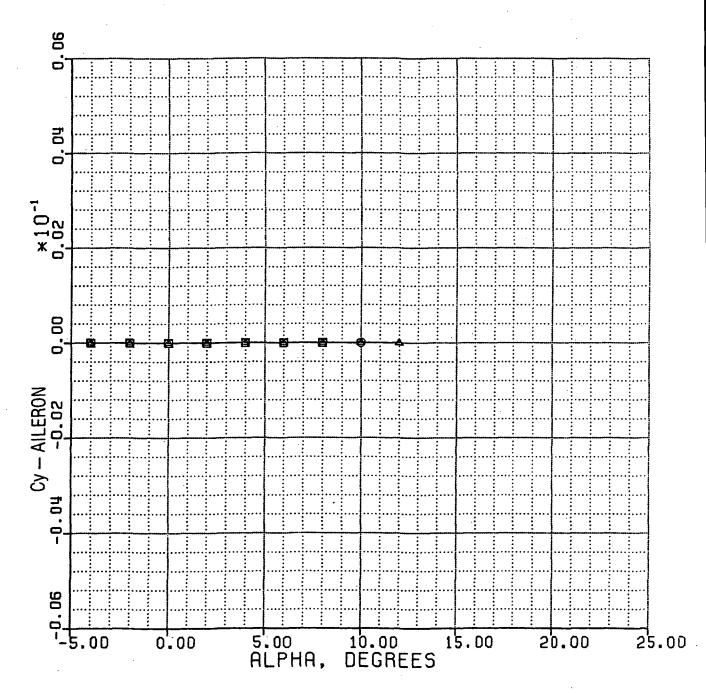
7-27-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
O PALT = 20K ALP: -4 TO B
O PALT = 30K ALP: -4 TO 10
A ALT = 40K ALP: -4 TO 12
A ALT = 50K ALP: -4 TO 14
```



7-27-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

O ALT = 30K ALP: -4 TO 8
O ALT = 40K ALP: -4 TO 10
A ALT = 50K ALP: -4 TO 12



CI - AILERON VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

```
BLT = S.L. M# = .2 TO 1.05

BLT = 10K M# = .2 TO 1.2

ALT = 20K M# = .3 TO 1.4
```

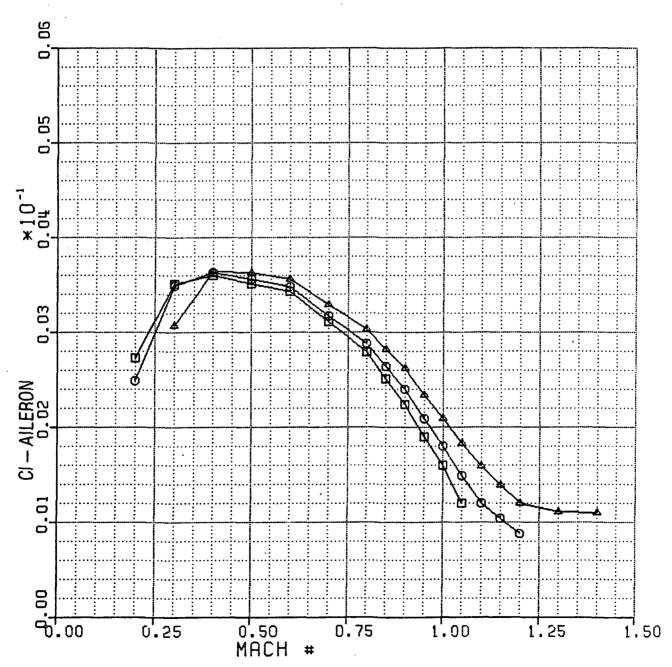


Figure 55(a)

CI - AILERON VS MACH

7-7-83 X-29A 1-G TRIM NØRMAL MØDE XCG = 451.0 WT = 15K

HLT = 30K M# = .3 TO 1.5 HLT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

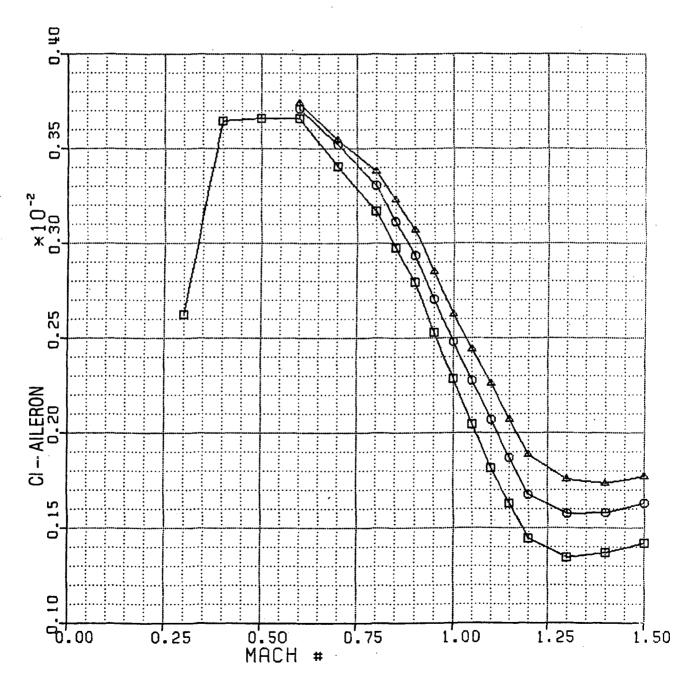


Figure 55(b)

6-16-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = S.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22

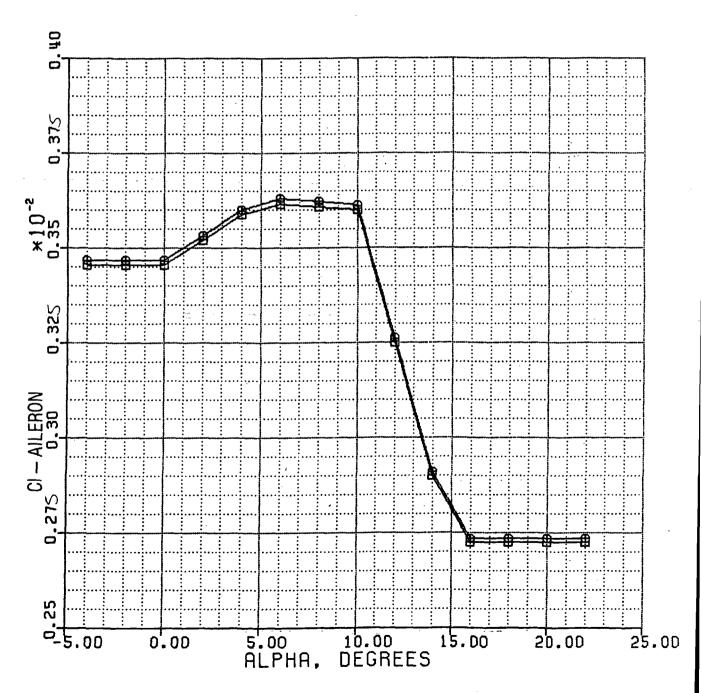
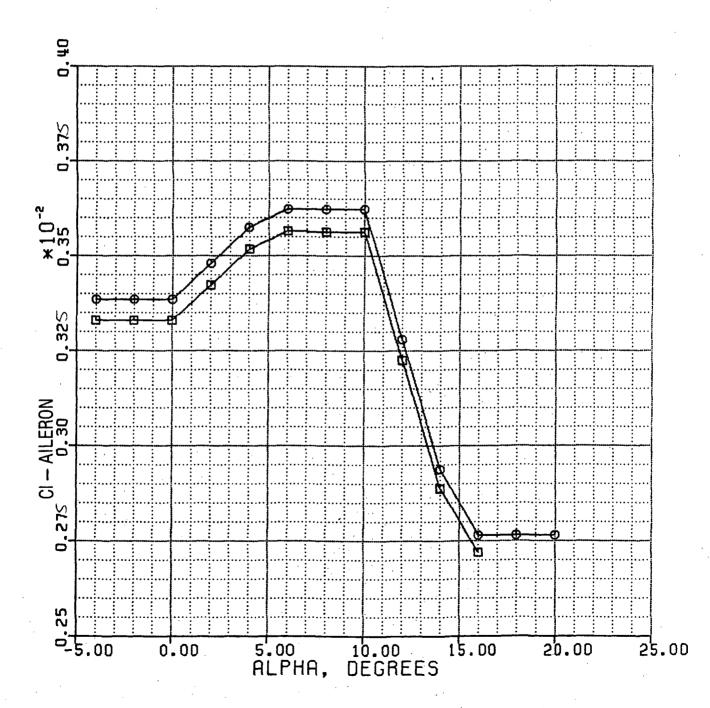


Figure 56(a)

6-17-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 10K ALP: -4 TO 16 0 ALT = 20K ALP: -4 TO 20

STATE AND STATE



6-30-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

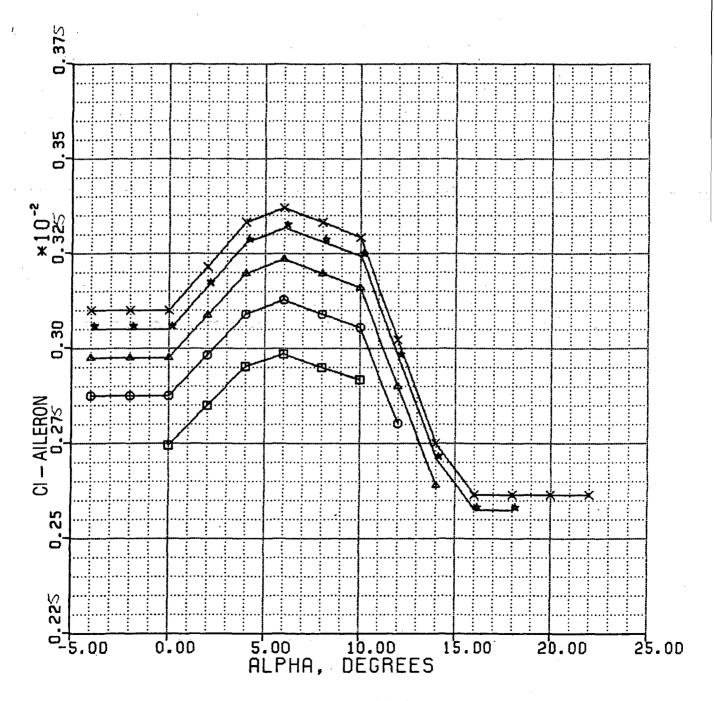
A ALP = 30K ALP: -4 TO 14

A ALP = 40K ALP: -4 TO 18

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A ALP: -4 TO 22

OF POOR QUALITY
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7-1-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

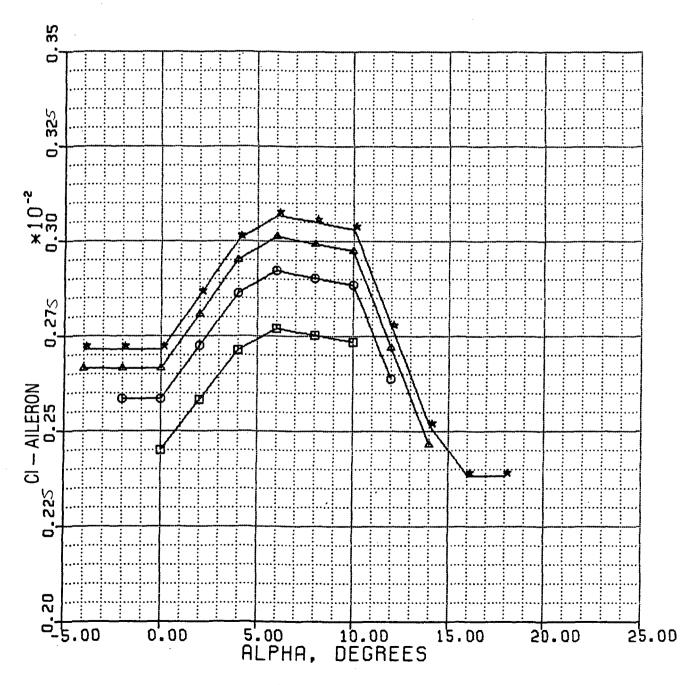


Figure 56(d)

```
7-1-83 X-29A M# = 1.2 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM
```

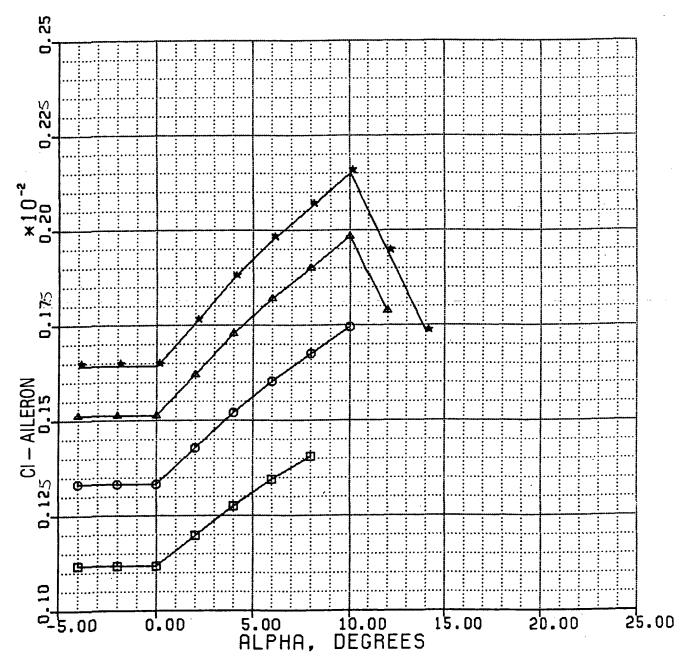


Figure 56(e)

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8 9 ALT = 40K ALP: -4 TO 10 ALT = 50K ALP: -4 TO 12

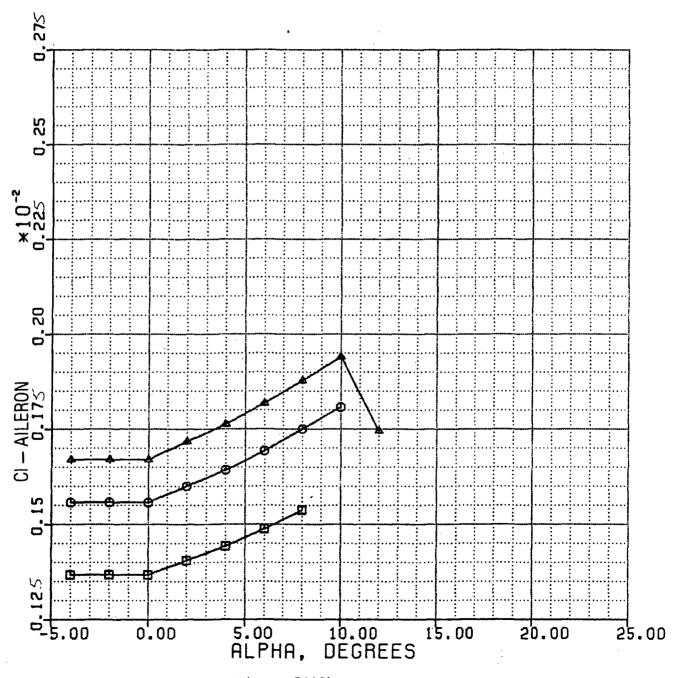


Figure 56(f)

Cn - AILERON VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

O ALT = S.L. M# = .2 TO 1.05 O ALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4

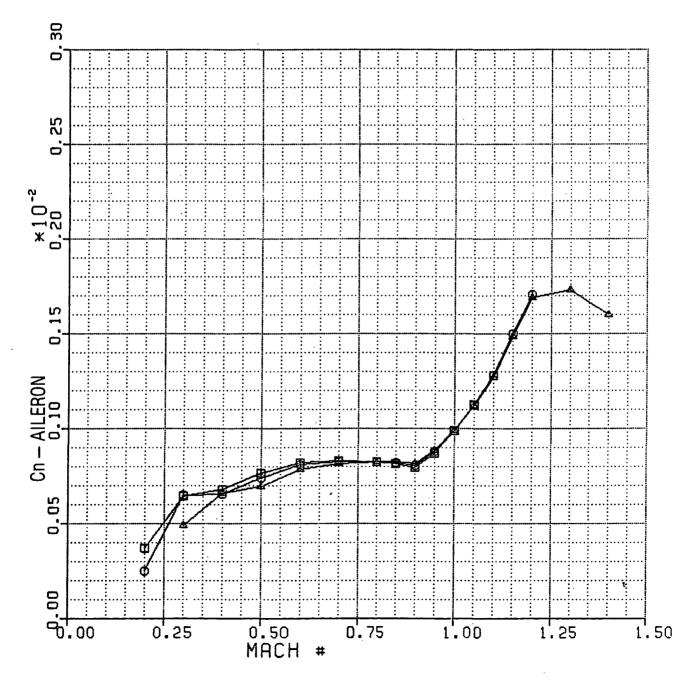


Figure 57(a)

Cn - AILERON VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

O ALT = 30K M# = .3 TO 1.5 O ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

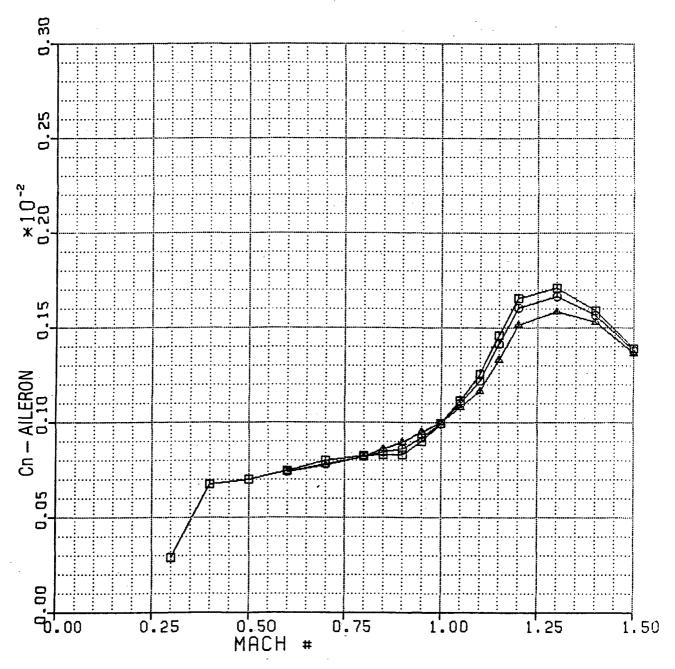


Figure 57(b)

6-16-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 5.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22

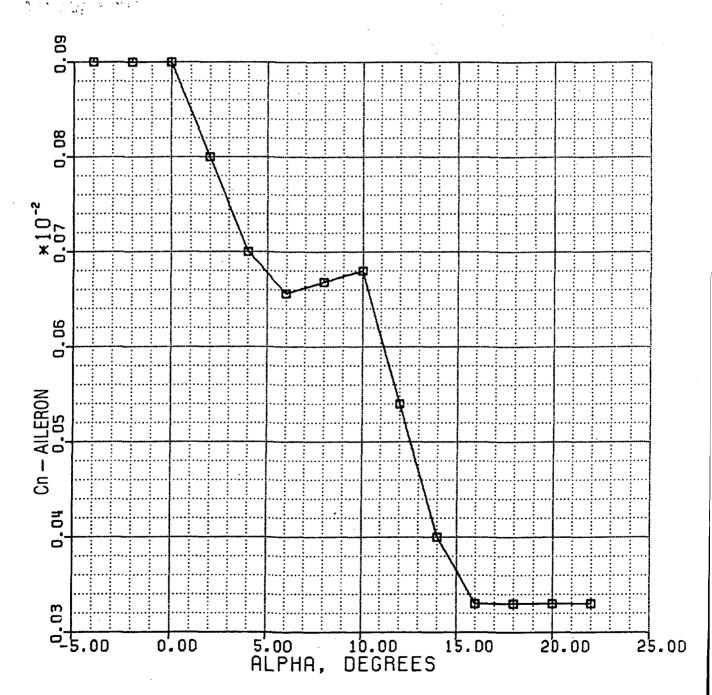


Figure 58(a)

6-17-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 10K ALP: -4 TO 16 9 ALT = 20K ALP: -4 TO 20

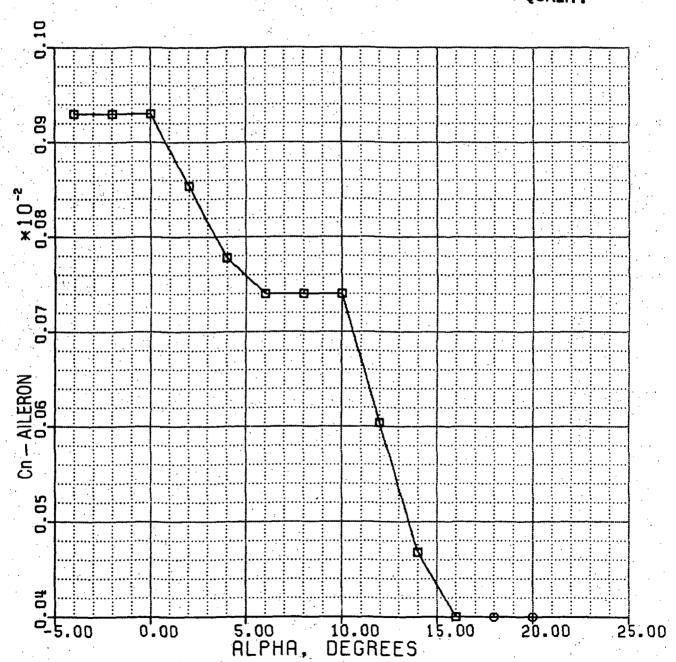


Figure 58(b)

ALT = 40K ALP: -4 TO 18 ORIGINAL PAGE 19

ALT = 50K ALP: -4 TO 22 OF POOR QUALITY

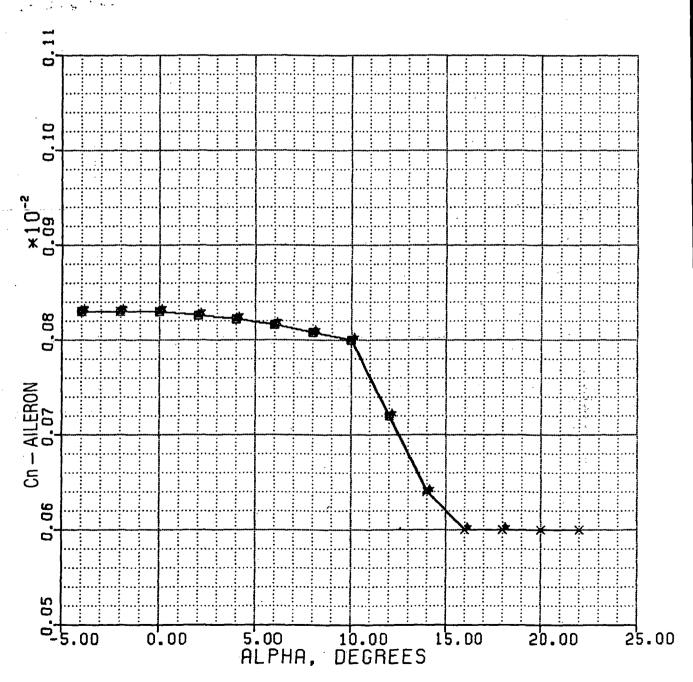


Figure 58(c)

Cn - AILERON VS ALPHA

7-1-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 20K ALP: 0 TO 10 _____ ALT = 30K ALP: -2 TO 12 ___ ALT = 40K ALP: -4 TO 14 A ALT = 50K ALP: -4 TO 18 ORIGINAL PAGE IS

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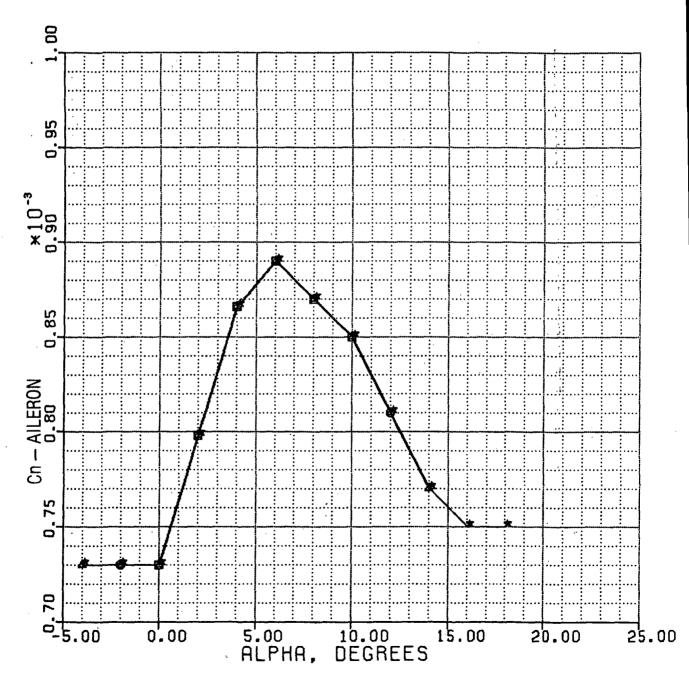


Figure 58(d)

Cn - AILERON VS ALPHA

7-1-83 X-29A M# = 1.2 NØRMÅL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14

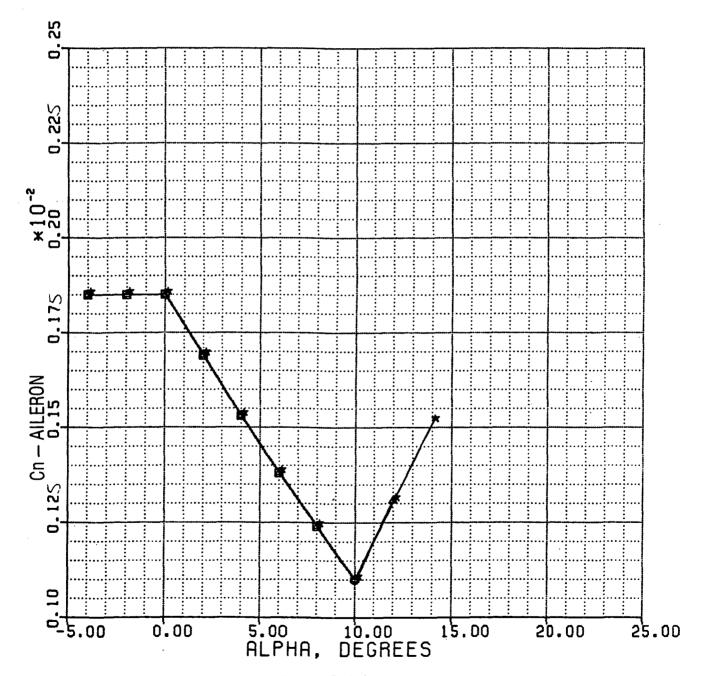


Figure 58(e)

Cn - AILERON VS ALPHA

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

PARTIE WERE

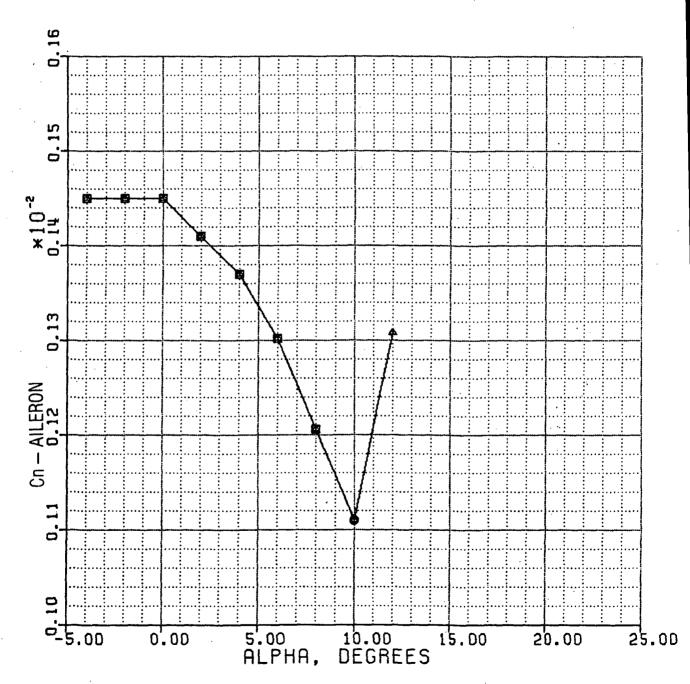


Figure 58(f)

Cy - RUDDER VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = S.L. M# = .2 TO 1.05 P ALT = 10K M# = .2 TO 1.2 ALT = 20K M# = .3 TO 1.4

were their factors

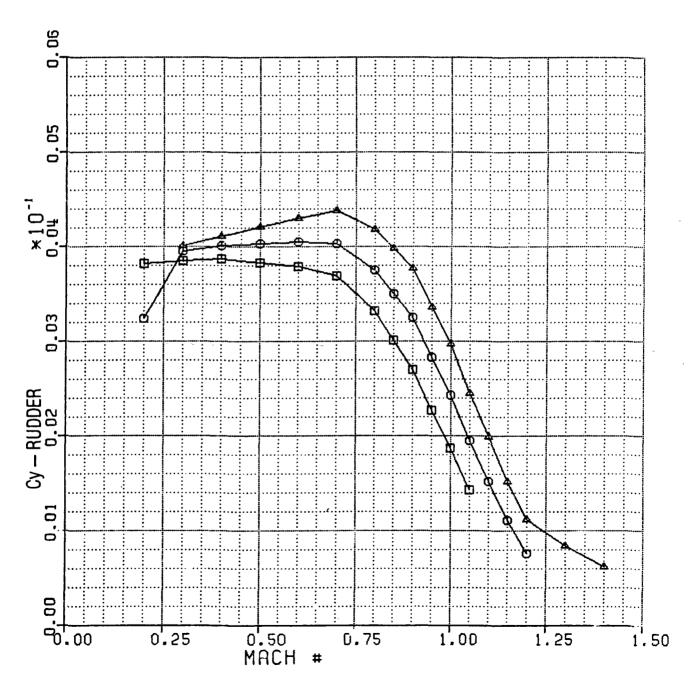
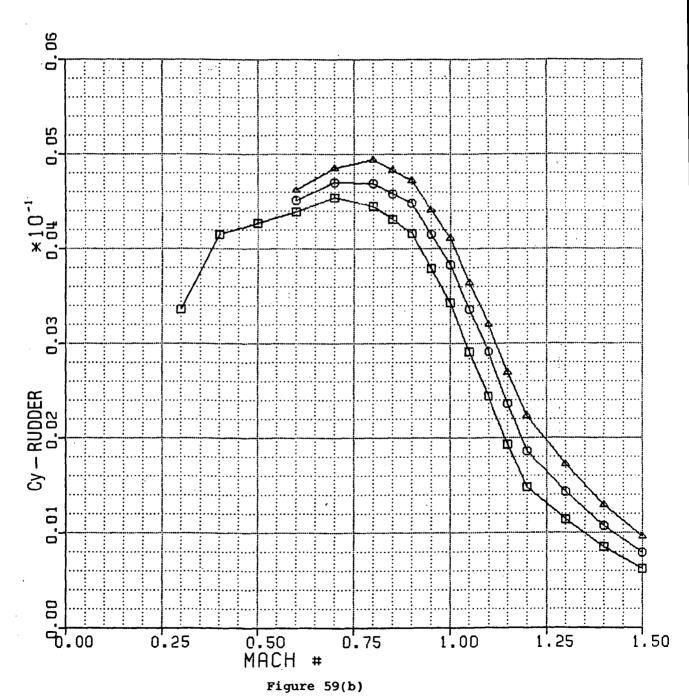


Figure 59(a)

Cy - RUDDER VS MACH



7-26-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = S.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22

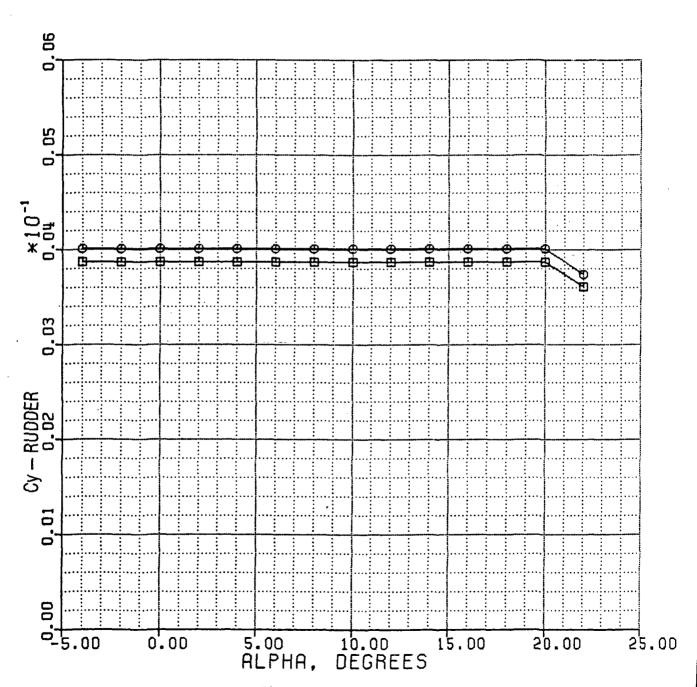


Figure 60(a)

7-26-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

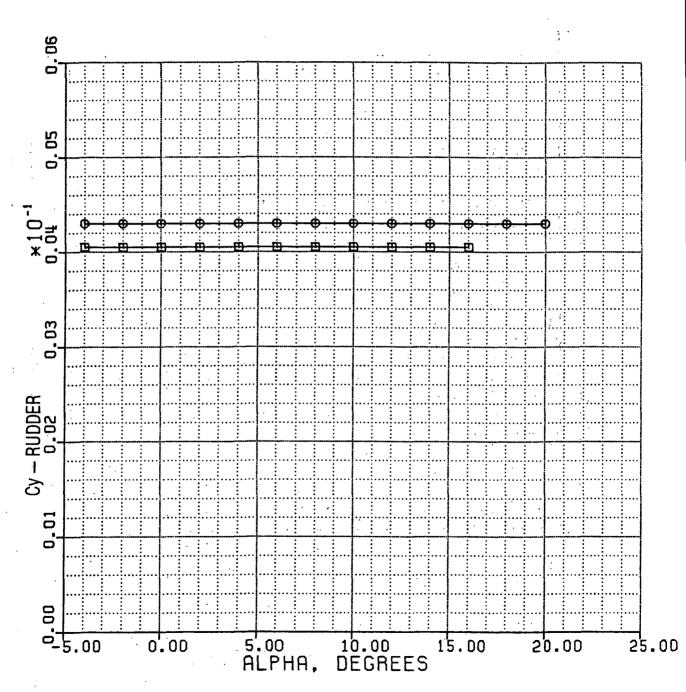


Figure 60(b)

```
7-26-83 X-29A M# = 0.8 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALT = 30K ALP: -4 TO 14

A ALT = 40K ALP: -4 TO 18

A ALT = 40K ALP: -4 TO 22
```

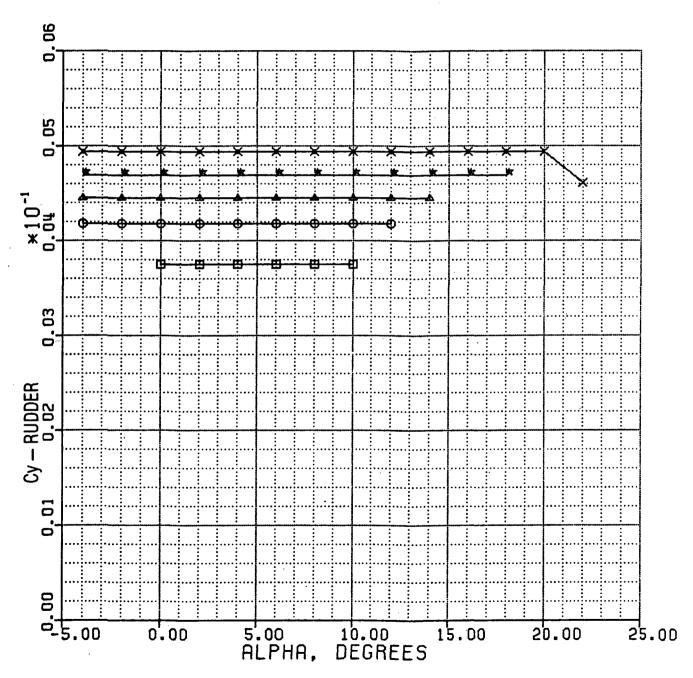


Figure 60(c)

7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: 0 T0 10

P ALT = 30K ALP: -2 T0 12

ALT = 40K ALP: -4 T0 14

ALT = 50K ALP: -4 T0 18

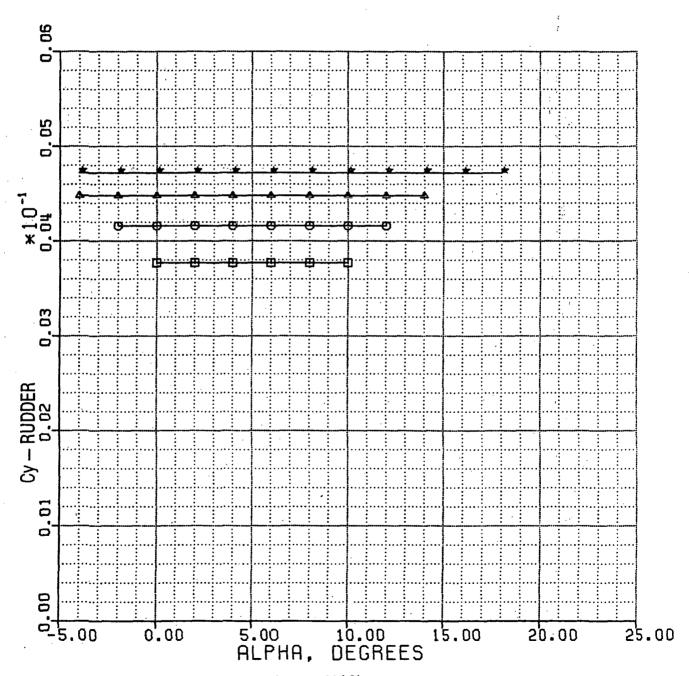


Figure 60(d)

7-27-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

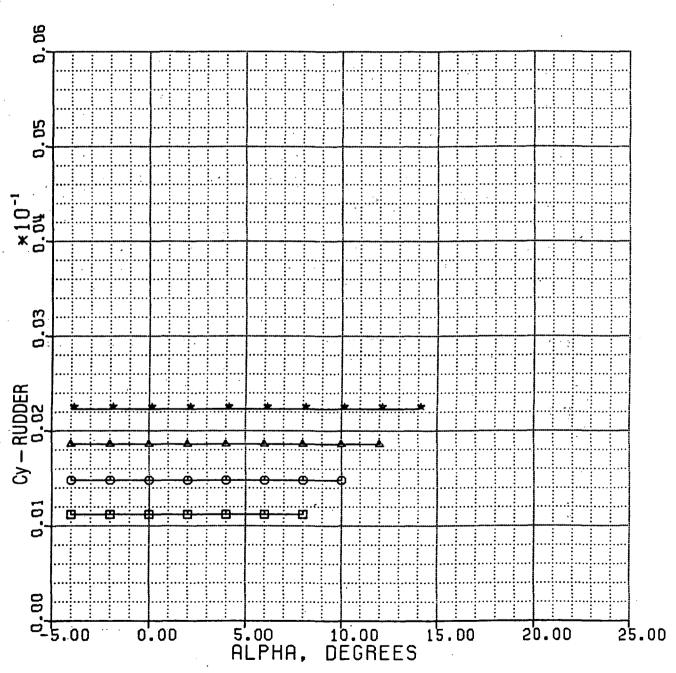


Figure 60(e)

7-27-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8 9 ALT = 40K ALP: -4 TO 10 ALT = 50K ALP: -4 TO 12

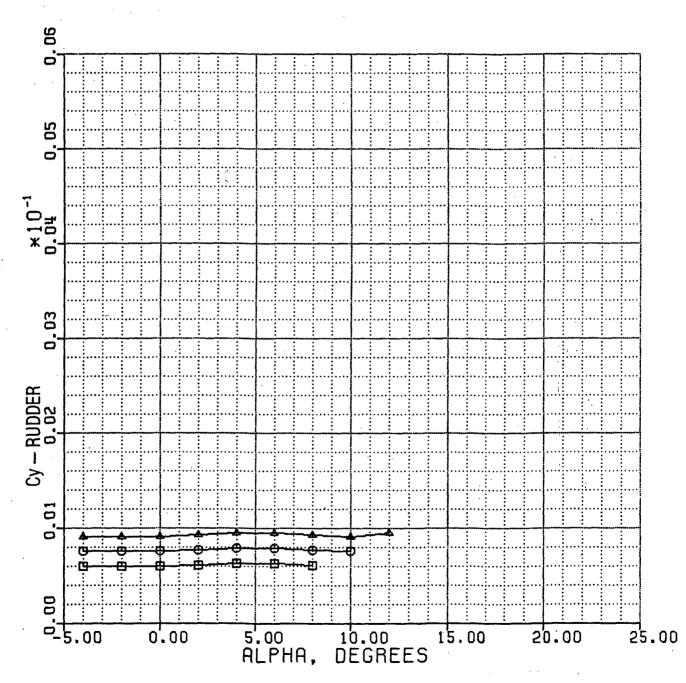
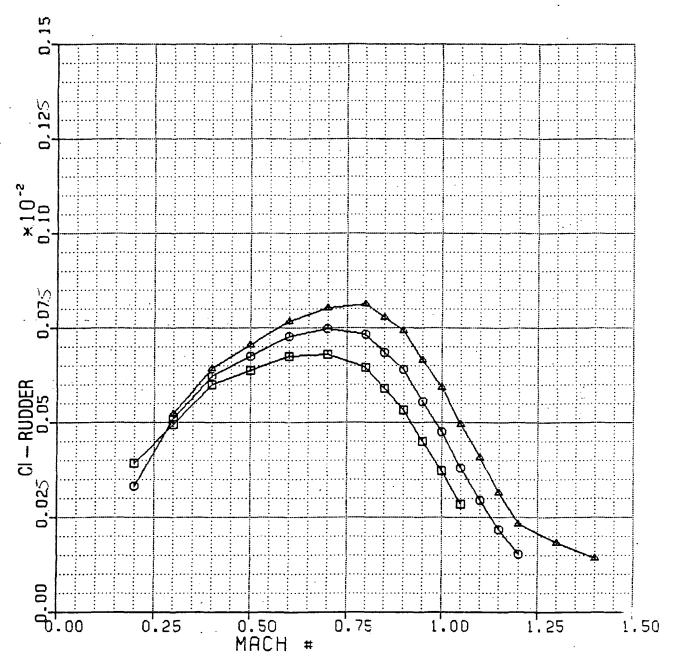


Figure 60(f)

CI - RUDDER VS MACH

7-6-83 X-29A 1-G TRIM NORMAL XCG = 451.0 WT = 15Kpn ALT = S.L. M* = .2 T0 1.05M = .2 TO 1.2ORIGINAL PAGE IS ALT = 20K M* = .3 T0 1.4

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CI - RUDDER VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

PALT = 30K M# = .3 TO 1.5 PALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

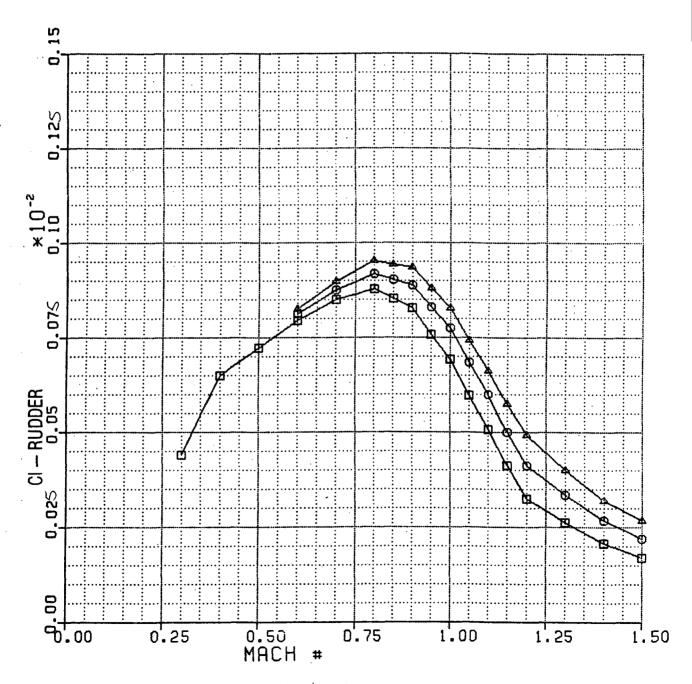


Figure 61(b)

7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = S.L. ALP: -4 TO 22 P ALT = 10K ALP: -4 TO 22

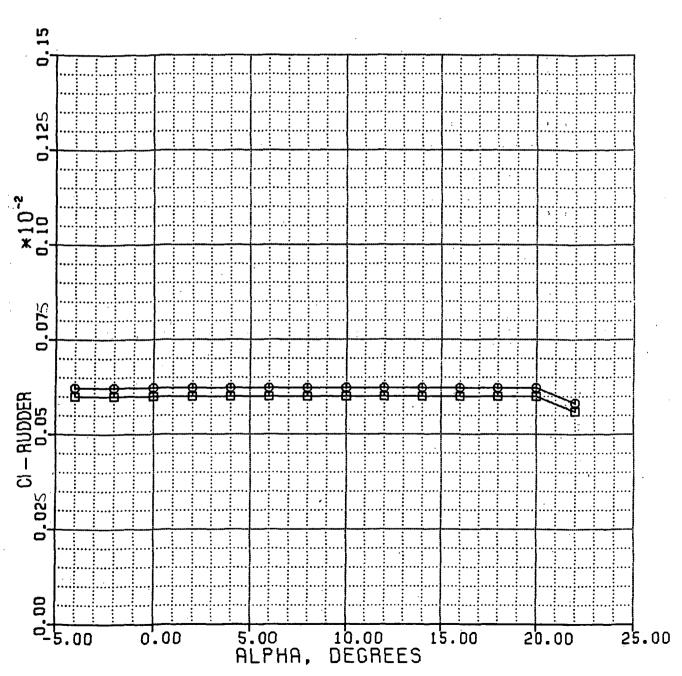


Figure 62(a)

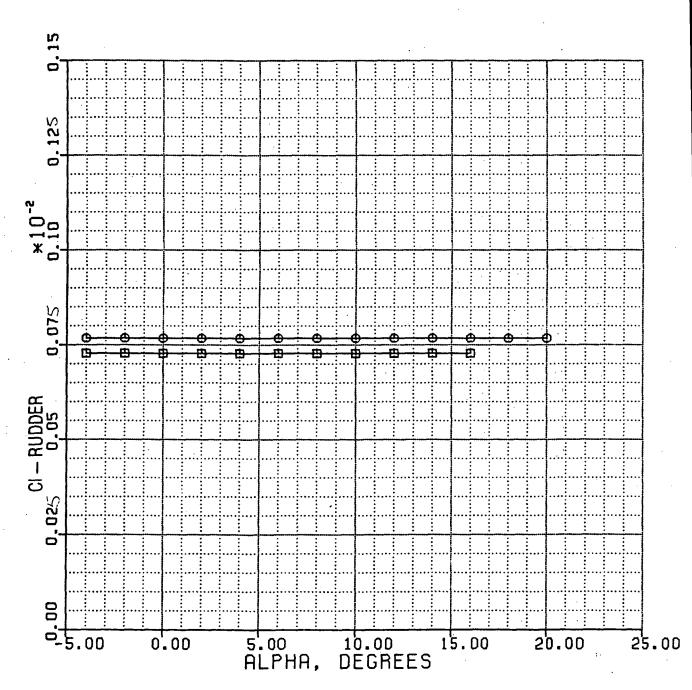


Figure 62(b)

```
7-26-83 X-29A M# = 0.8 NØRMAL MØDE

XCG = 451.0 WT = 15K ALPHA TRIM
```

```
P ALT = 10K ALP: 0 T0 10

P ALT = 20K ALP: -4 T0 12

A ALT = 30K ALP: -4 T0 14

P ALT = 40K ALP: -4 T0 18

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X ALT = 50K ALP: -4 T0 22

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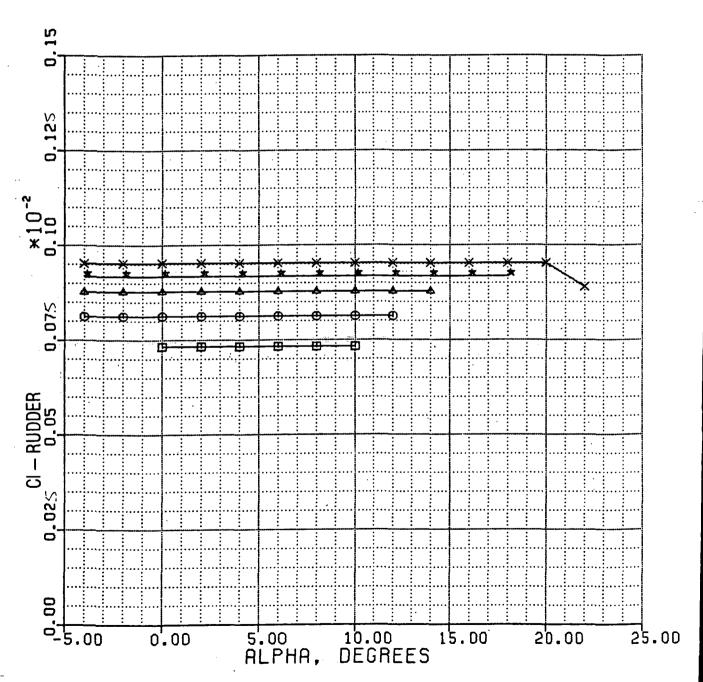


Figure 62(c)

7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

PALT = 20K RLP: 0 TO 10

PALT = 30K ALP: -2 TO 12

ALT = 40K ALP: -4 TO 14

ALT = 50K ALP: -4 TO 18

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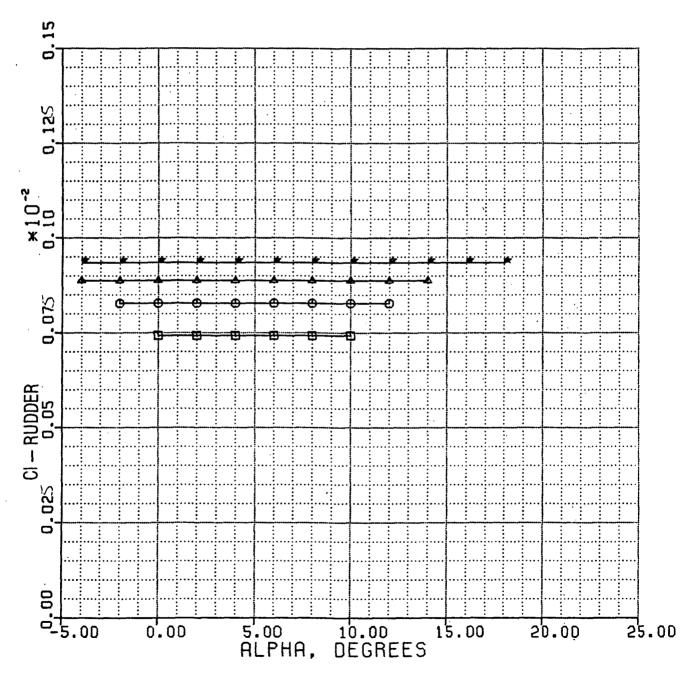


Figure 62(d)

7-27-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

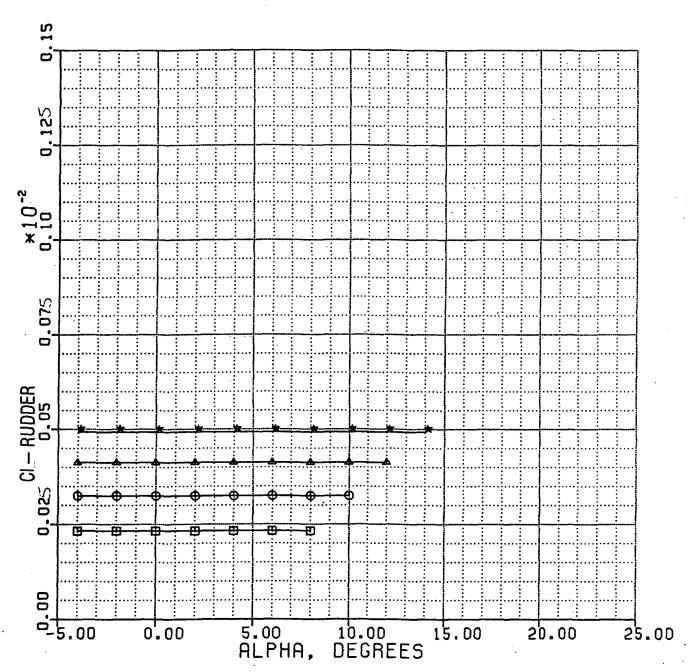


Figure 62(e)

7-27-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 30K ALP: -4 TO 8

P ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12

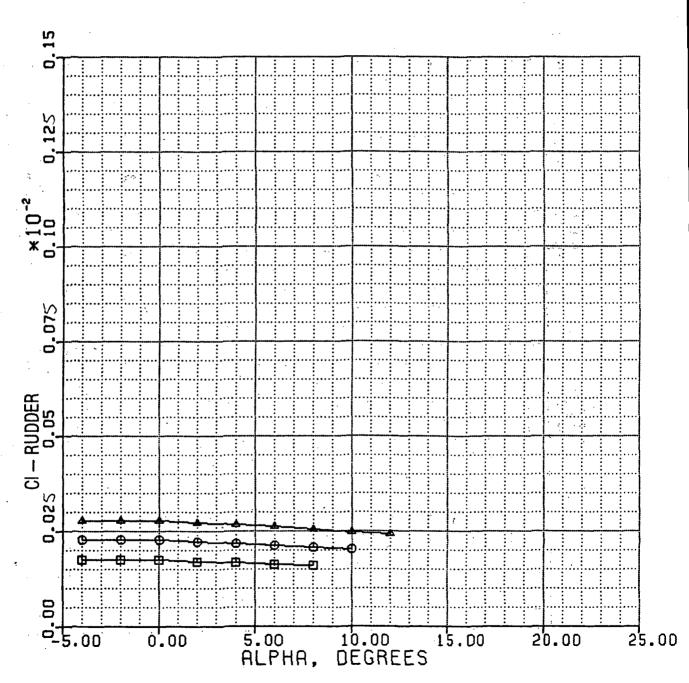


Figure 62(f)

Cn - RUDDER VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = S.L. M# = .2 TO 1.05

P ALT = 10K M# = .2 TO 1.2

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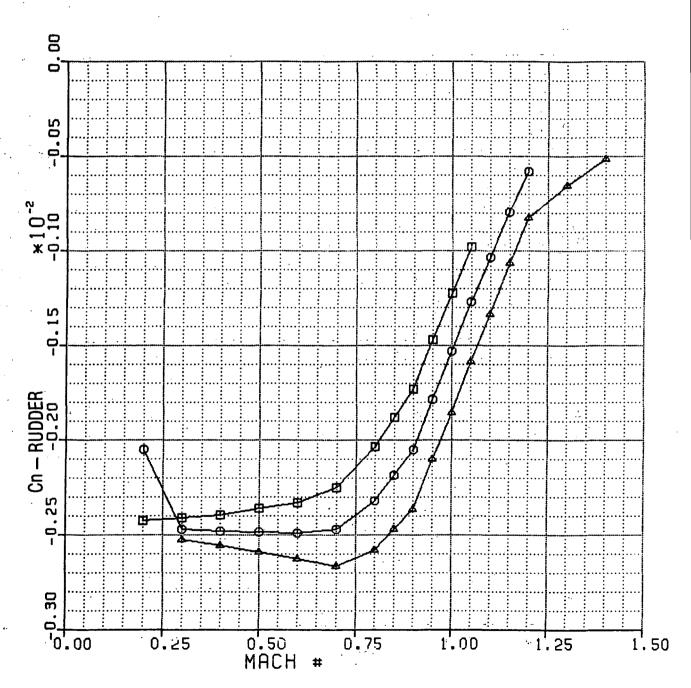


Figure 63(a)

Cn — RUDDER VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

PALT = 30K M# = .3 TO 1.5 PALT = 40K M# = .6 TO 1.5 A ALT = 50K M# = .6 TO 1.5

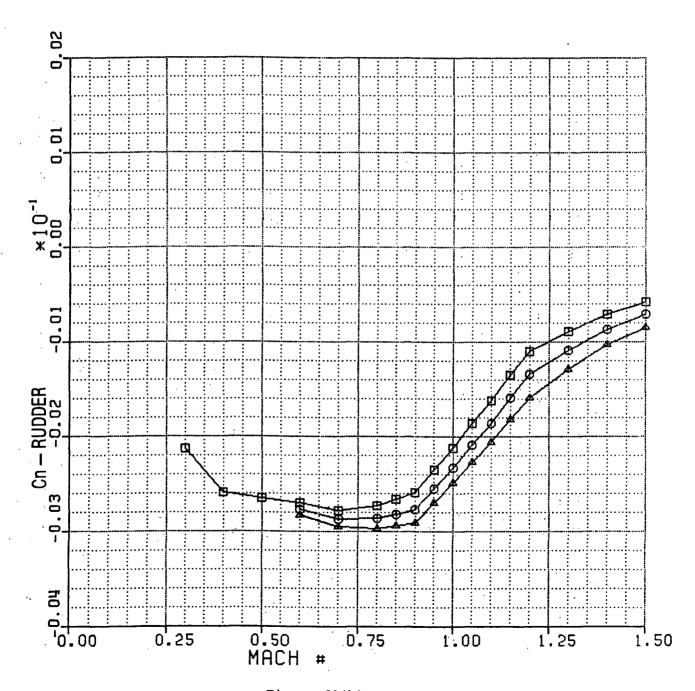


Figure 63(b)

7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

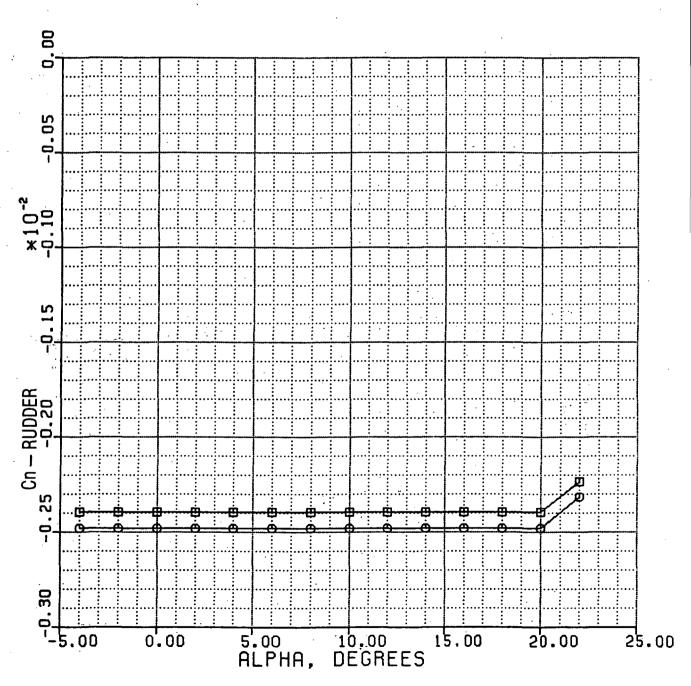


Figure 64(a)

7-26-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

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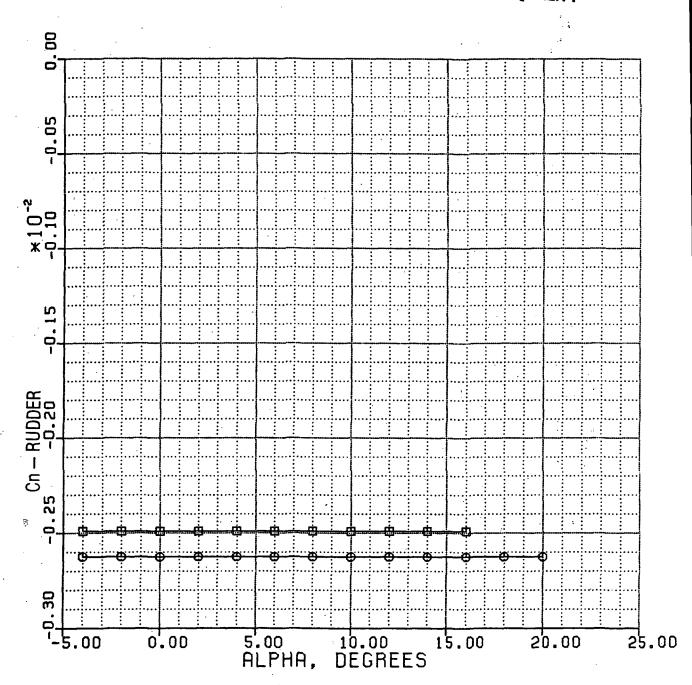


Figure 64(b)

7-26-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALT = 30K ALP: -4 TO 14

A ALT = 40K ALP: -4 TO 18

A ALT = 40K ALP: -4 TO 22
```

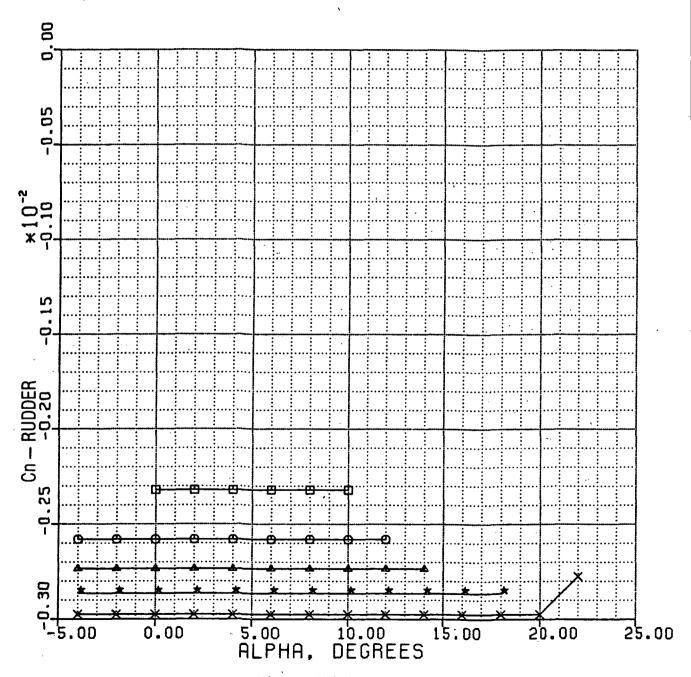


Figure 64(c)

7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: 0 T0 10

P ALT = 30K ALP: -2 T0 12

A ALT = 40K ALP: -4 T0 14

A ALT = 50K ALP: -4 T0 18

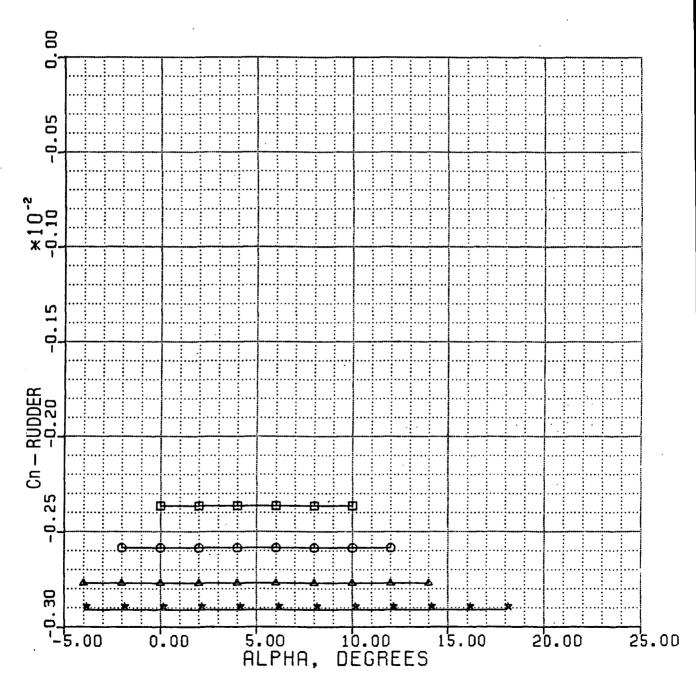


Figure 64(d)

7-27-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14

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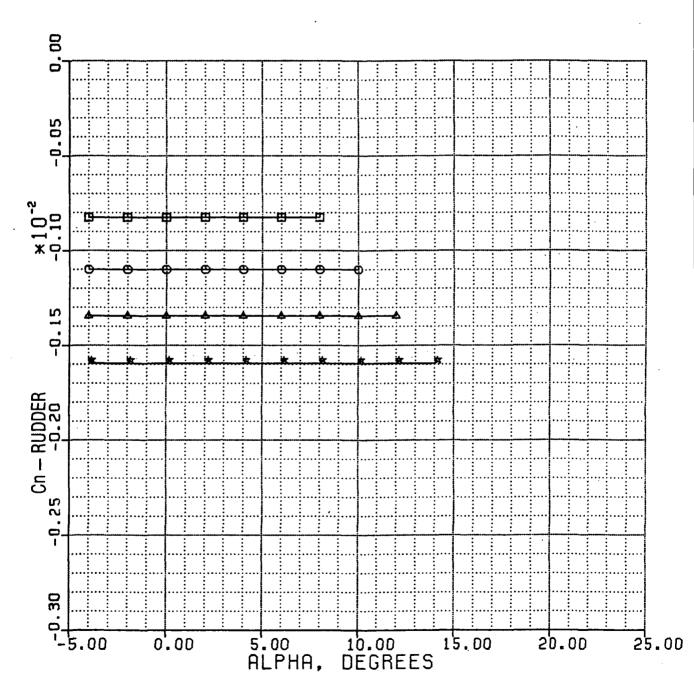


Figure 64(e)

7-27-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P RLT = 30K RLP: -4 TO 8

P RLT = 40K RLP: -4 TO 10

A RLT = 50K RLP: -4 TO 12

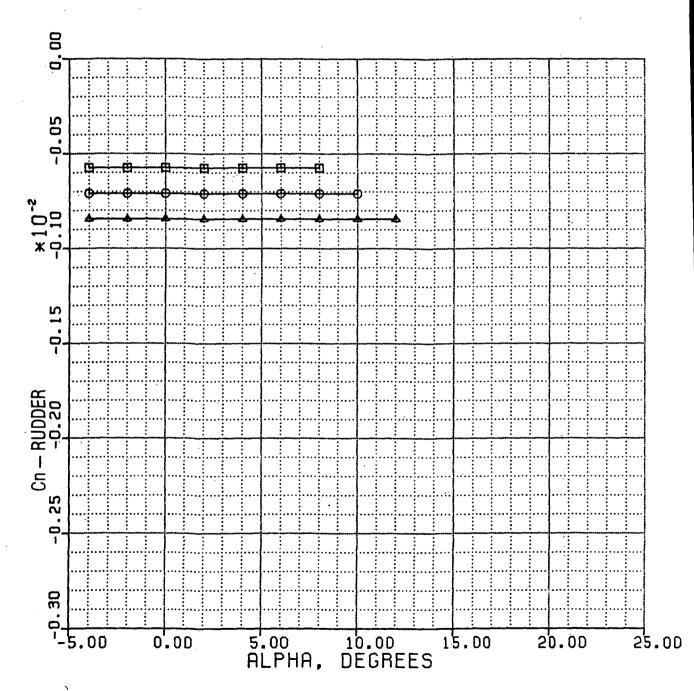


Figure 64(f)

CL-ALPHA VS MACH #

7-5-83 X-29A 1-G TRIM NORMAL MODE

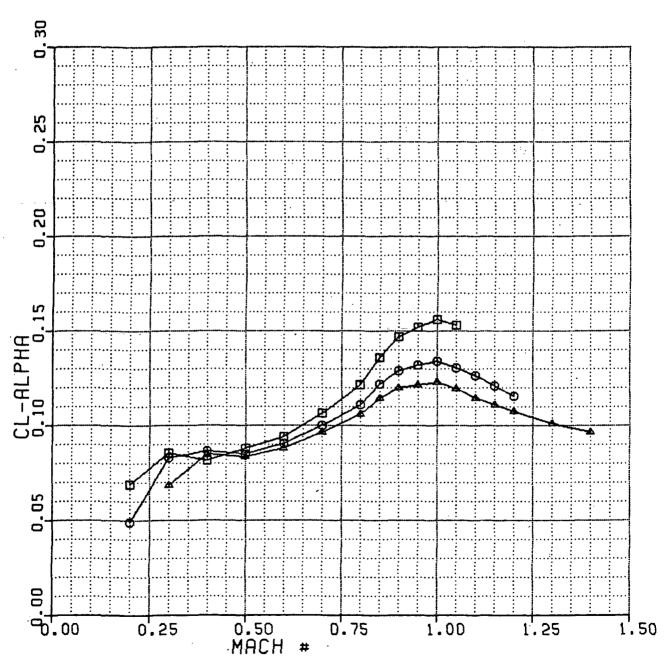
XCG = 451.0 WT = 15K

B ALT = S.L. M# = .2 TO 1.05

ALT = 10K M# = .2 TO 1.2

ALT = 20K M# = .3 TO 1.4

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CL-ALPHA VS MACH # 7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

PALT = 30K M# = .3 TO 1.5 PALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

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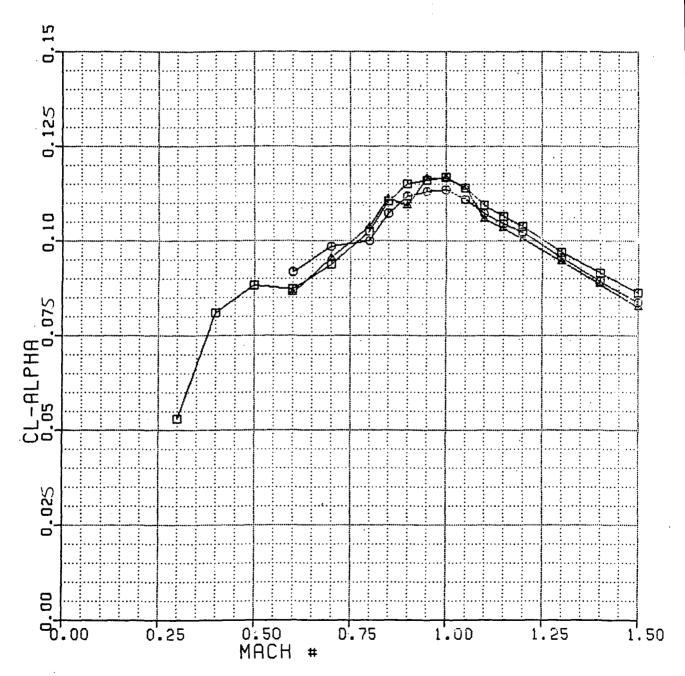


Figure 65(b)

CL-ALPHA VS ALPHA 6-15-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = S.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22

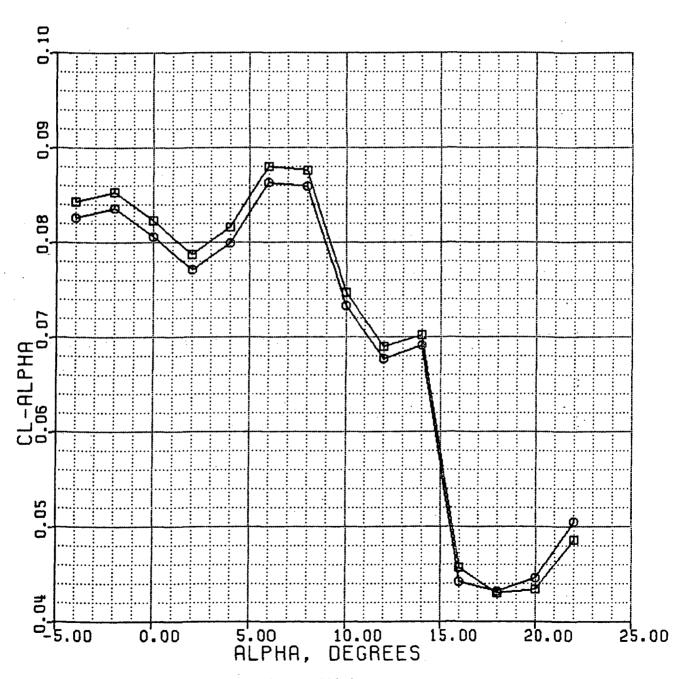


Figure 66(a)

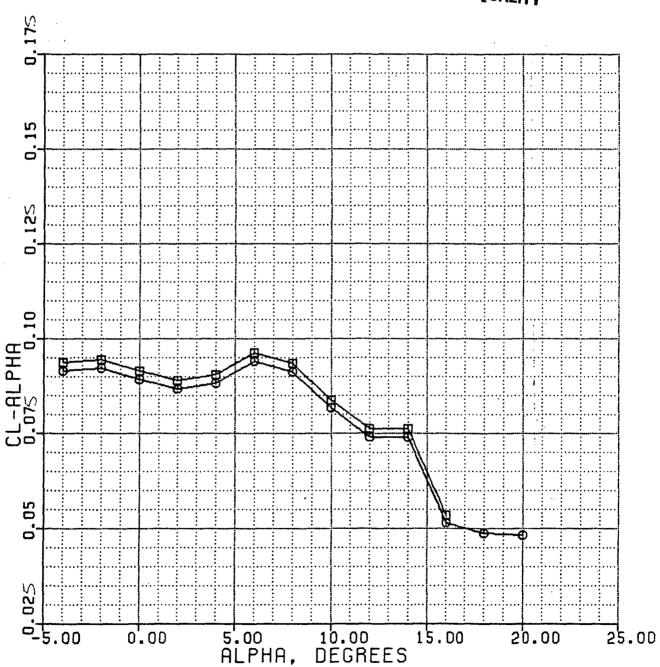


Figure 66(b)

CL-ALPHA VS ALPHA

6-17-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 TO 10

P O ALT = 20K ALP: -4 TO 12

ALP = 30K ALP: -4 TO 14

ALP: -4 TO 18

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ALT = 40K ALP: -4 TO 22
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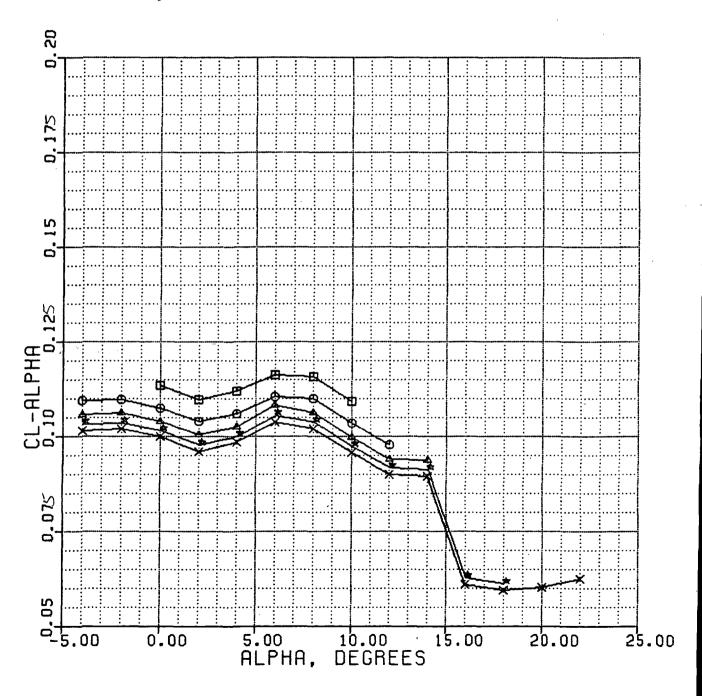


Figure 66(c)

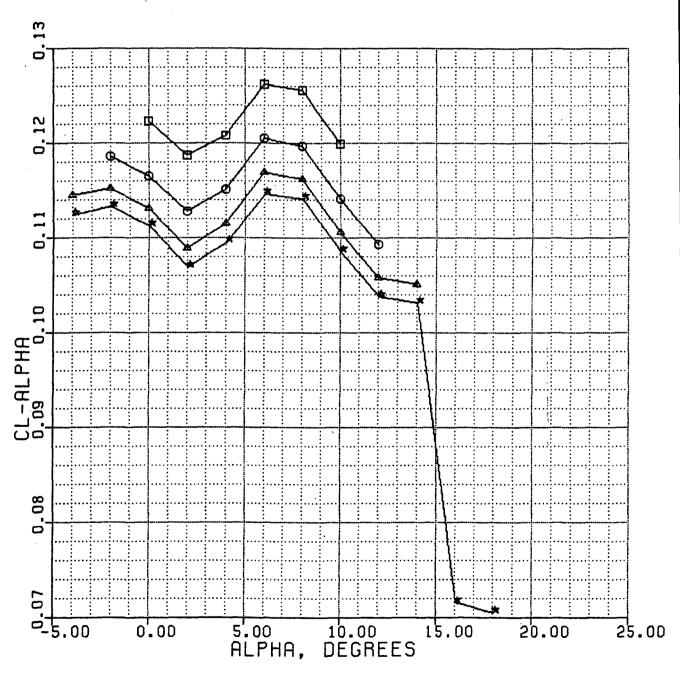


Figure 66(d)

CL-ALPHA VS ALPHA 7-1-83 X-29A M# = 1.2 NORMAL MODE

X-1-83 X-29H M# = 1.2 NORMHL MOUE XCG = 451.0 WT = 15K ALPHA TRIM

```
PALT = 20K ALP: -4 TO 8

PALT = 30K ALP: -4 TO 10

ALT = 40K ALP: -4 TO 12

ALT = 40K ALP: -4 TO 12

ALT = 50K ALP: -4 TO 14

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```

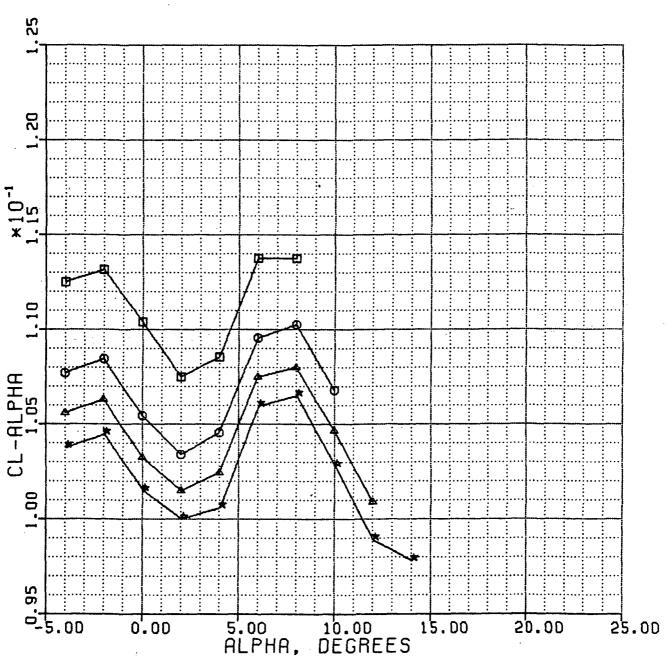


Figure 66(e)

CL-ALPHA VS ALPHA 7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM __O ALT = 40K ALP: -4 TO 10 _ ALT = 50K ALP: -4 TO 12 ORIGINAL PAGE IS

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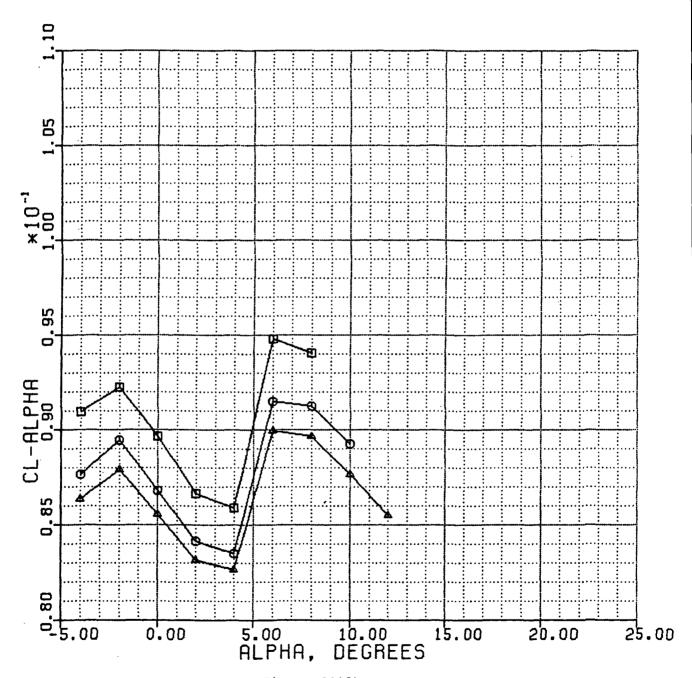


Figure 66(f)

CD-ALPHA VS MACH # 7-5-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = S.L. M# = .2 TO 1.05.

P ALT = 10K M# = .2 TO 1.2

A ALT = 20K M# = .3 TO 1.4

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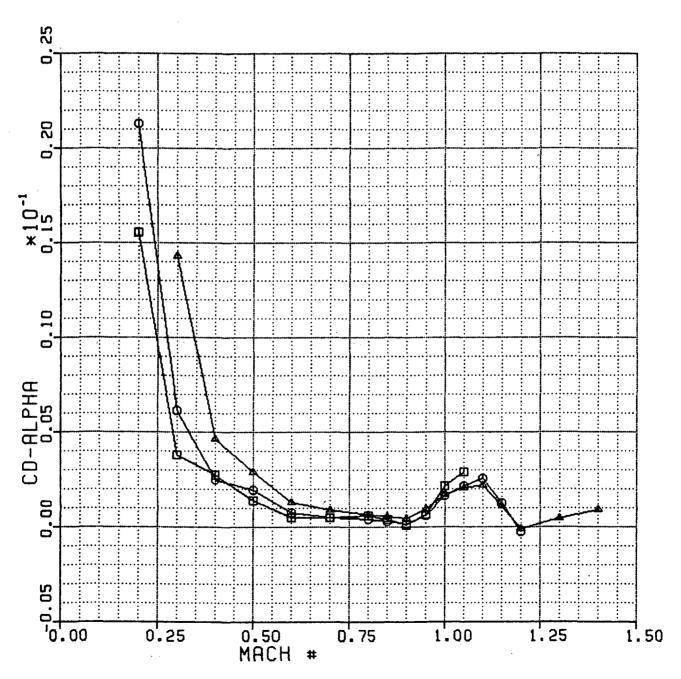


Figure 67(a)

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CD-ALPHA VS MACH # 7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K
```

```
9 ALT = 30K M# = .3 TO 1.5

9 ALT = 40K M# = .6 TO 1.5

ALT = 50K M# = .6 TO 1.5
```

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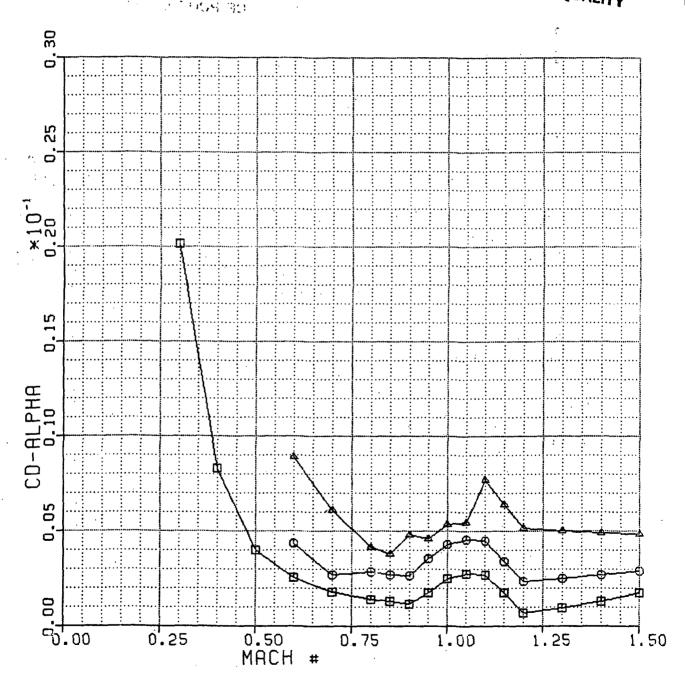


Figure 67(b)

CD-ALPHA VS ALPHA
6-15-83 X-29A M# = 0.4 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

B RLT = S.L. ALP: -4 TØ 22

B ALT = 10K ALP: -4 TØ 22

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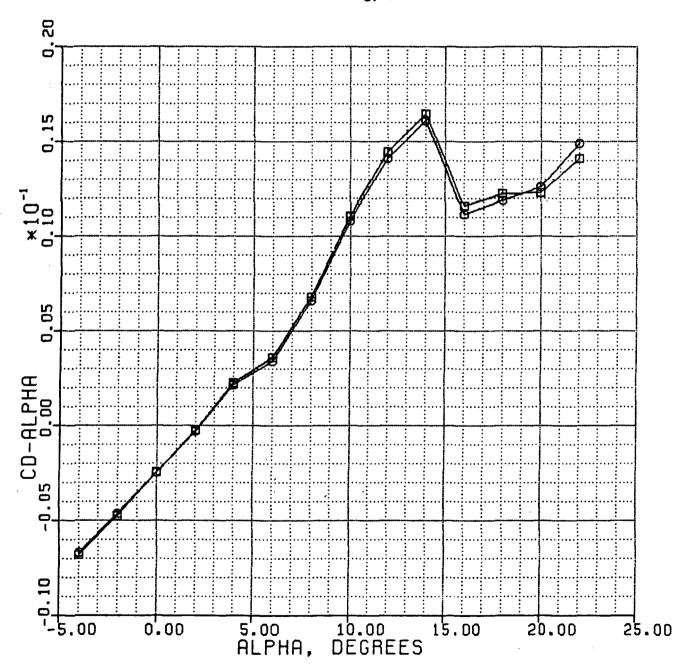


Figure 68(a)



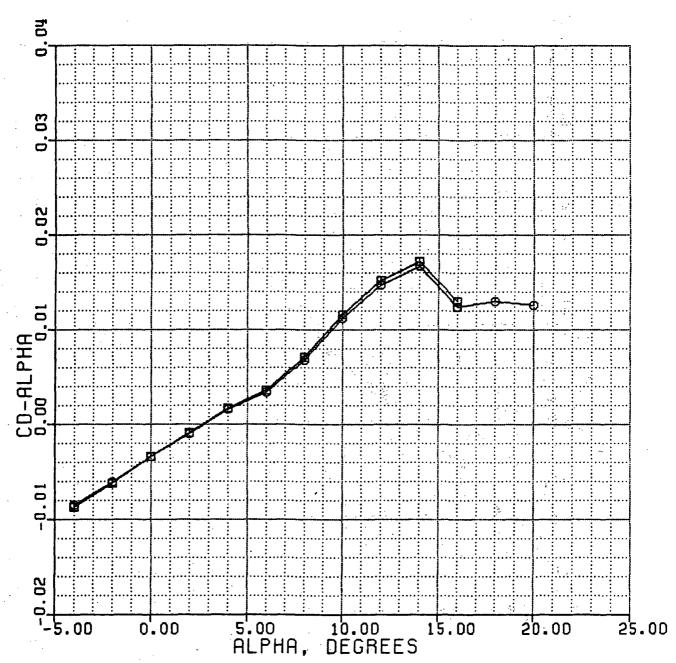


Figure 68(b)

CD-ALPHA VS ALPHA

6-17-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

ALT = 10K ALP: 0 TO 10 RLT = 20KALP: -4 TO 12 ALP = 30KALP: -4 TO 14 # ALT = 40K ALP: -4 TO 18

→ ALT = 50K ALP: -4 TO 22

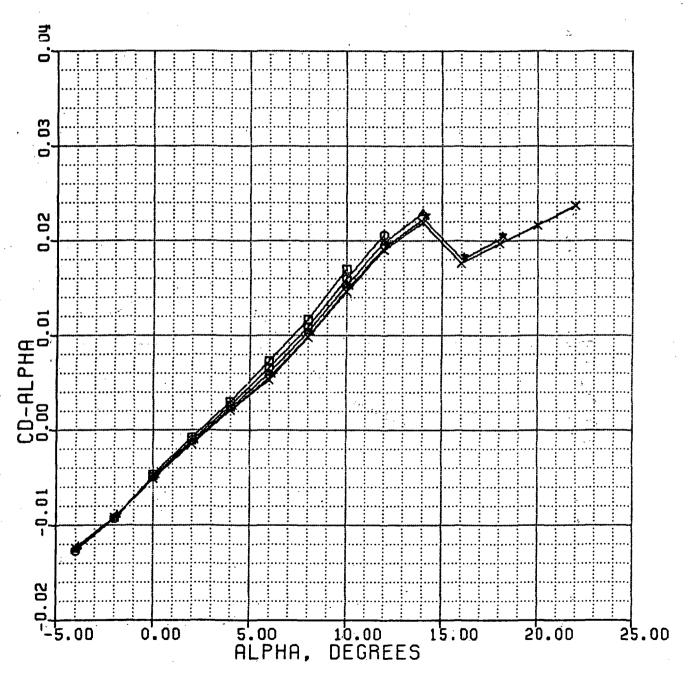


Figure 68(c)

CD-ALPHA VS ALPHA

7-1-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: 0 T0 10

P ALT = 30K ALP: -2 T0 12

ALT = 40K ALP: -4 T0 14

ALT = 50K ALP: -4 T0 18
```

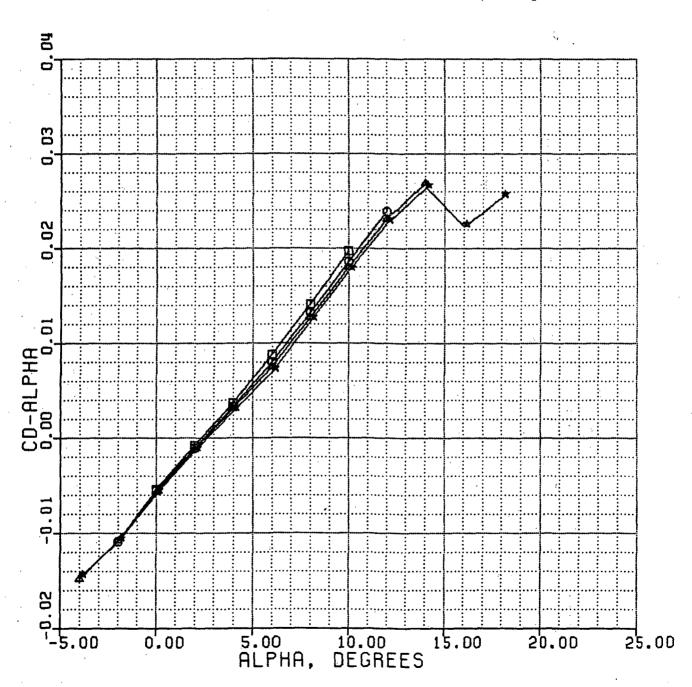


Figure 68(d)

CD-ALPHA VS ALPHA

7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

PALT = 20K ALP: -4 TO 8

PALT = 30K ALP: -4 TO 10

ALT = 40K ALP: -4 TO 12

ALT = 50K ALP: -4 TO 14

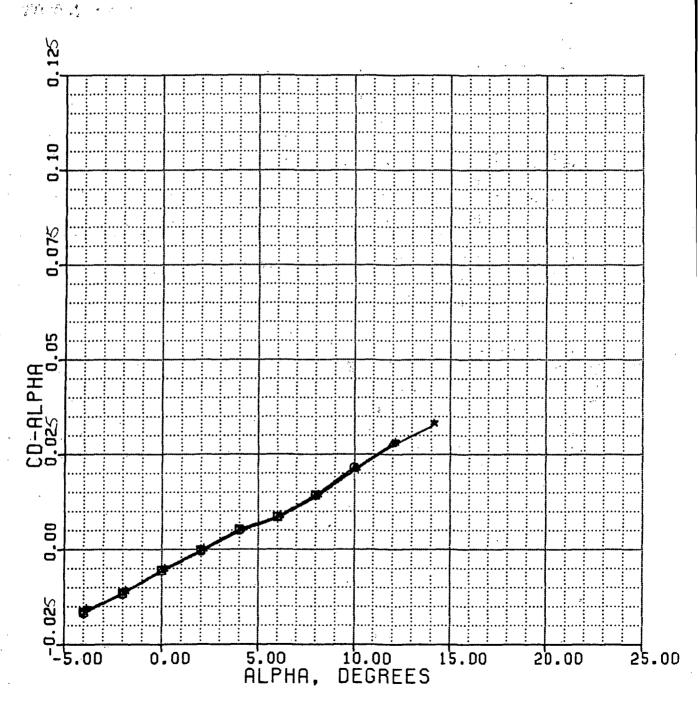


Figure 68(e)

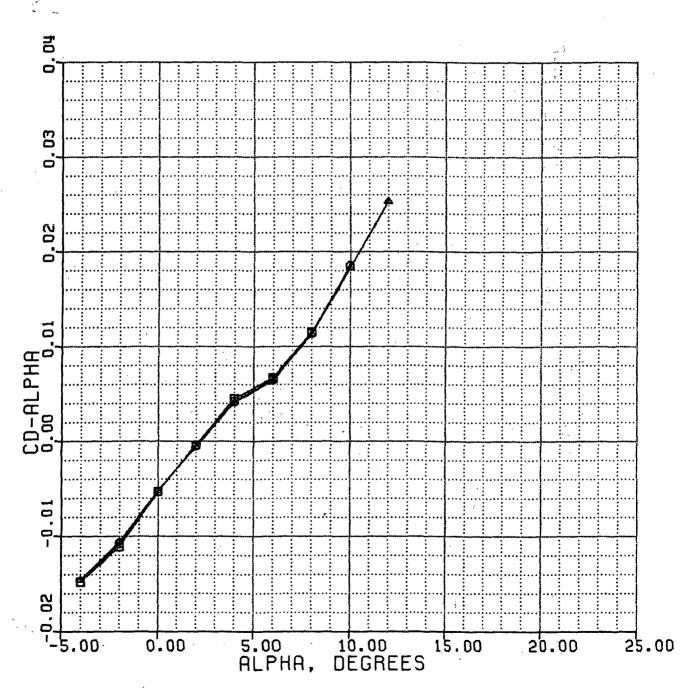
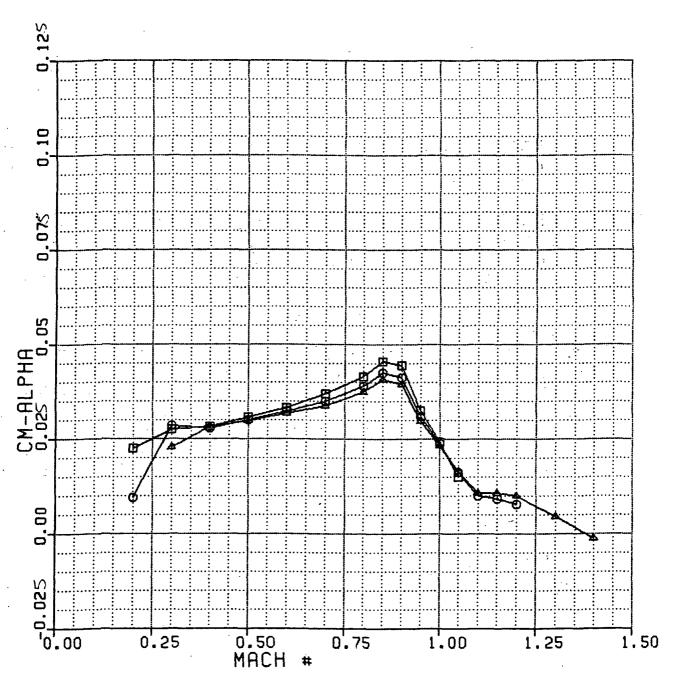


Figure 68(f)



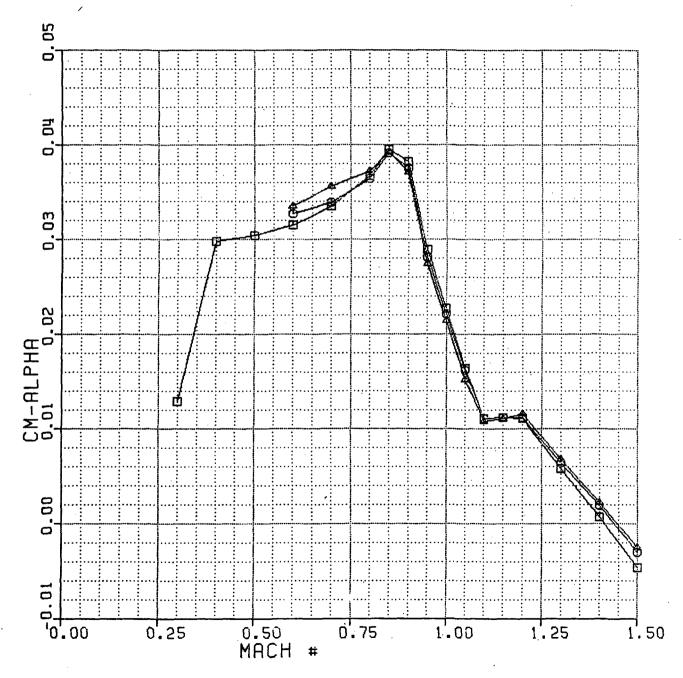


Figure 69(b)

CM-ALPHA VS ALPHA

6-15-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = S.L. ALP: -4 TO 22 P ALT = 10K ALP: -4 TO 22

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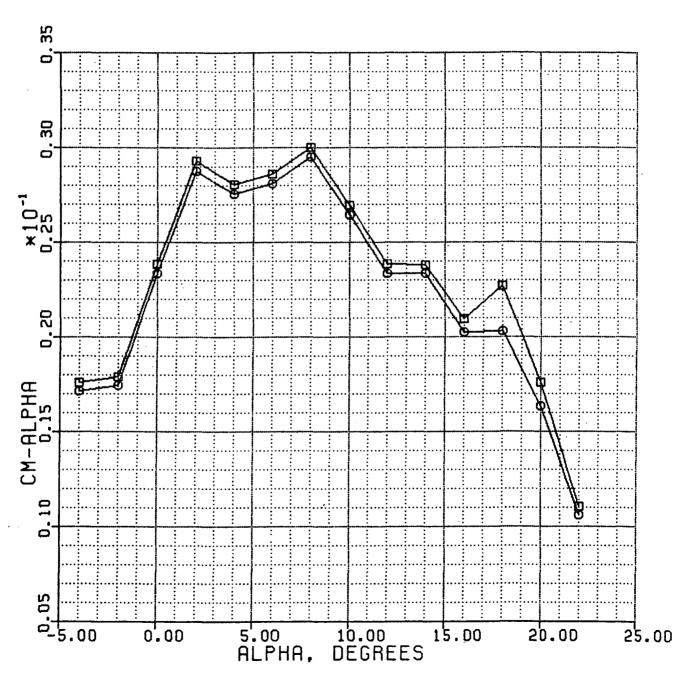


Figure 70(a)

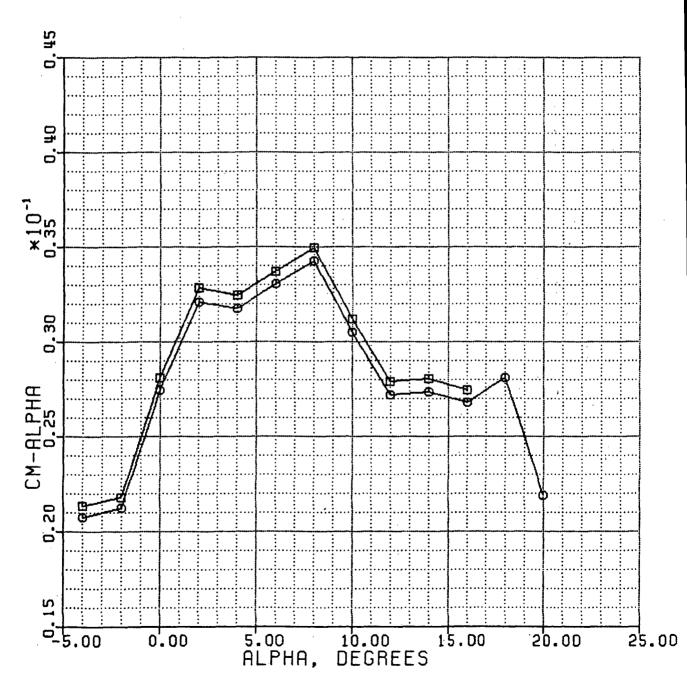


Figure 70(b)

CM-ALPHA VS ALPHA 6-17-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM B ALT = 10K ALP: 0 TO 10 C O ALT = 20K ALP: -4 TO 12 ALP = 30K ALP: -4 TO 14 ALP = 30K ALP: -4 TO 18 ALT = 40K ALP: -4 TO 18 OF POOR QUALITY ALT = 50K ALP: -4 TO 22

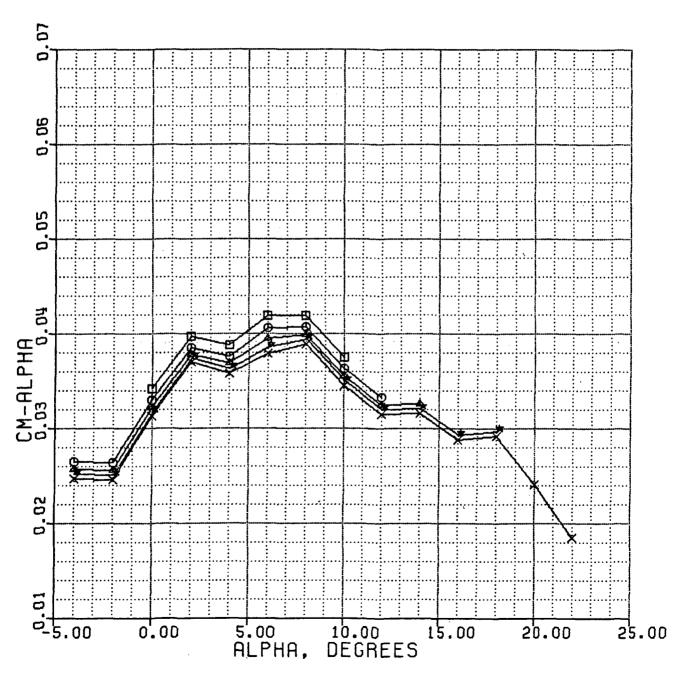


Figure 70(c)

CM-ALPHA VS ALPHA

7-1-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

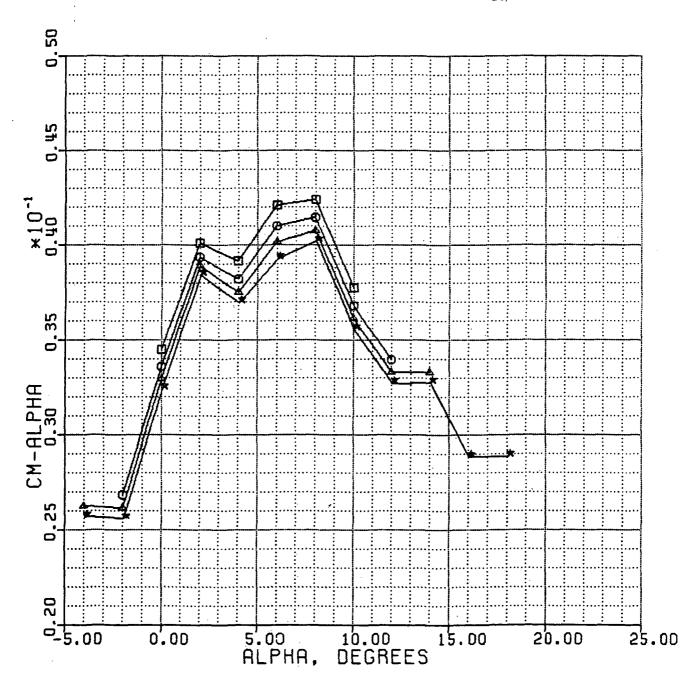


Figure 70(d)

```
CM-ALPHA VS ALPHA
7-1-83 X-29A M# = 1.2 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 20K ALP: -4 TØ 8

C ALT = 30K ALP: -4 TØ 10

ALT = 40K ALP: -4 TØ 12

ALT = 50K ALP: -4 TØ 14

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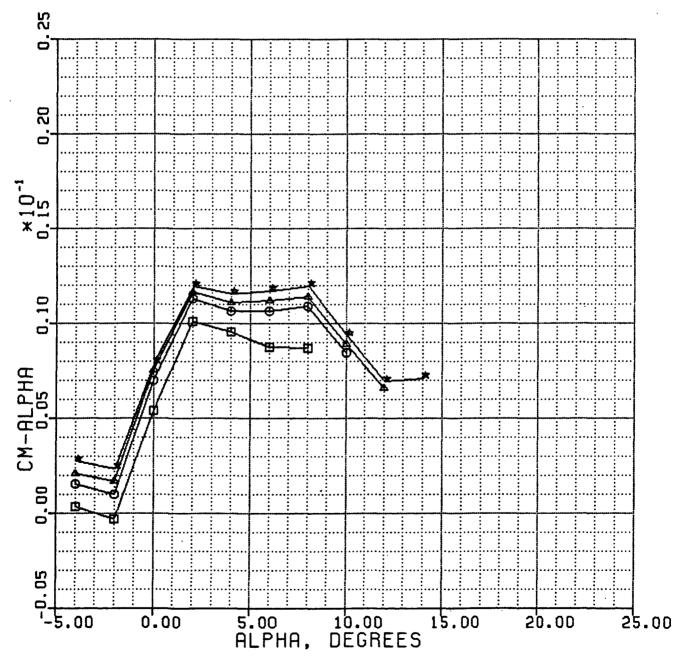


Figure 70(e)

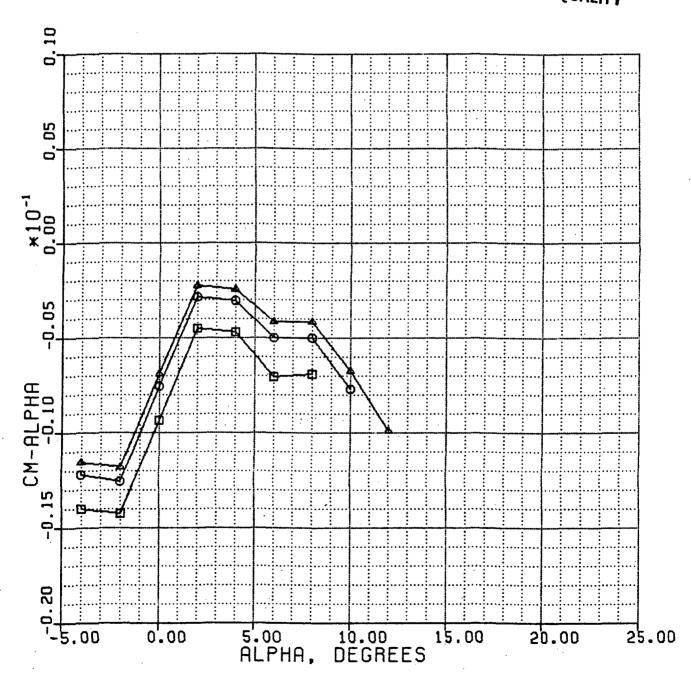


Figure 70(f)

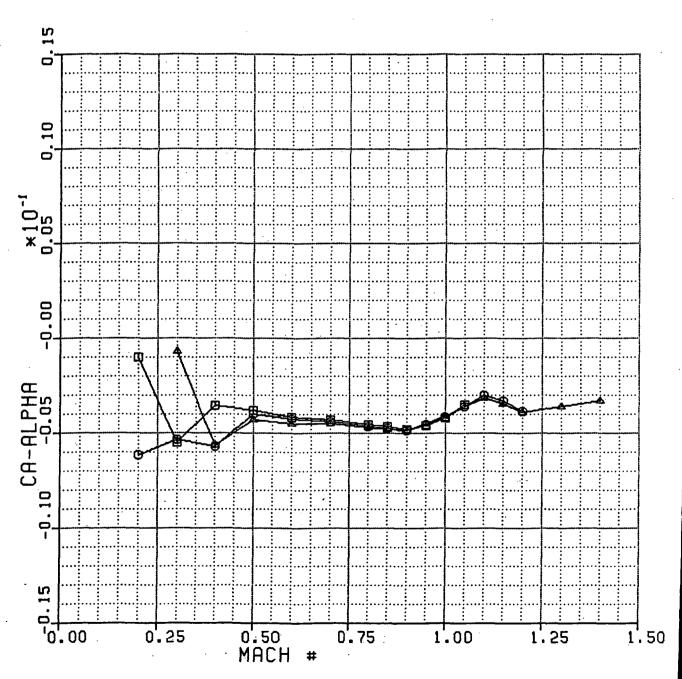
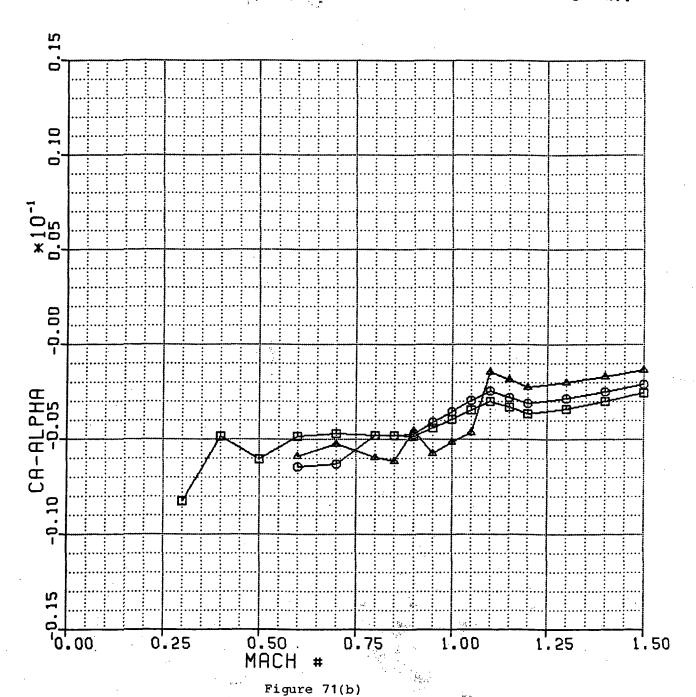


Figure 71(a)

CA-ALPHA VS MACH # 7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K



CA-ALPHA VS ALPHA 7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

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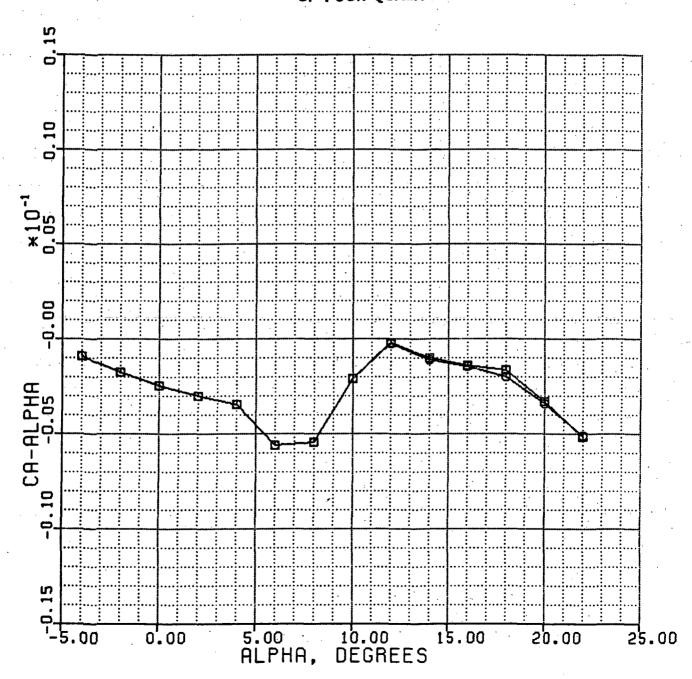


Figure 72(a)

CA-ALPHA VS ALPHA

7-26-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

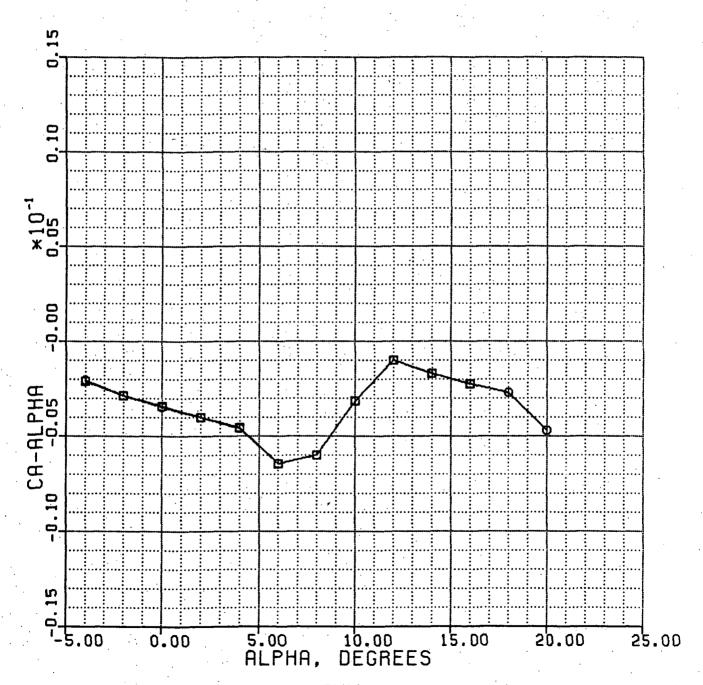


Figure 72(b)

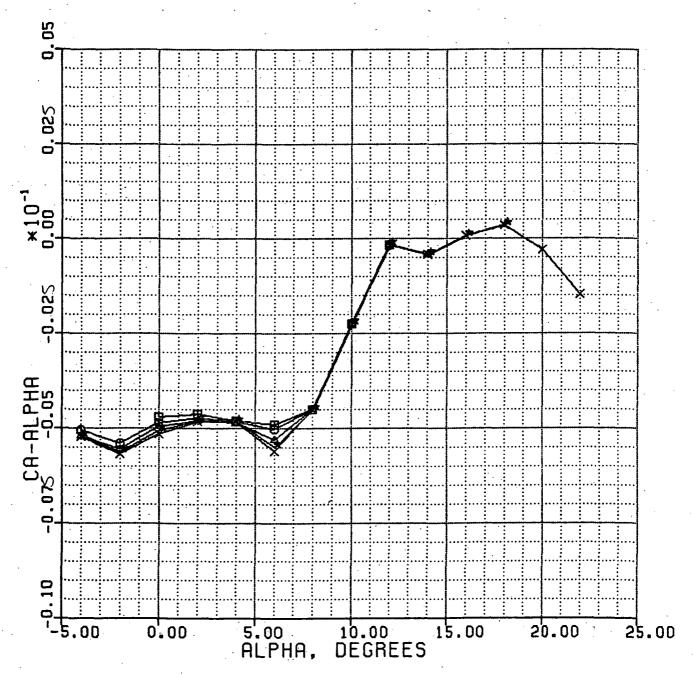


Figure 72(c)

CA-ALPHA VS ALPHA 7-1-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM P1 ALT = 20K ALP: 0 TO 10 _n ALT = 30K ALP: -2 TO 12

ALT = 40K ALP: -4 TO 14 ★ ALT = 50K ALP: -4 TO 18

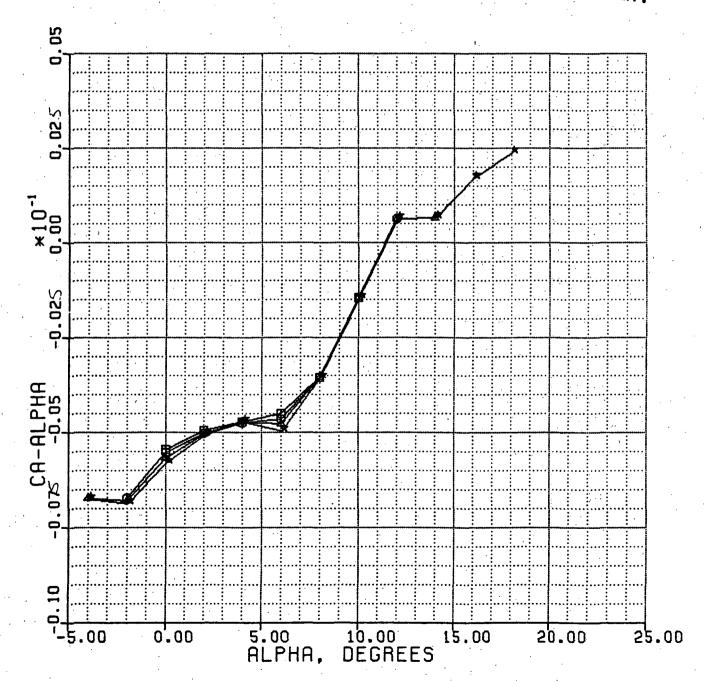


Figure 72(d)

CA-ALPHA VS ALPHA

7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

(CG = 451.0 WI = 15K HEFTH INI)

O PLT = 30K PLP: -4 TO 10

A PLT = 40K PLP: -4 TO 12

ALT = 40K ALP: -4 TO 12

★ ALT = 50K ALP: -4 TO 14

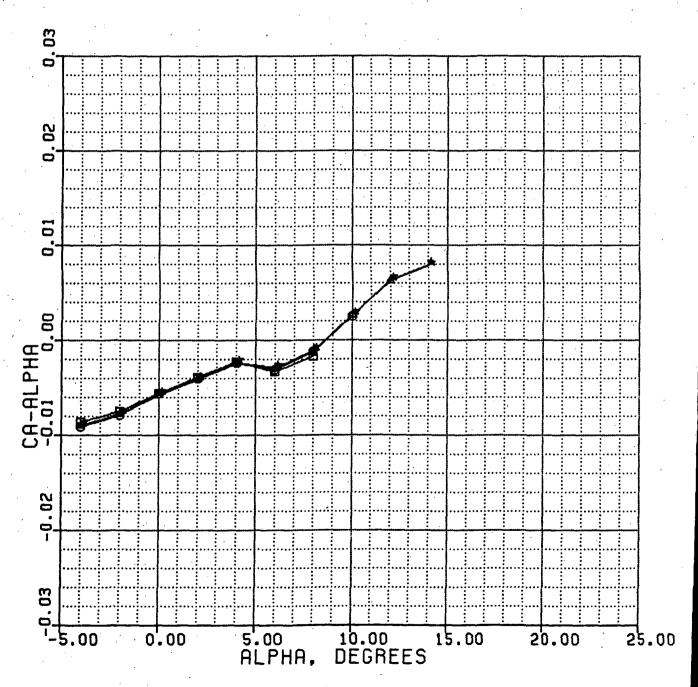


Figure 72(e)

CA-ALPHA VS ALPHA

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 30K ALP: -4 TO 8

P ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12

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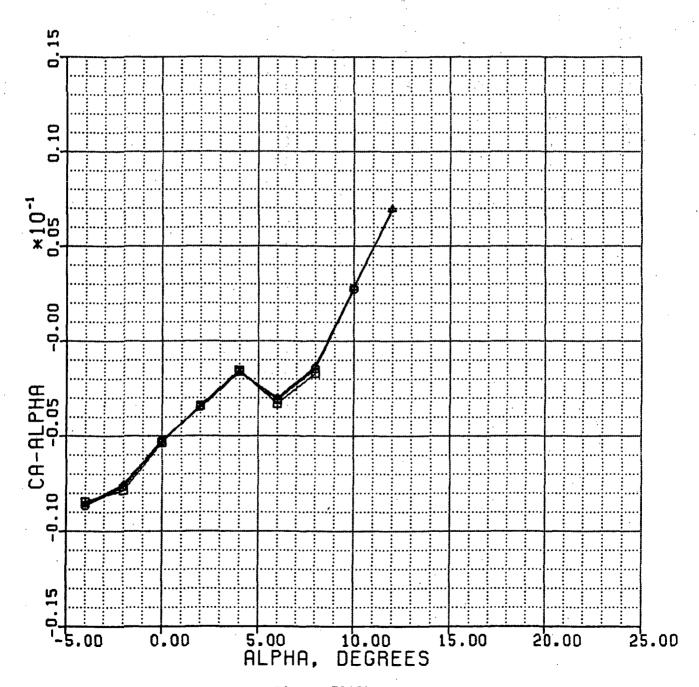


Figure 72(f)

CN-ALPHA VS MACH # 7-5-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

rg.....rg ALT = S.L. M# = .2 T0 1.05 $\overline{-0}$ ALT = 10K M# = .2 T0 1.2____ ALT = 20K M = .3 T0 1.4

and the second second

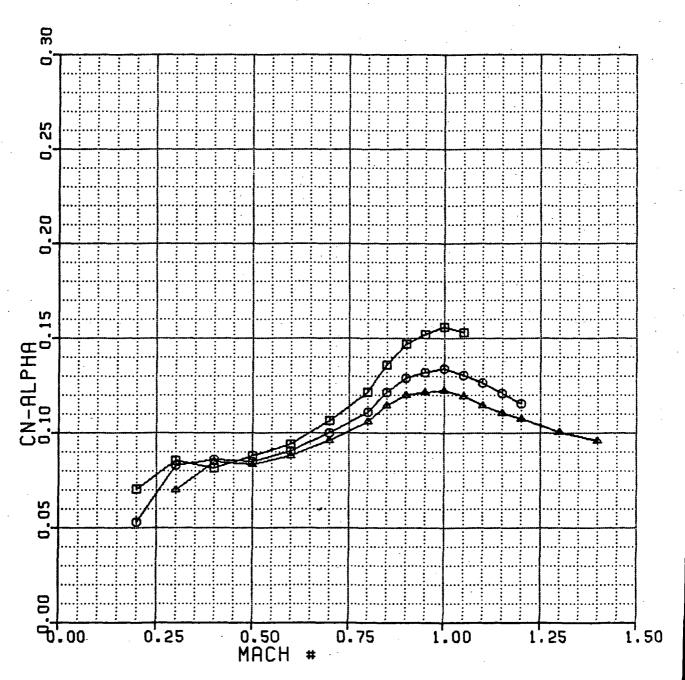


Figure 73(a)

CN-ALPHA VS MACH # 7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

1 4 N 16 17 1

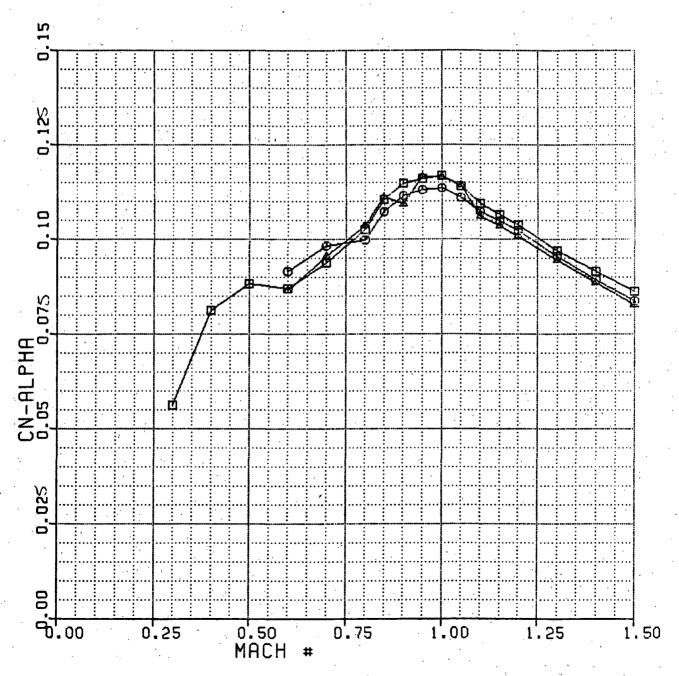


Figure 73(b)

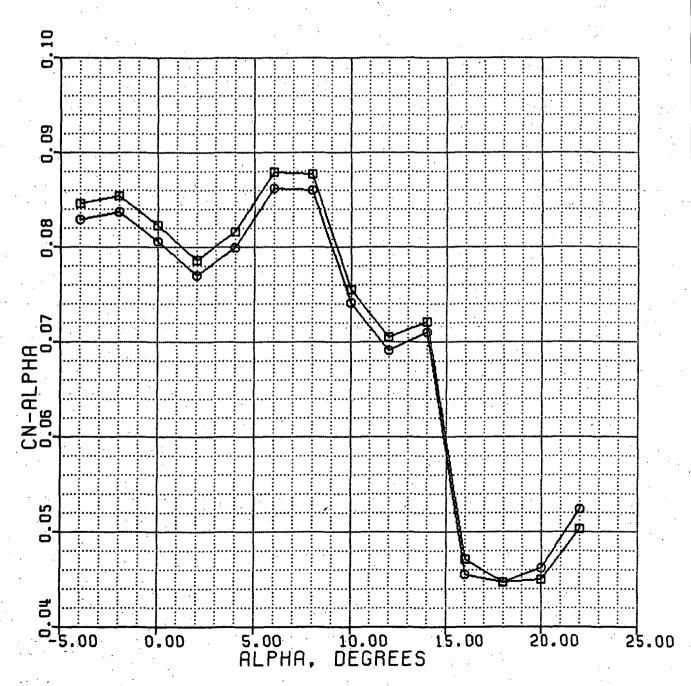


Figure 74(a)

CN-ALPHA VS ALPHA

6-16-83 X-29A M# = 0.6 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 10K ALP: -4 TO 16 0 ALT = 20K ALP: -4 TO 20

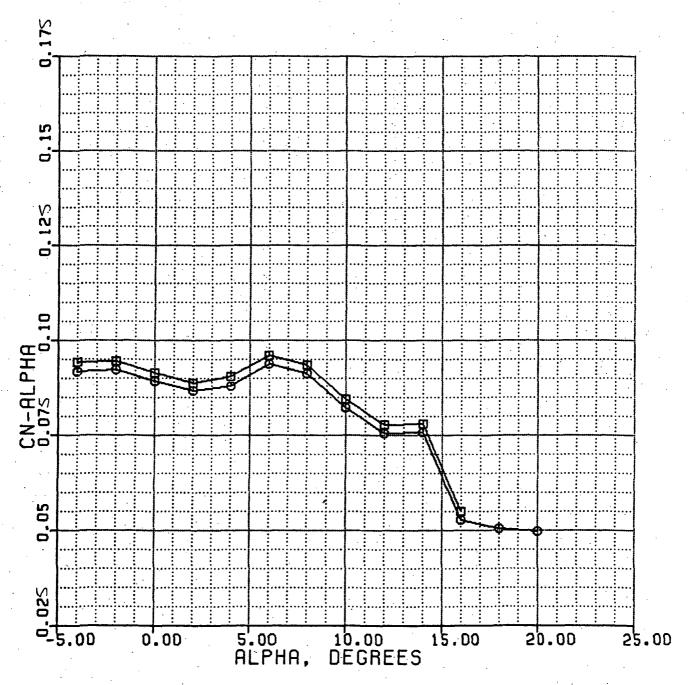


Figure 74(b)

CN-ALPHA VS ALPHA 6-17-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 T0 10
P ALT = 20K ALP: -4 T0 12
ALP = 30K ALP: -4 T0 14
ALP = 40K ALP: -4 T0 18
ALP: -4 T0 22
```

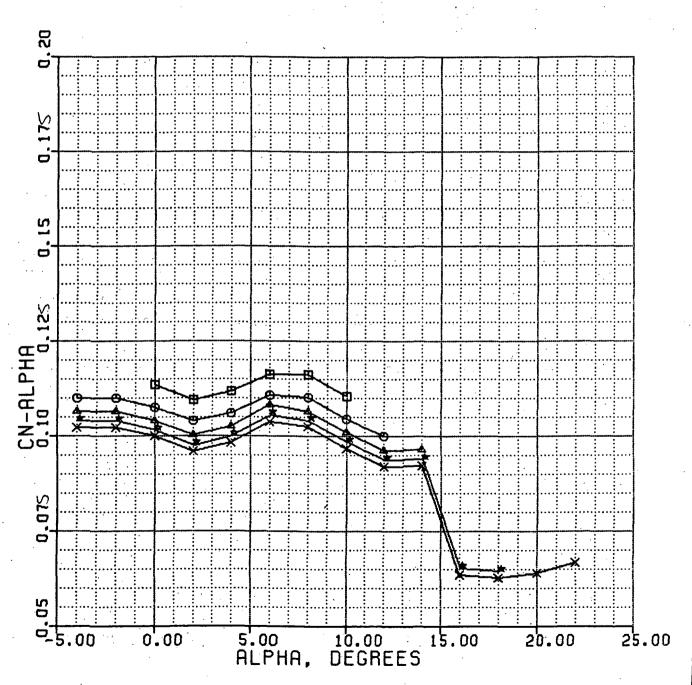


Figure 74(c)

```
CN-ALPHA VS ALPHA
7-1-83 X-29A M# = 0.9 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 20K ALP: 0 TO 10

ALT = 30K ALP: -2 TO 12

ALT = 40K ALP: -4 TO 14

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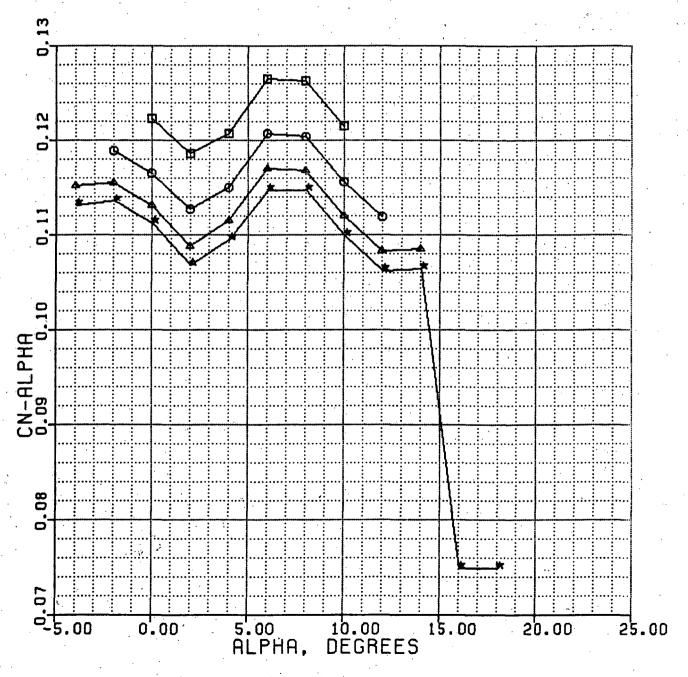
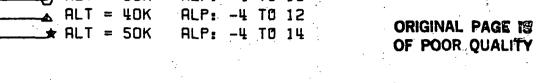


Figure 74(d)



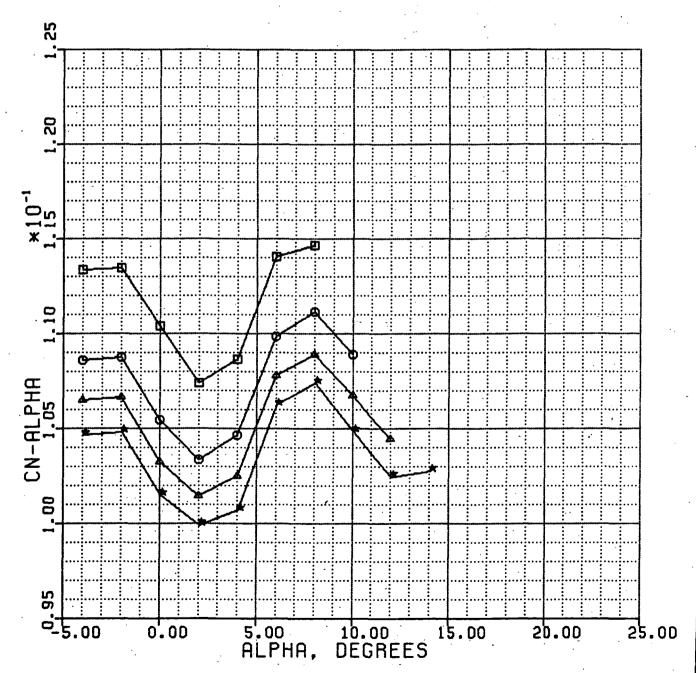


Figure 74(e)

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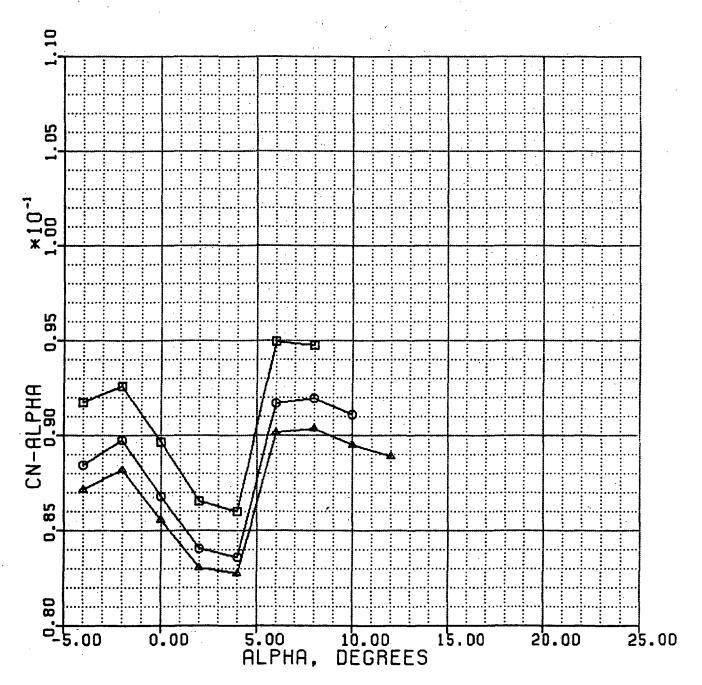


Figure 74(f)

Cy - BETA VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

g ALT = S.L. M# = .2 TO 1.05 g ALT = 10K M# = .2 TO 1.2 ALT = 20K M# = .3 TO 1.4

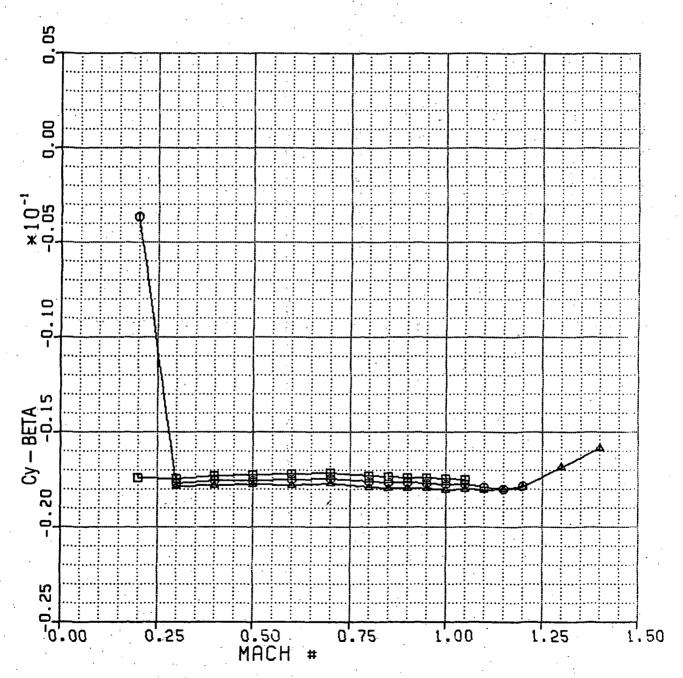


Figure 75(a)

Cy - BETA VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

THE COMMENTS.

9 ALT = 30K M# = .3 TO 1.5 9 ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

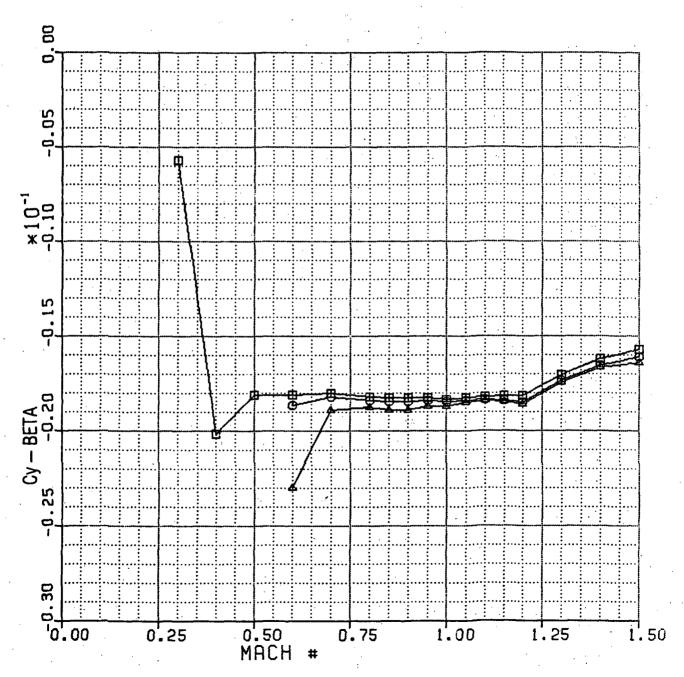


Figure 75(b)

Cy - BETA VS ALPHA

6-16-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

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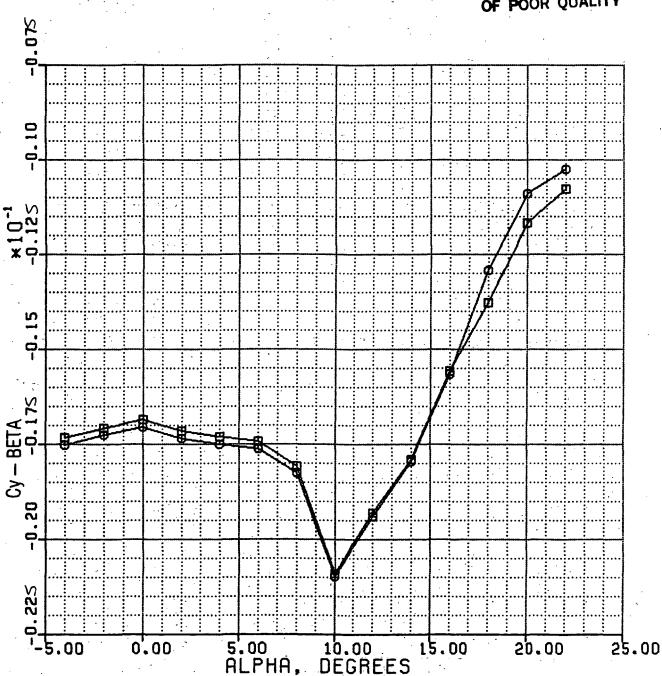


Figure 76(a)

Cy - BETA VS ALPHA

6-17-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

______ ALT = 10K ALP: -4 TO 16 ALP: -4 TO 20 ______ ALT = 20K

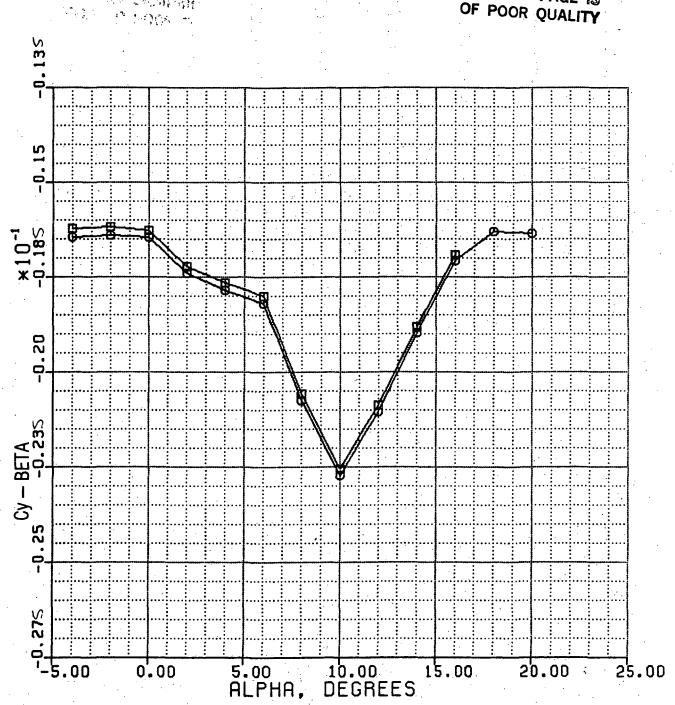


Figure 76(b)

Cy - BETA VS ALPHA

```
6-30-83 X-29A M# = 0.8 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM
```

```
P ALT = 10K ALP: 0 T0 10

P ALT = 20K ALP: -4 T0 12

A ALP = 30K ALP: -4 T0 14

A ALT = 40K ALP: -4 T0 18

A ALT = 50K ALP: -4 T0 22
```

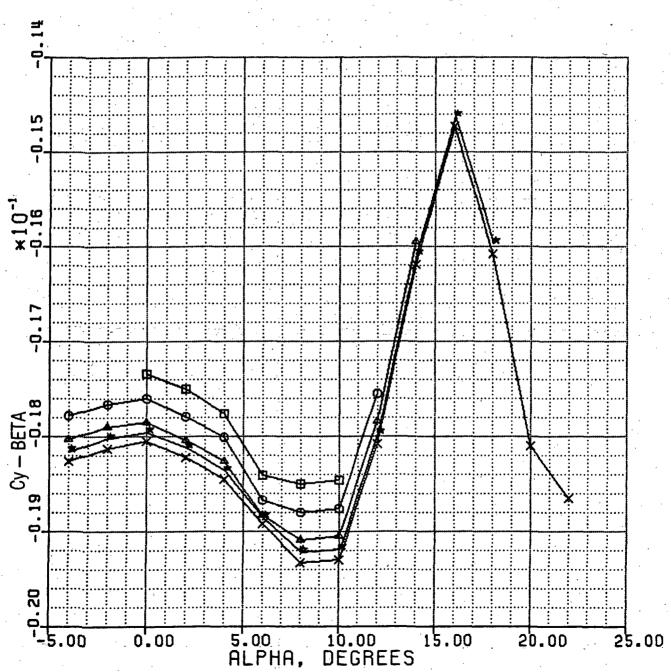


Figure 76(c)

```
7-1-83 X-29A M# = 0.9 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM
```

```
P ALT = 20K ALP: 0 TO 10

P ALT = 30K ALP: -2 TO 12

A ALT = 40K ALP: -4 TO 14

OF

A ALT = 50K ALP: -4 TO 18

OF
```

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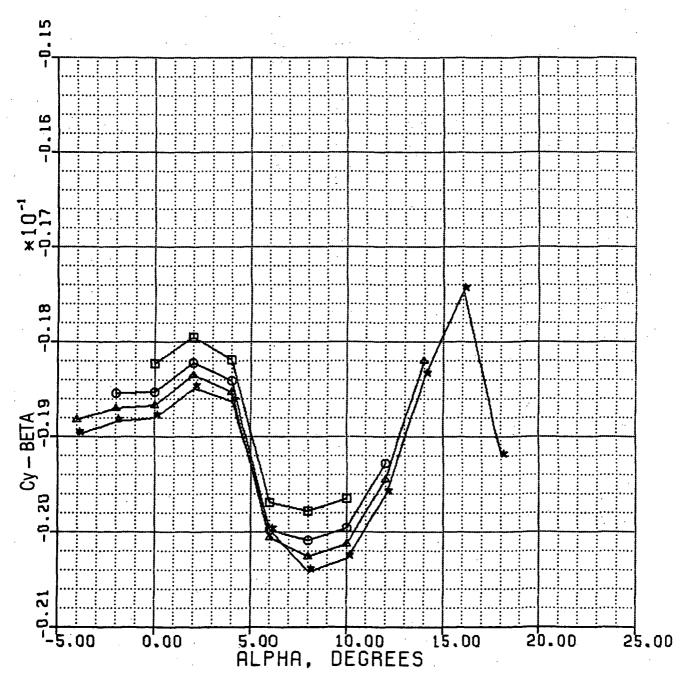


Figure 76(d)

C,

7-1-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
O ALT = 20K ALP: -4 TO 8
O O ALT = 30K ALP: -4 TO 10
A ALT = 40K ALP: -4 TO 12
A ALT = 50K ALP: -4 TO 14
```

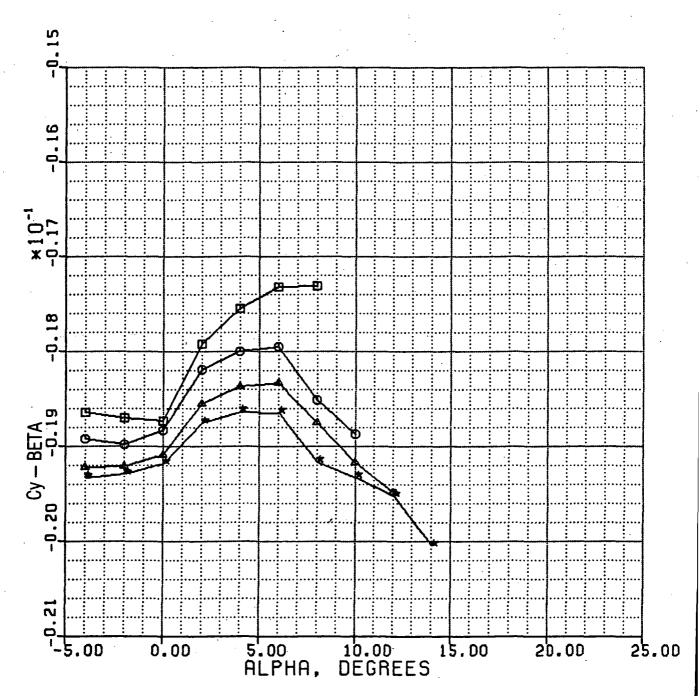


Figure 76(e)

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

O ALT = 30K ALP: -4 TO 8
O ALT = 40K ALP: -4 TO 10
A ALT = 50K ALP: -4 TO 12

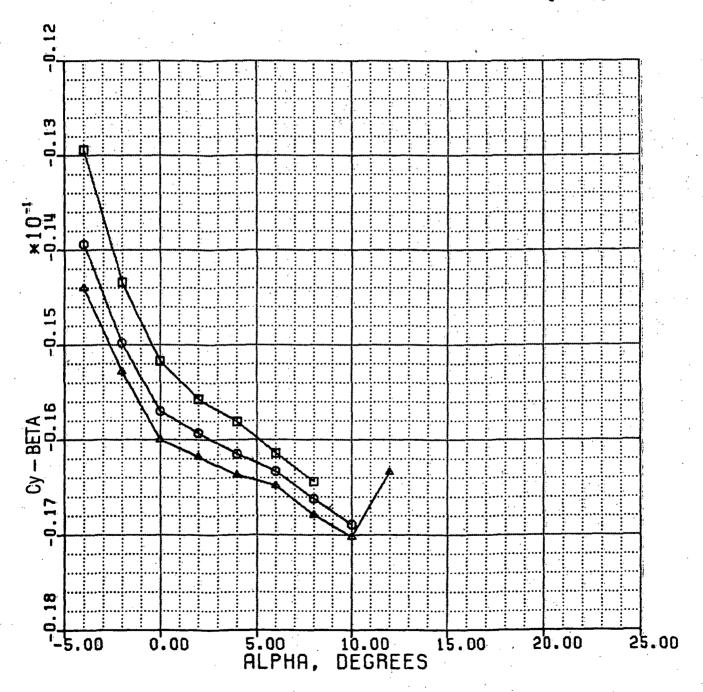


Figure 76(f)

CI - BETA VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

PALT = S.L. M# = .2 TO 1.05 PALT = 10K M# = .2 TO 1.2 ALT = 20K M# = .3 TO 1.4

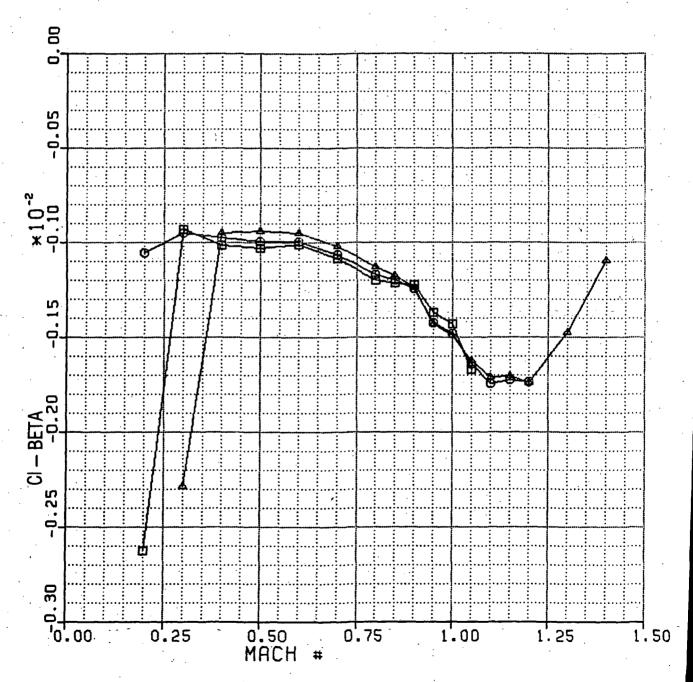


Figure 77(a)

CI - BETA VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 A ALT = 50K M# = .6 TO 1.5

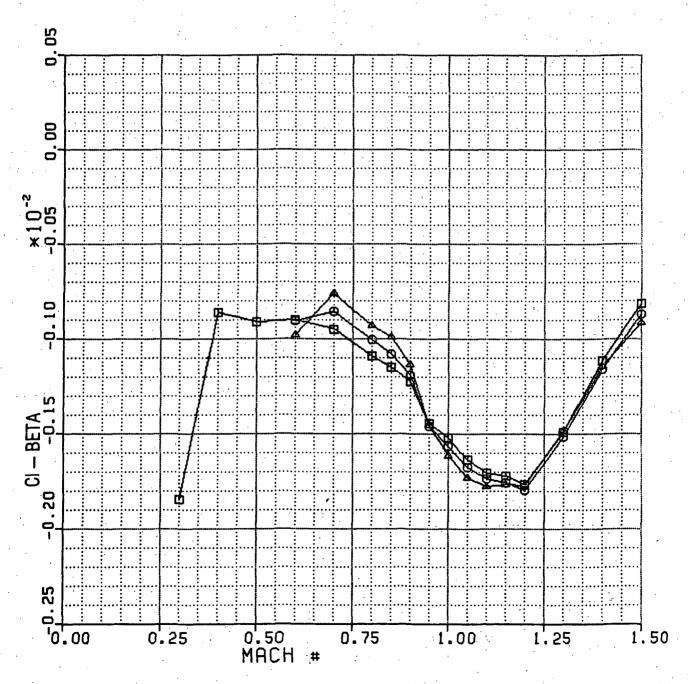


Figure 77(b)

6-16-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

Q ALT = S.L. ALP: -4 TO 22 Q ALT = 10K ALP: -4 TO 22

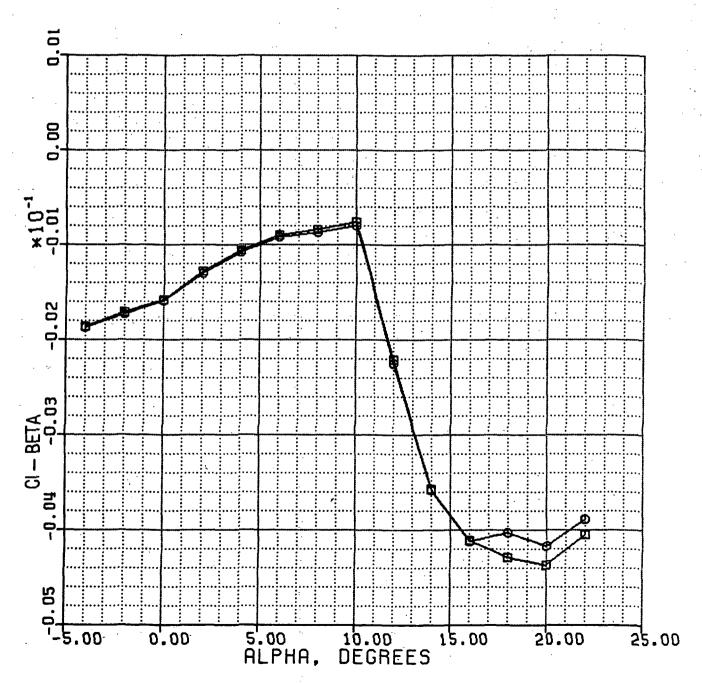


Figure 78(a)

6-17-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

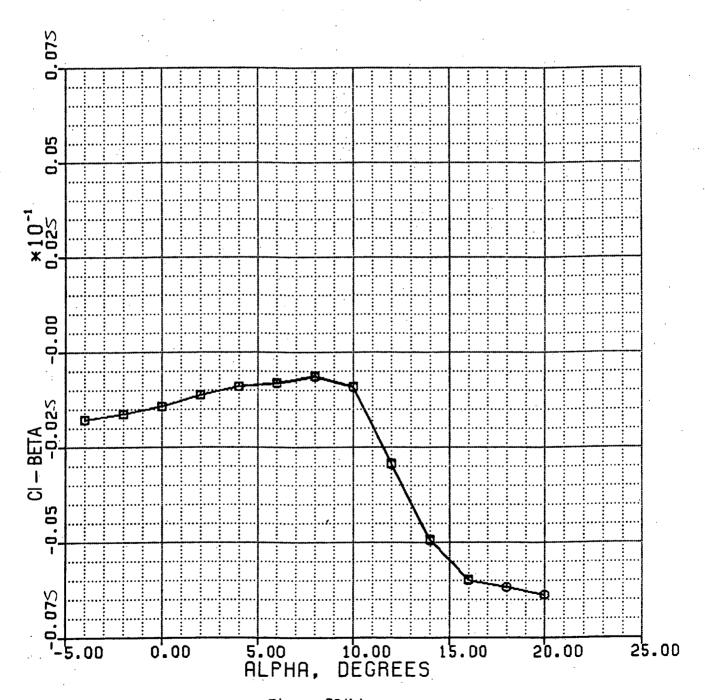


Figure 78(b)

6-30-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: 0 T0 10
P ALT = 20K ALP: -4 T0 12
A ALP = 30K ALP: -4 T0 14
A ALT = 40K ALP: -4 T0 18
A ALT = 50K ALP: -4 T0 22

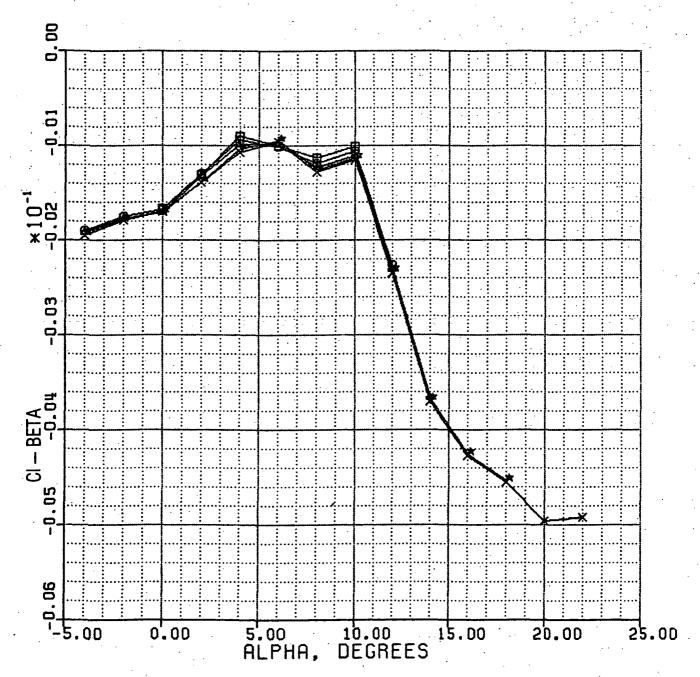


Figure 78(c)

7-1-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

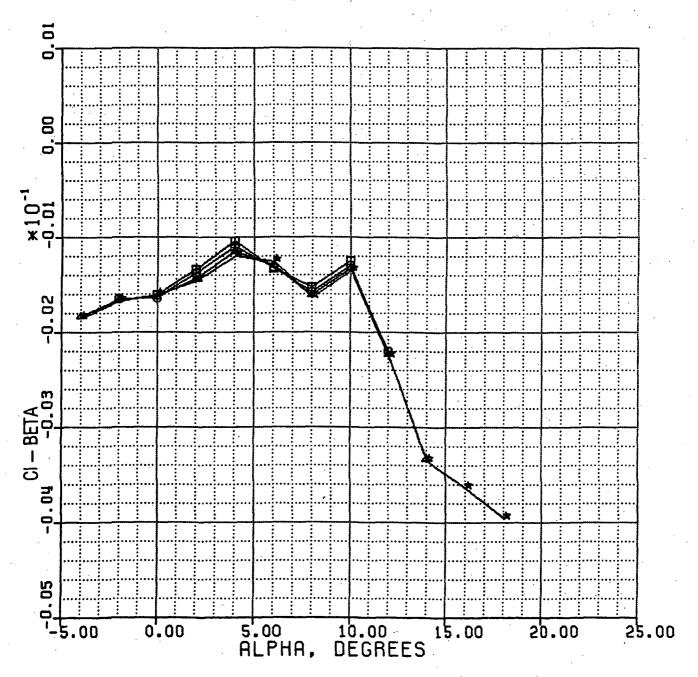


Figure 78(d)

7-1-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

ALT = 40K ALP: -4 TO 12

ALT = 50K ALP: -4 TO 14
```

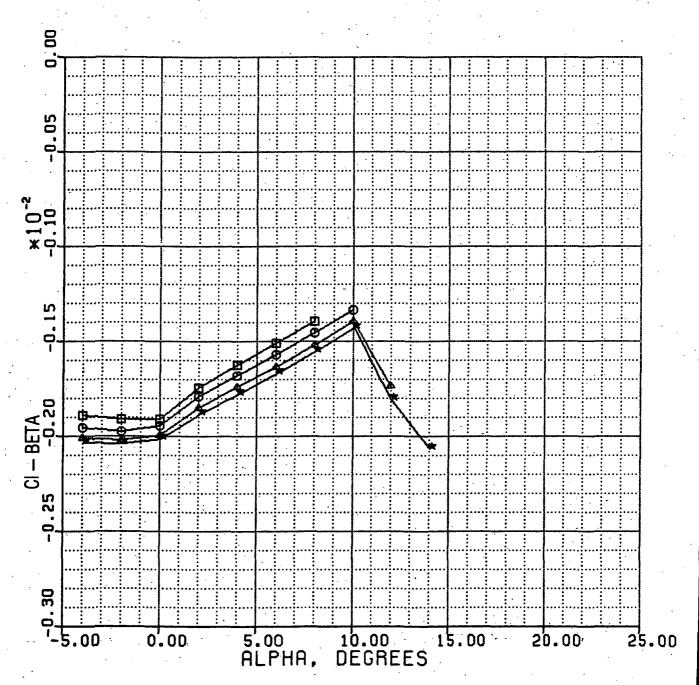


Figure 78(e)

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7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

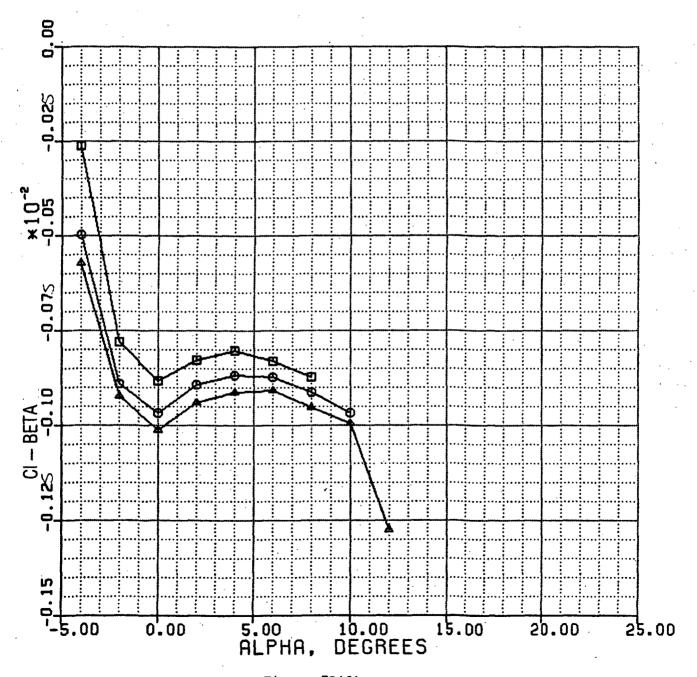


Figure 78(f)

Cn - BETA VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

PALT = S.L. M# = .2 TO 1.05

PALT = 10K M# = .2 TO 1.2

A RLT = 20K M# = .3 TO 1.4

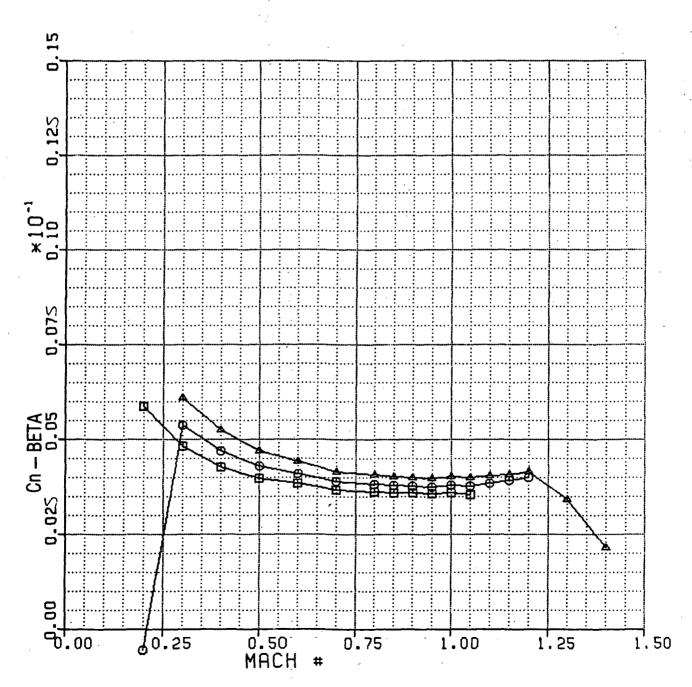


Figure 79(a)

Cn - BETA VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

PALT = 30K M# = .3 TO 1.5 PALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

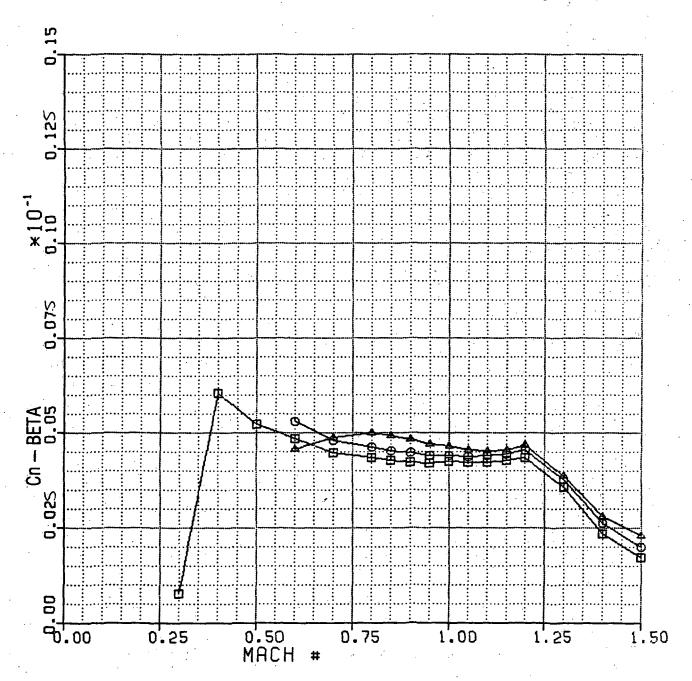


Figure 79(b)

6-16-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

D ALT = S.L. ALP: -4 TO 22 D ALT = 10K ALP: -4 TO 22

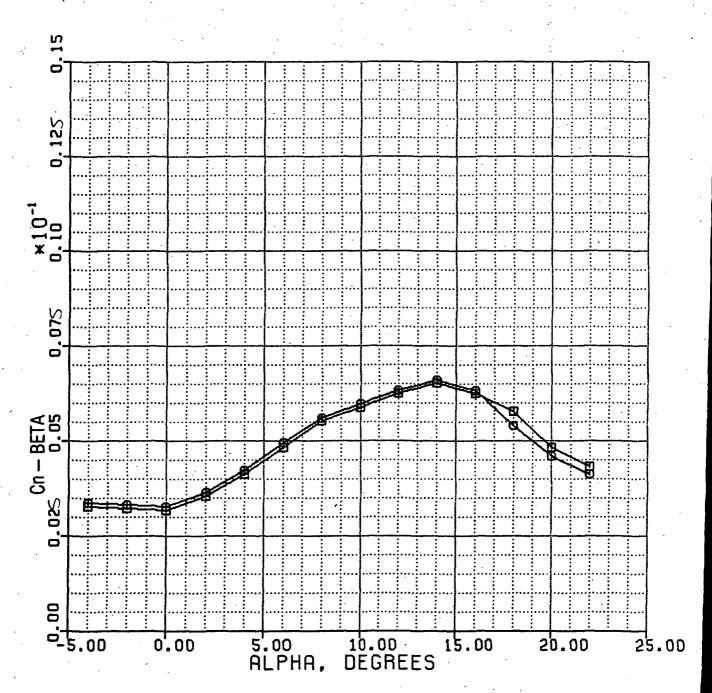


Figure 80(a)

6-17-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

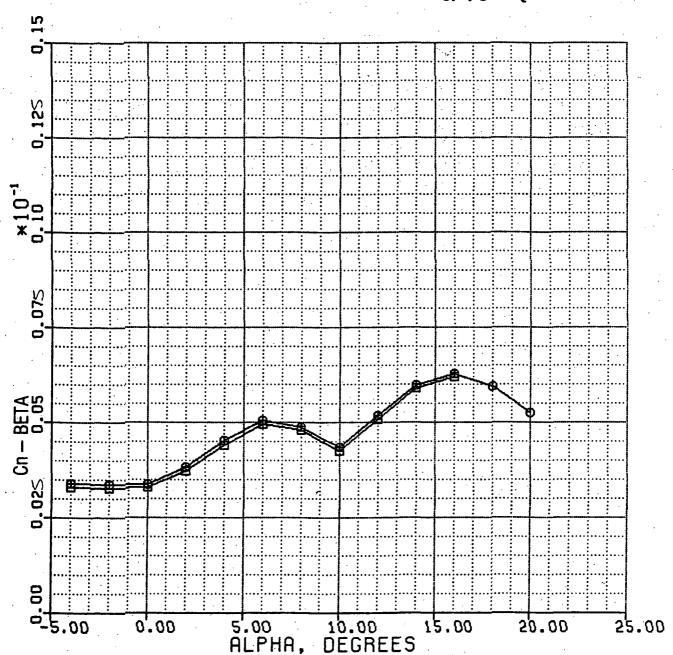


Figure 80(b)

6-30-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALP = 30K ALP: -4 TO 14

A ALT = 40K ALP: -4 TO 18

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A ALT = 50K ALP: -4 TO 22

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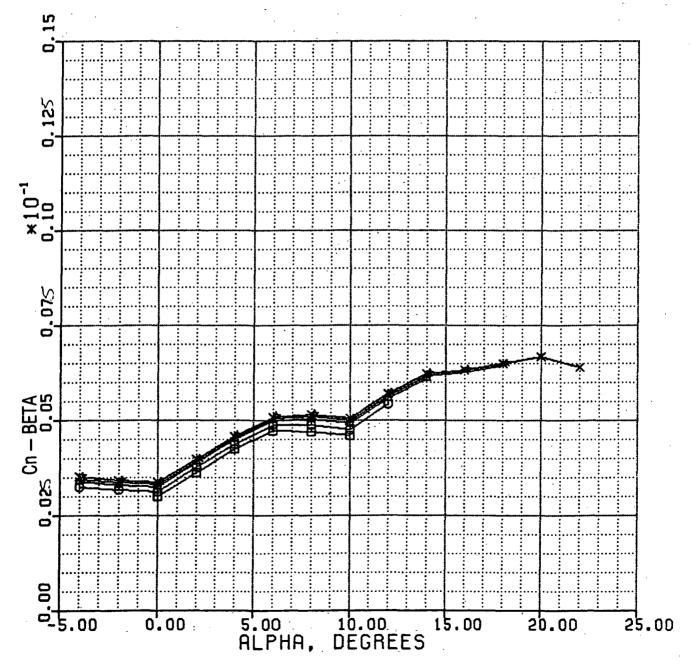


Figure 80(c)

```
7-1-83 X-29A M# = 0.9 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM
```

```
9 ALT = 20K ALP: 0 T0 10

9 ALT = 30K ALP: -2 T0 12

A ALT = 40K ALP: -4 T0 14

A ALT = 50K ALP: -4 T0 18
```

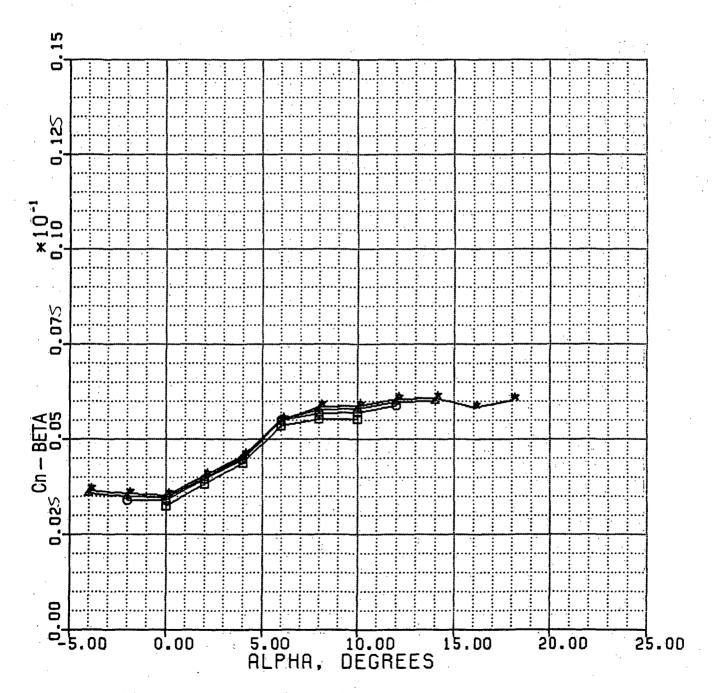


Figure 80(d)

7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
PALT = 20K ALP: -4 TO 8

PALT = 30K ALP: -4 TO 10

ALT = 40K ALP: -4 TO 12

ALT = 50K ALP: -4 TO 14
```

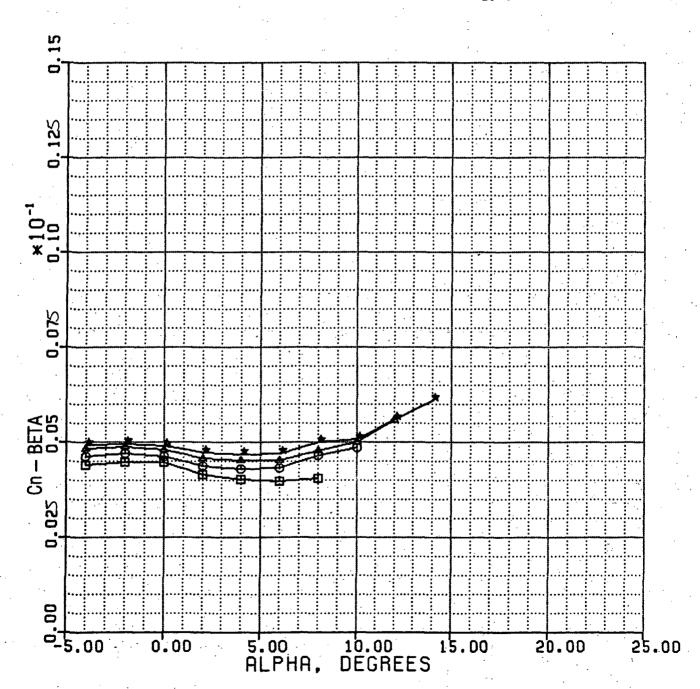


Figure 80(e)

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8

9 ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12

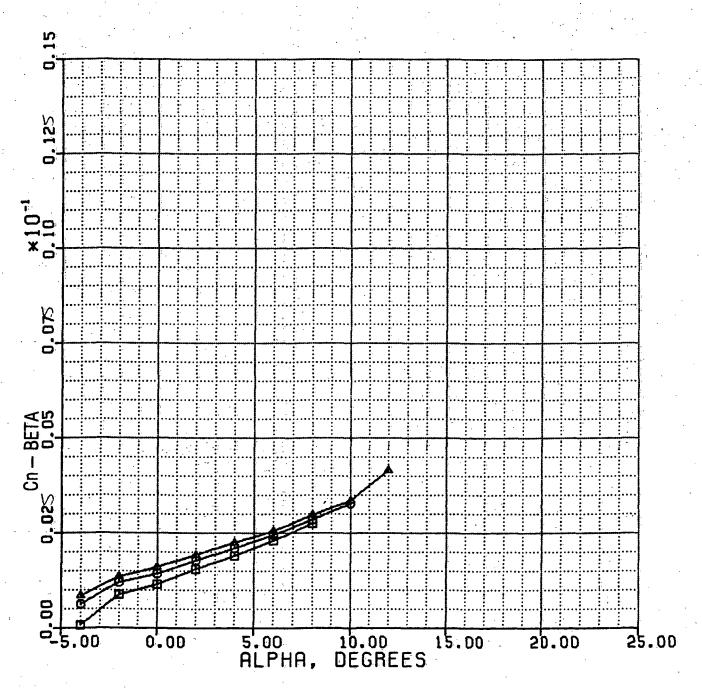


Figure 80(f)

Cn — BETA DYNAMIC VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MCDE XCG = 451.0 WT = 15K

PALT = S.L. M# = .2 TO 1.05 PALT = 10K M# = .2 TO 1.2 ALT = 20K M# = .3 TO 1.4

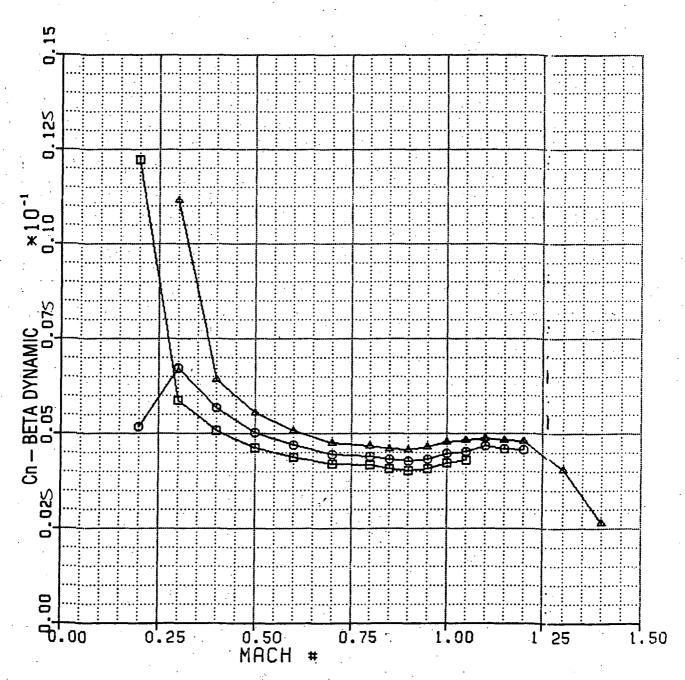


Figure 81(a)

Cn — BETA DYNAMIC VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

CARRY AND

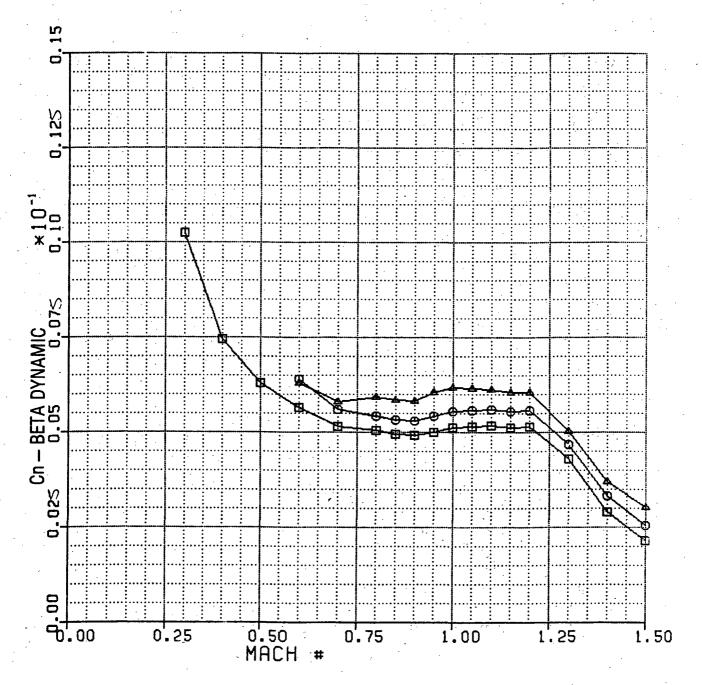


Figure 81(b)

7-26-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

n = 5.L. ALP: -4 TO 22 n = 10K ALP: -4 TO 22

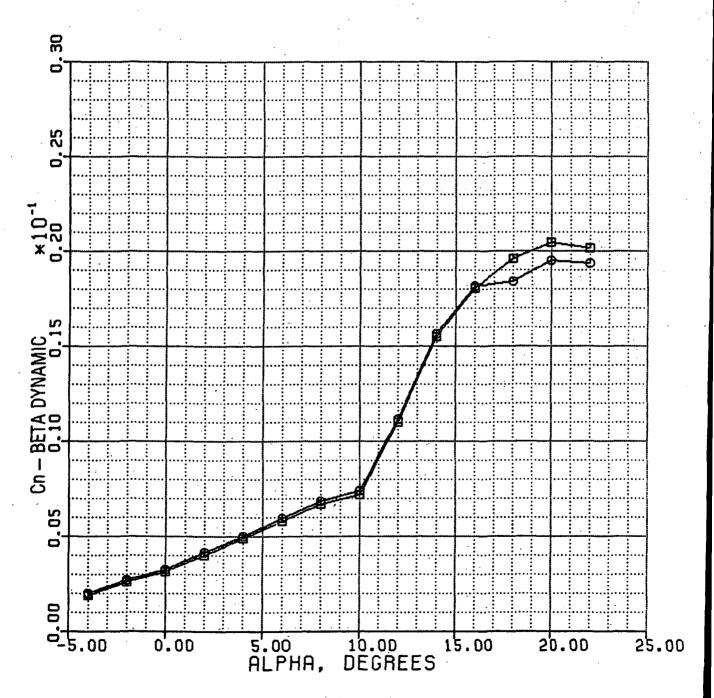


Figure 82(a)

7-26-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

D ALT = 10K ALP: -4 TO 16 D ALT = 20K ALP: -4 TO 20

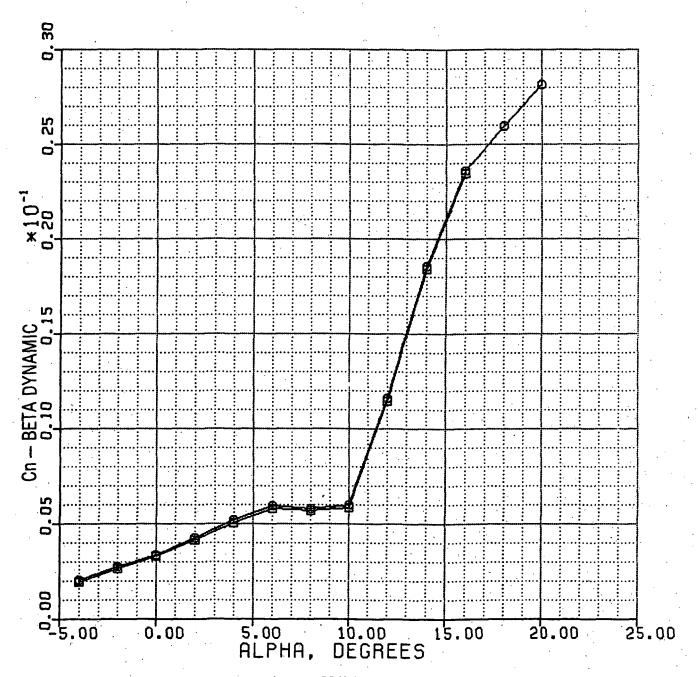


Figure 82(b)

7-27-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 T0 10
P ALT = 20K ALP: -4 T0 12
A ALT = 30K ALP: -4 T0 14
A ALT = 40K ALP: -4 T0 18
A ALT = 50K ALP: -4 T0 22
```

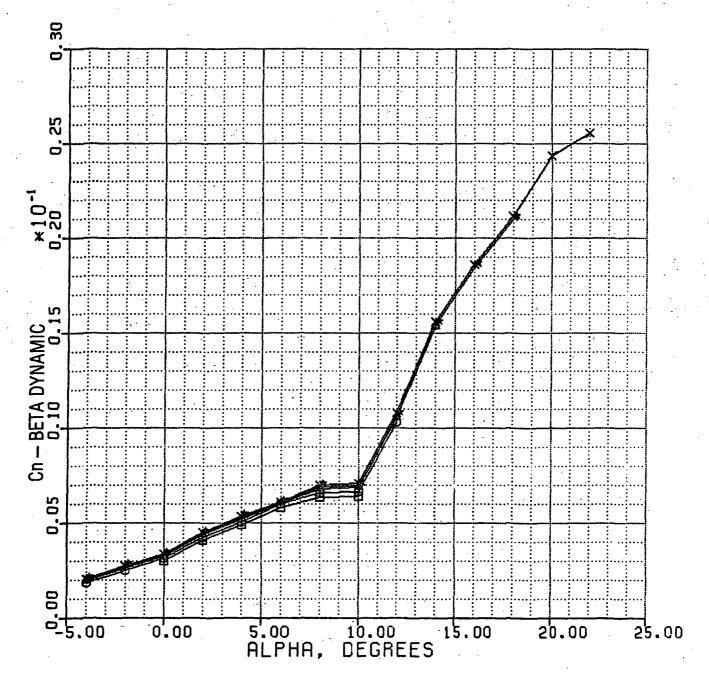


Figure 82(c)

7-27-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

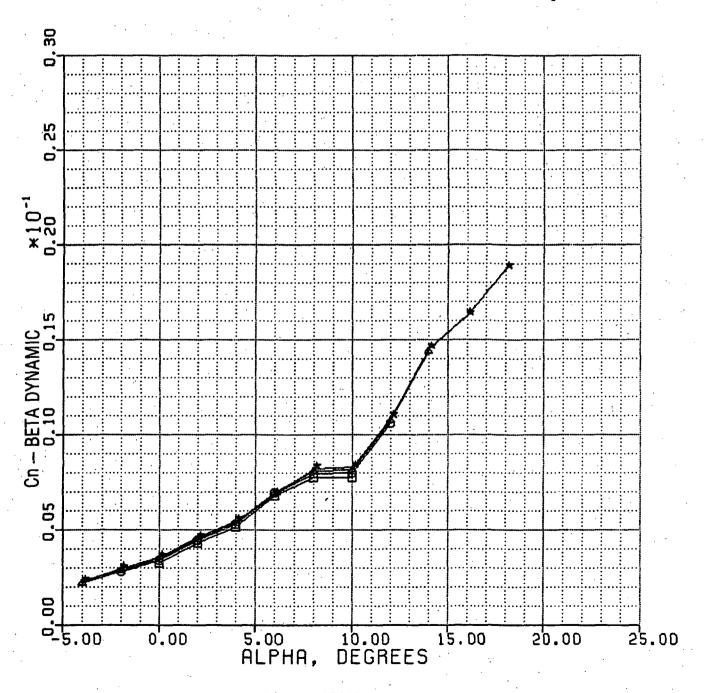
```
P ALT = 20K ALP: 0 TO 10

P ALT = 30K ALP: -2 TO 12

A ALT = 40K ALP: -4 TO 14

A ALT = 50K ALP: -4 TO 18
```

1 M. Down



7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

O O ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

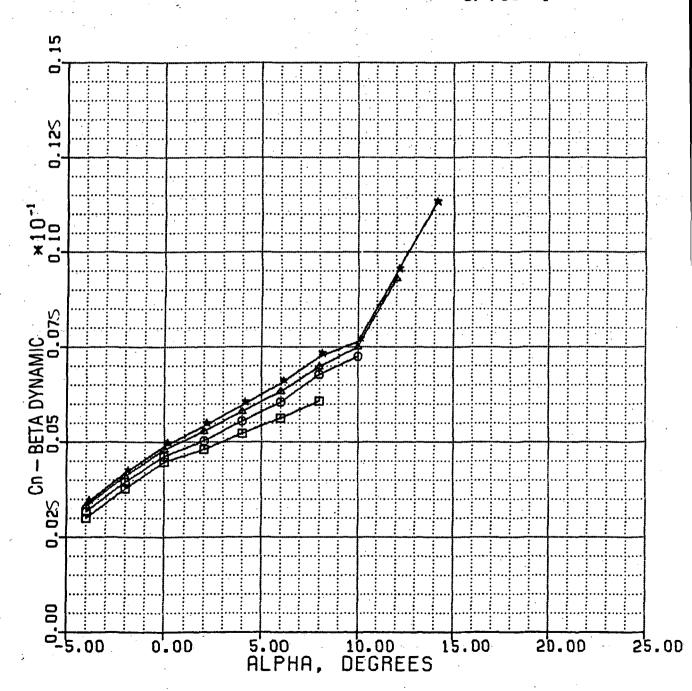


Figure 82(e)

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

BLT = 30K ALP: -4 TO 8

BLT = 40K ALP: -4 TO 10

ALT = 50K ALP: -4 TO 12

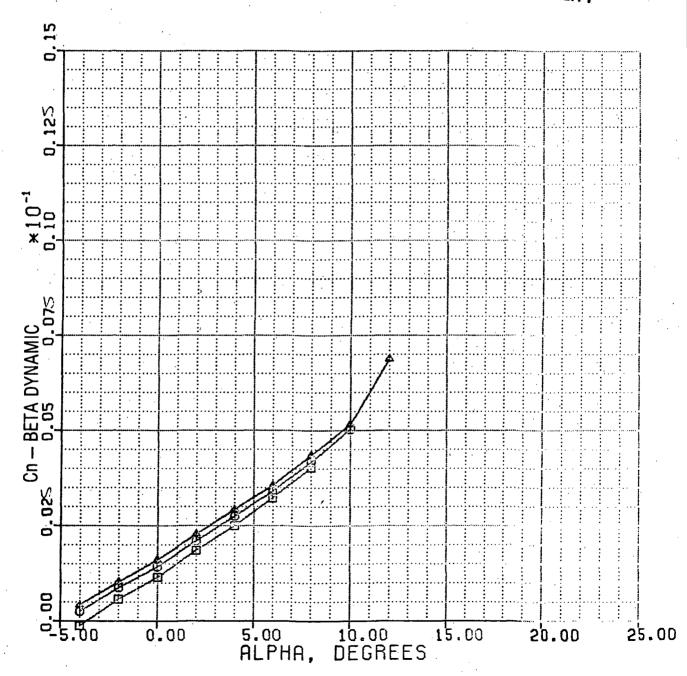


Figure 82(f)

CL-ALPHA DØT VS MACH # 7-6-83 X-29A 1-G TRIM NØRMAL MØDE XCG = 451.0 WT = 15K

O ALT = S.L. M# = .2 TO 1.05 O ALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4

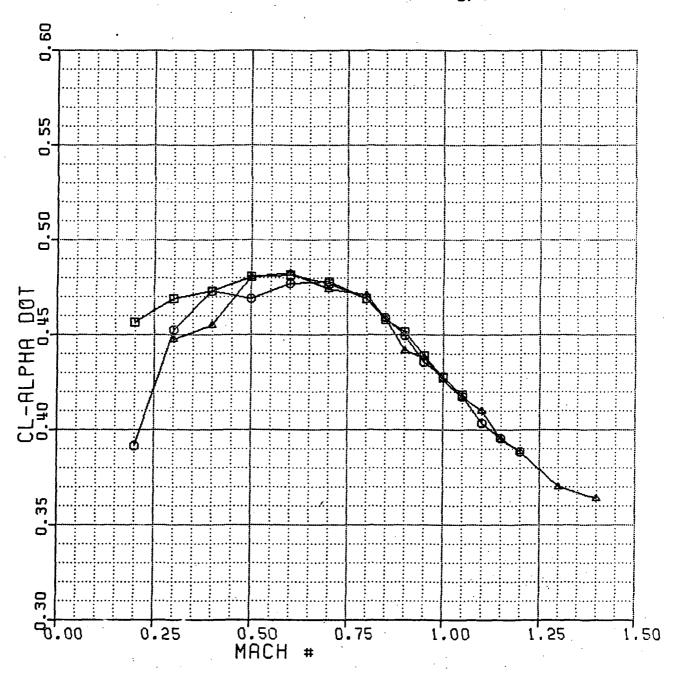


Figure 83(a)

```
CL-ALPHA DOT VS MACH #
7-7-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B ALT = 30K M# = .3 TO 1.5

CHAPHA DOT VS MACH #

7-7-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

B ALT = 50K M# = .6 TO 1.5
```

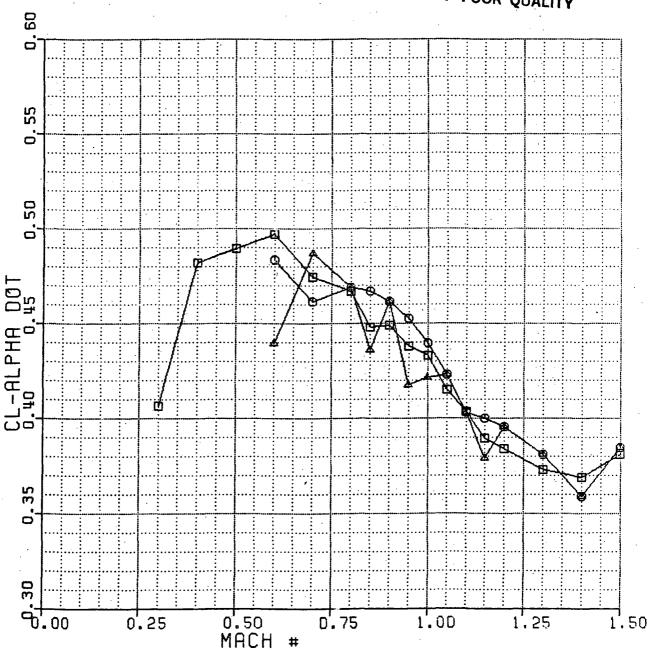
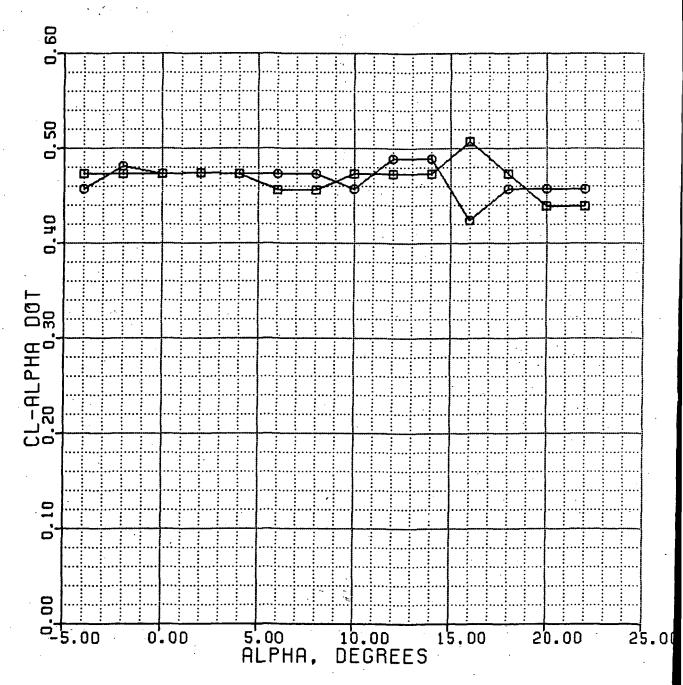
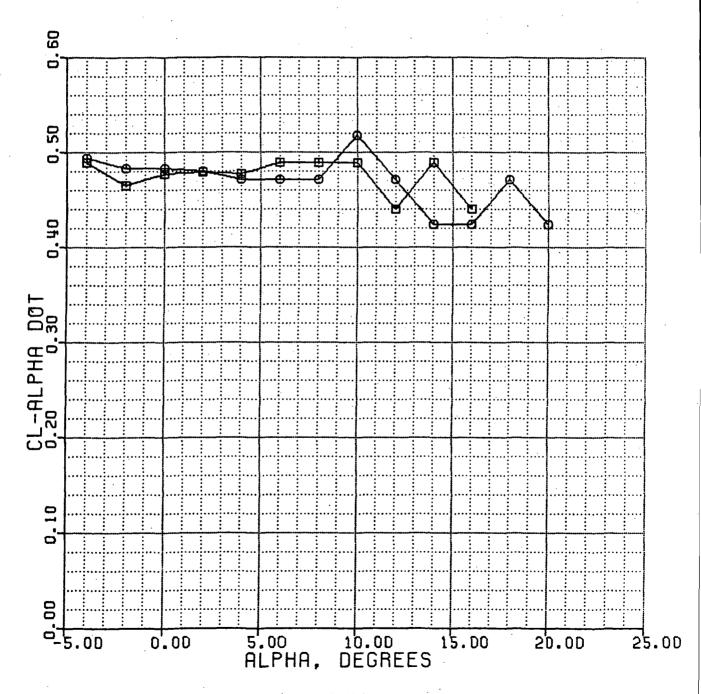


Figure 83(b)

CL-ALPHA DOT VS ALPHA 7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM





CL-ALPHA DØT VS ALPHA

7-26-83 X-29A M# = 0.8 NØRMAL MØDE XCG = $\frac{1}{4}51.0$ WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 TO 10
P ALT = 20K ALP: -4 TO 12
A ALT = 30K ALP: -4 TO 14
ALT = 40K ALP: -4 TO 18
ALT = 50K ALP: -4 TO 22
```

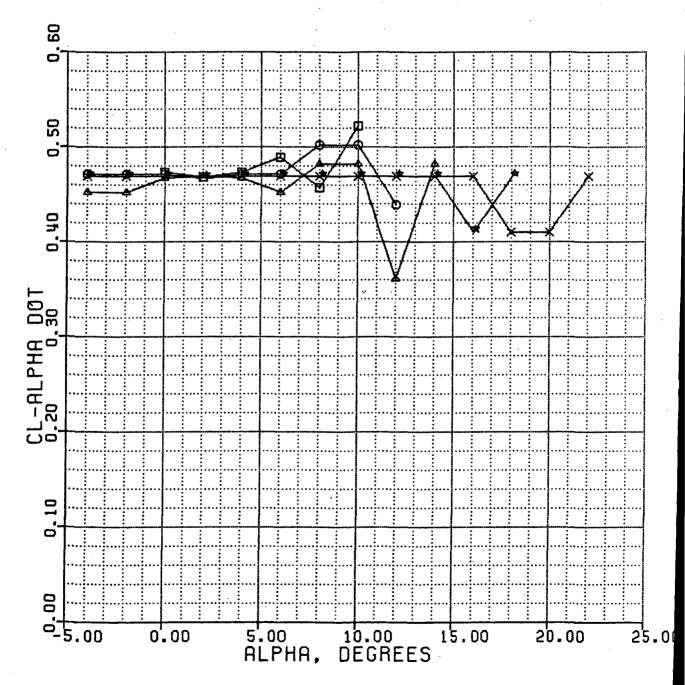


Figure 84(c)

CL-ALPHA DØT VS ALPHA

7-27-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
9 ALT = 20K ALP: 0 TO 10

9 ALT = 30K ALP: -2 TO 12

A ALT = 40K ALP: -4 TO 14

A ALT = 50K ALP: -4 TO 18
```

The state of the state of

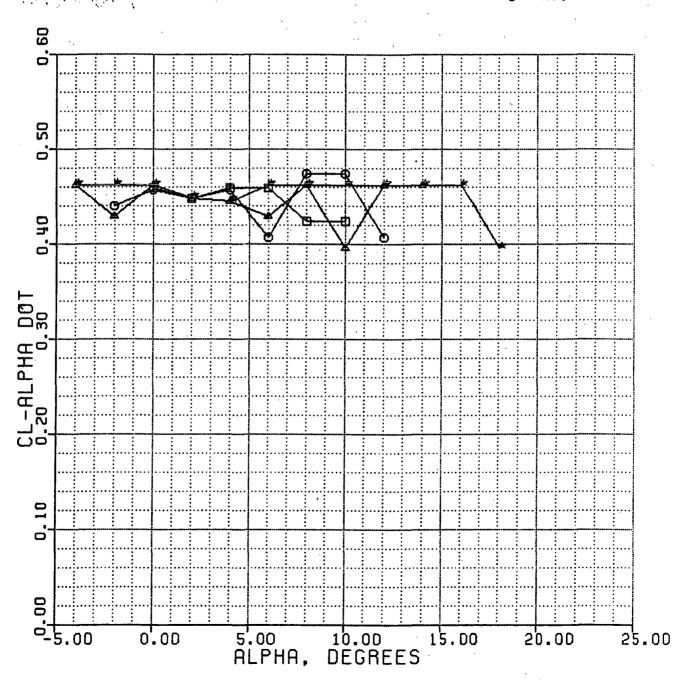


Figure 84(d)

CL-ALPHA DØT VS ALPHA

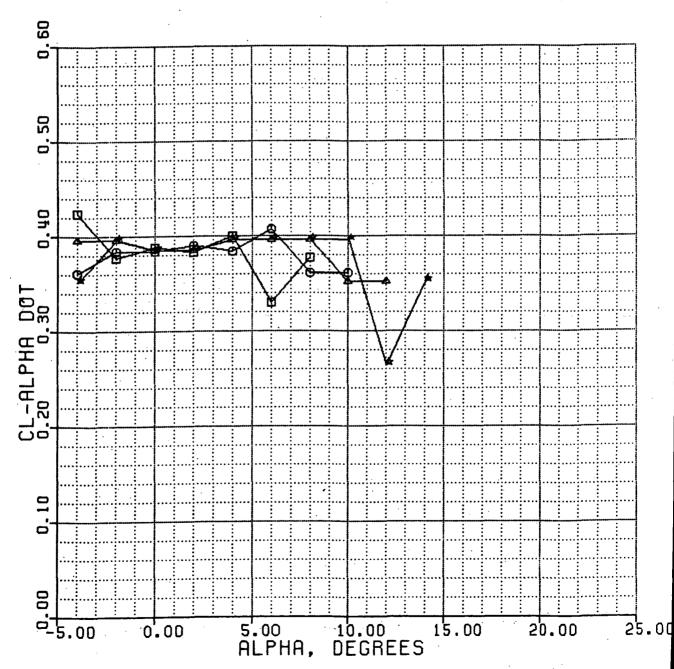
7-27-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

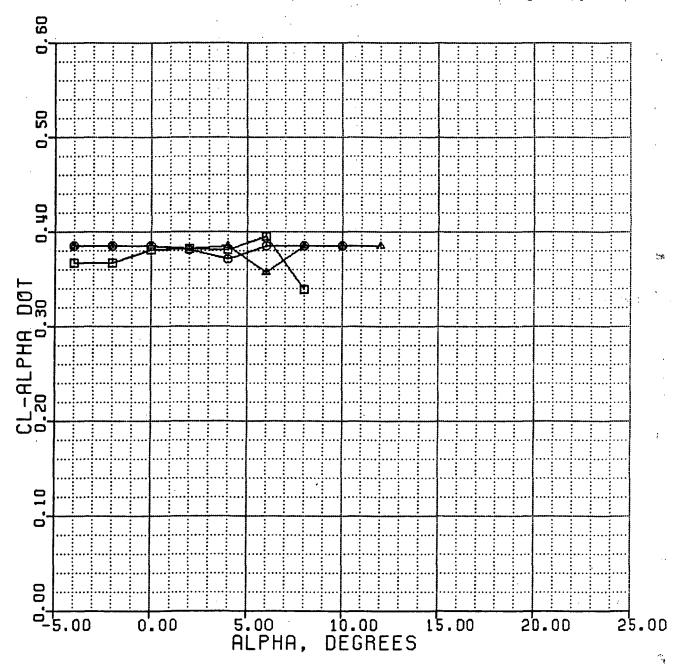
A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```



CL-ALPHA DØT VS ALPHA 7-27-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM B-B ALT = 30K ALP: -4 TØ B

O ALT = 30K ALP: -4 TO 8
O ALT = 40K ALP: -4 TO 10
A ALT = 50K ALP: -4 TO 12



CD-ALPHA DØT VS MACH # 7-6-83 X-29A 1-G TRIM NØRMAL MØDE XCG = 451.0 WT = 15K

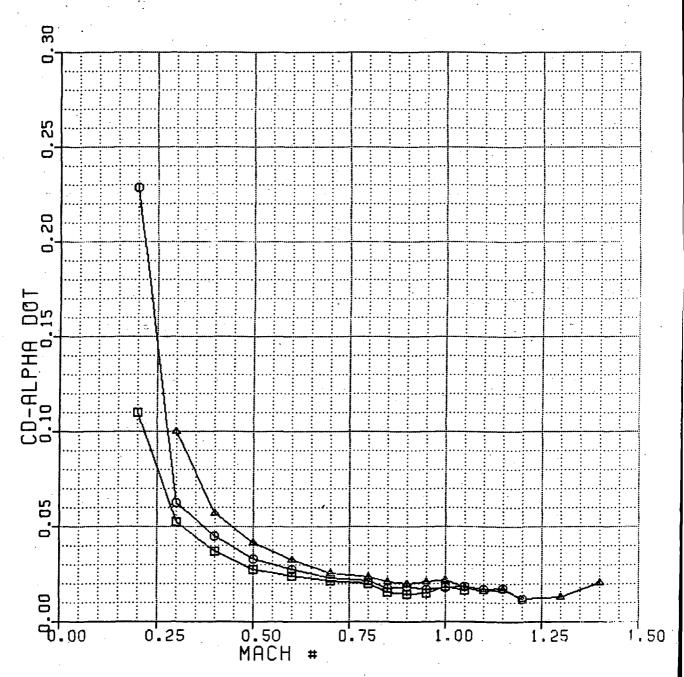


Figure 85(a)

CD-ALPHA DOT VS MACH # 7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

9 ALT = 30K M# = .3 TO 1.5 9 ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

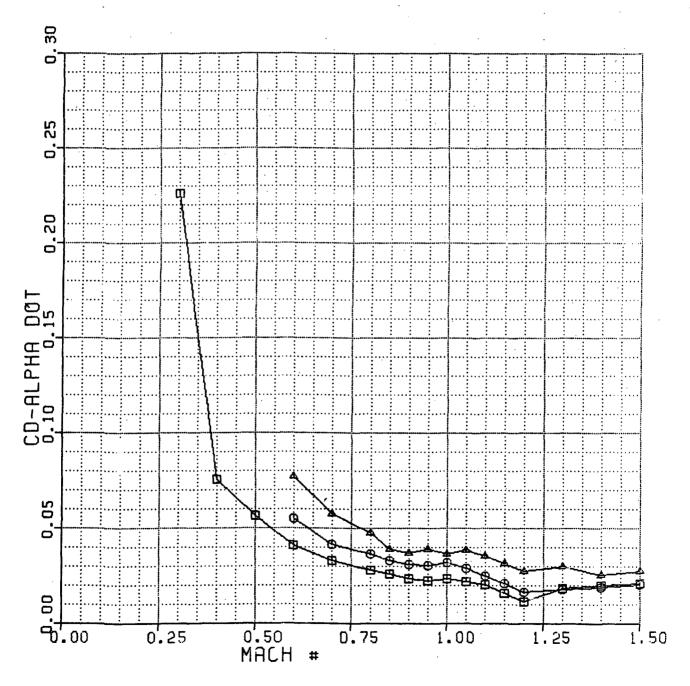


Figure 85(b)

CD-ALPHA DOT VS ALPHA
6-16-83 X-29A M# = 0.4 NØRMAL MØDE
XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = S.L. ALP: -4 TØ 22
CD-D ALT = 10K ALP: -4 TØ 22

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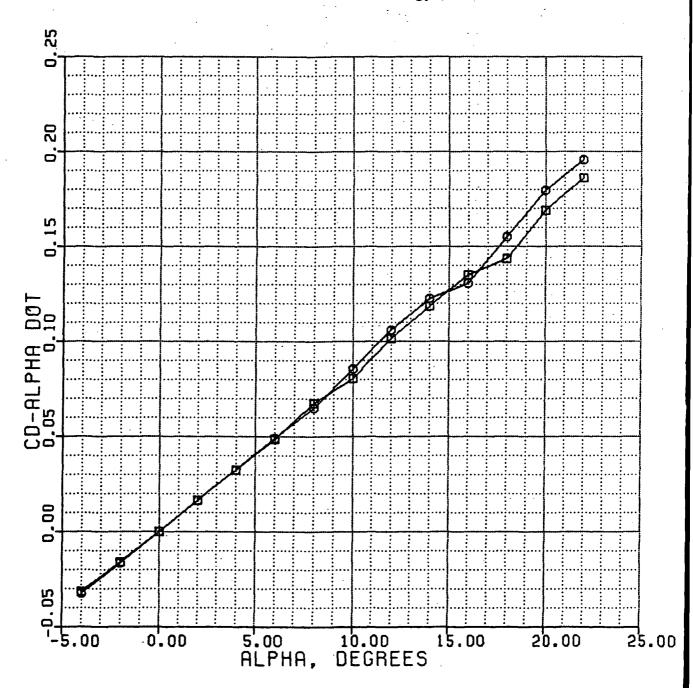
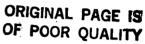


Figure 86(a)



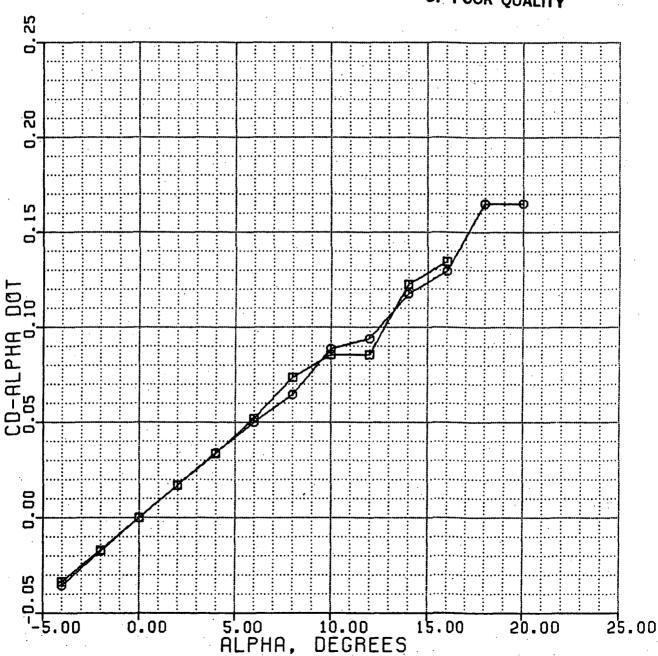
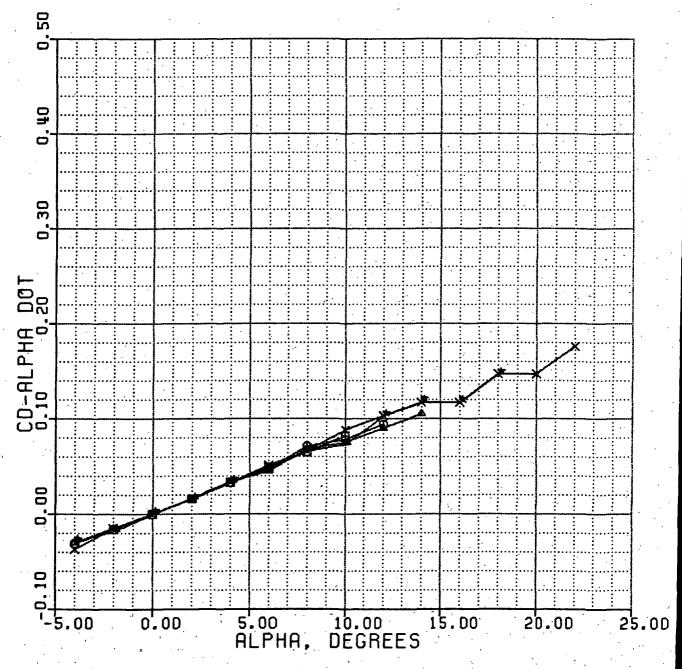


Figure 86(b)

6-30-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM



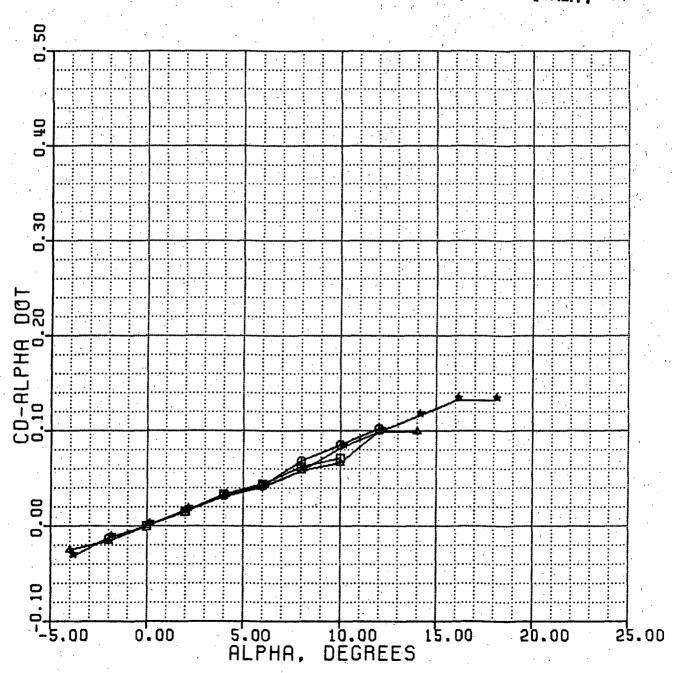


Figure 86(d)

```
CD-ALPHA DOT VS ALPHA
7-1-83
        X-29A
                M# = 1.2 NORMAL MODE
                         ALPHA TRIM
XCG = 451.0
            WT =
                   15K
       ALT = 20K
       ALT = 30K
       ALT = ,40K
                    -4 TO 12
                             ORIGINAL PAGE 18
      ★ ALT = 50K
    ,1;
                             OF POOR QUALITY
```

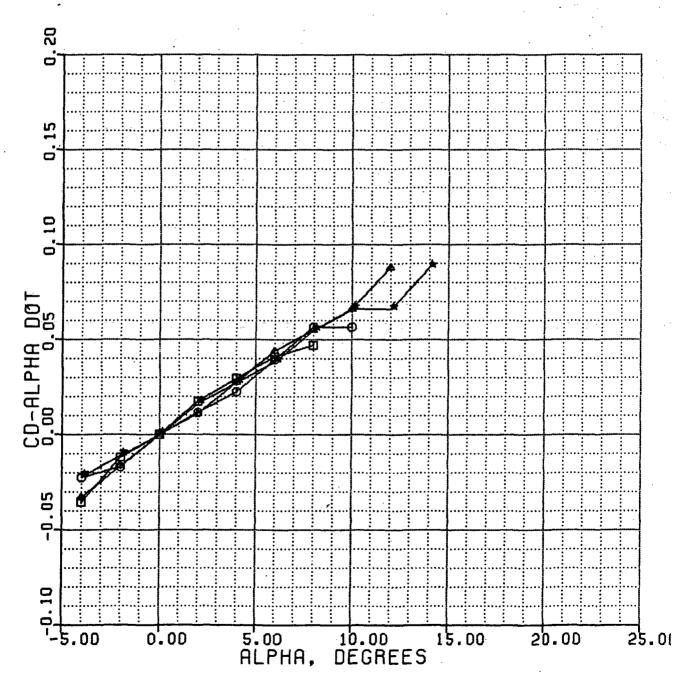


Figure 86(e)

CD-ALPHA DOT VS ALPHA 7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8

9 ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12

Salar Commence

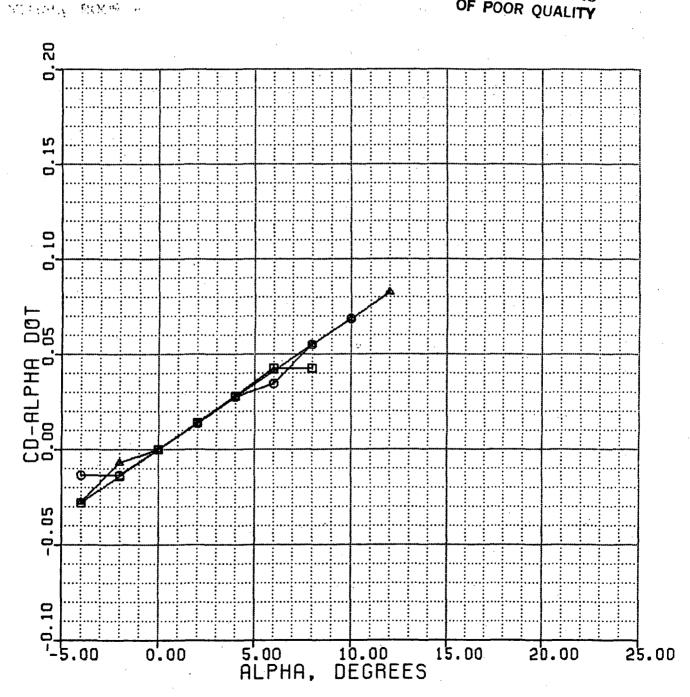


Figure 86(f)

CM-ALPHA DOT VS MACH # 7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K B ALT = S.L. M# = .2 TO 1.05 B ALT = 10K M# = .2 TO 1.2

_ ALT = 20K M# = .3 TO 1.4

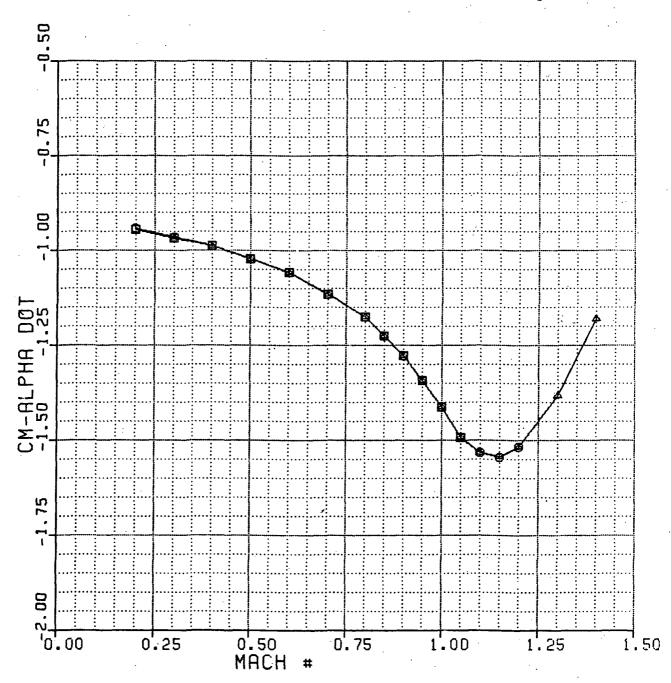


Figure 87(a)

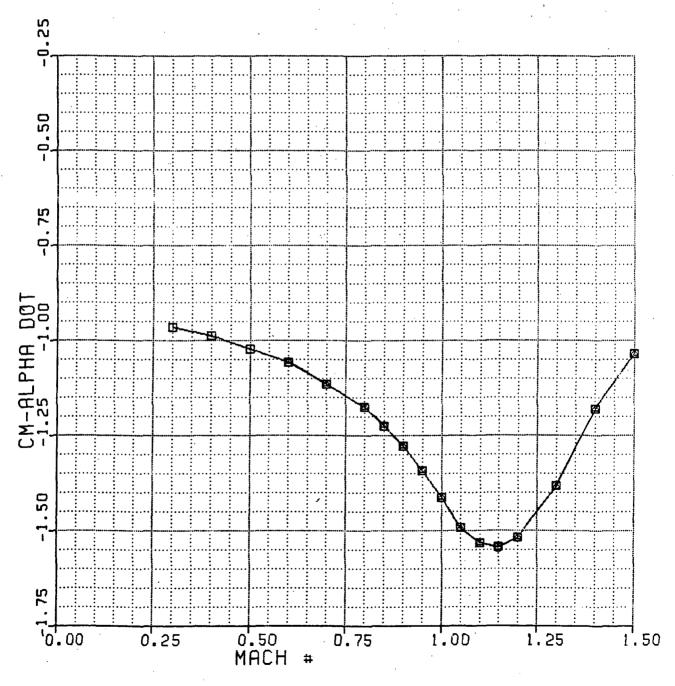


Figure 87(b)

7-26-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

3.000

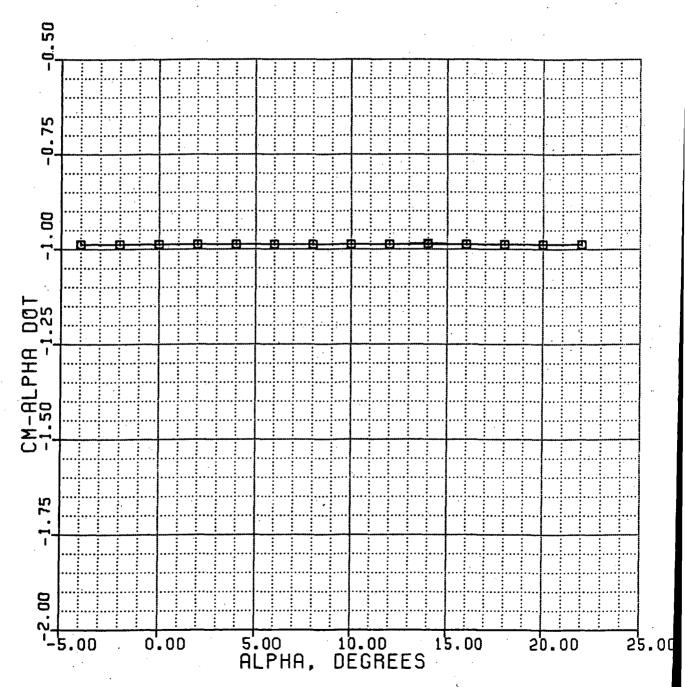


Figure 88(a)

7-26-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 10K ALP: -4 TO 16 0 ALT = 20K ALP: -4 TO 20

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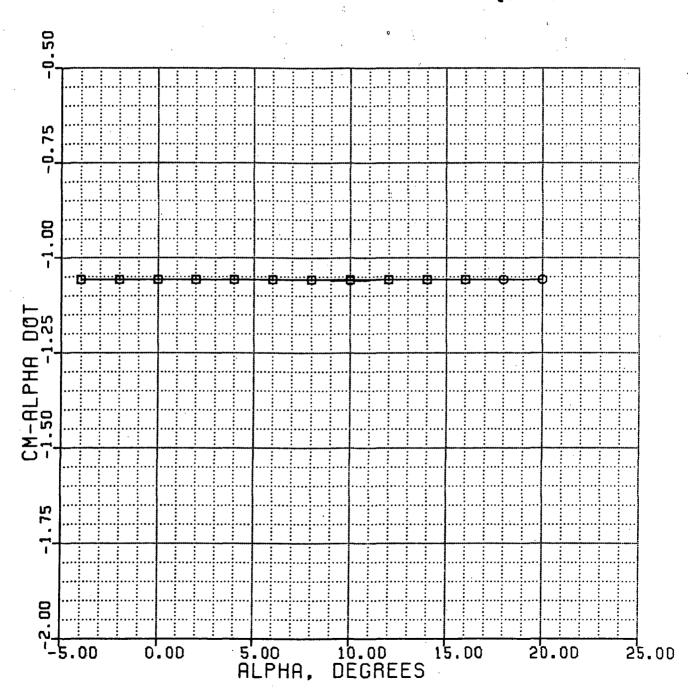
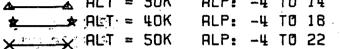
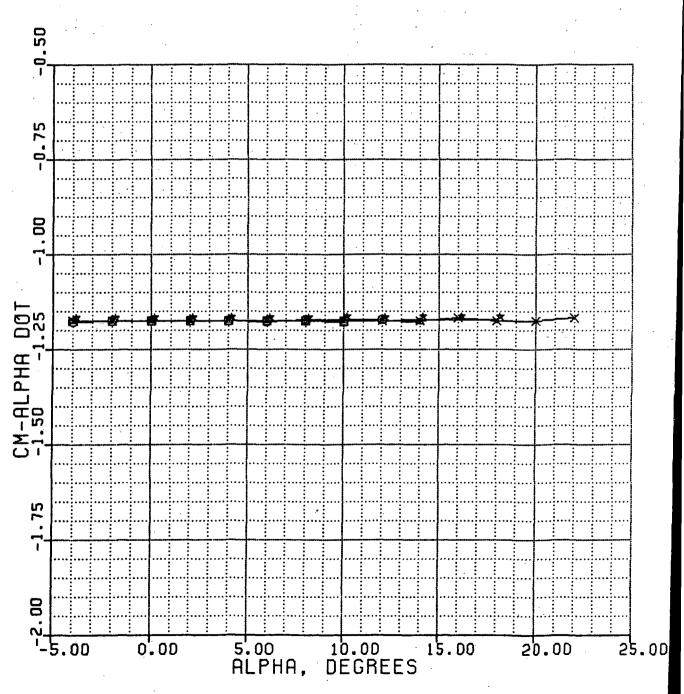


Figure 88(b)

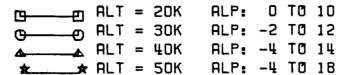
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7-27-83 X-29A M# = 0.9 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM



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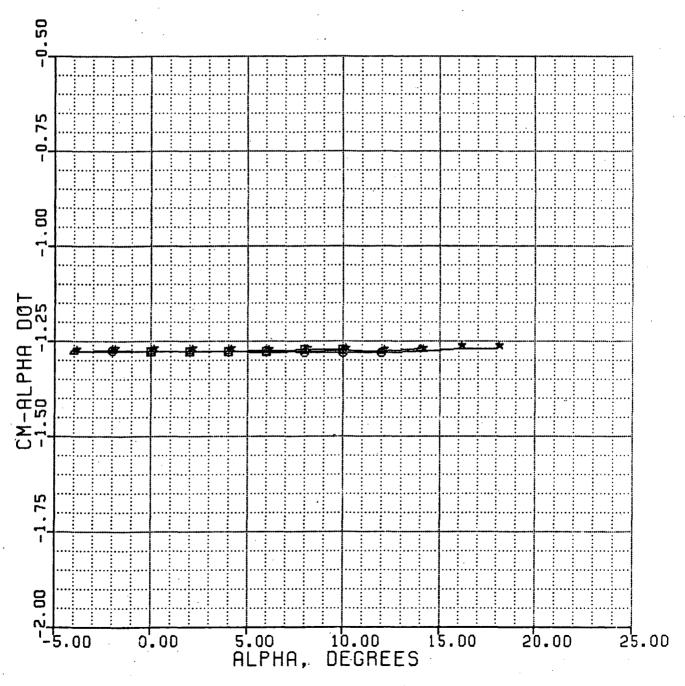


Figure 88(d)

7-27-83 X-29A M# = 1.2 NØRMAL MØDE

XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

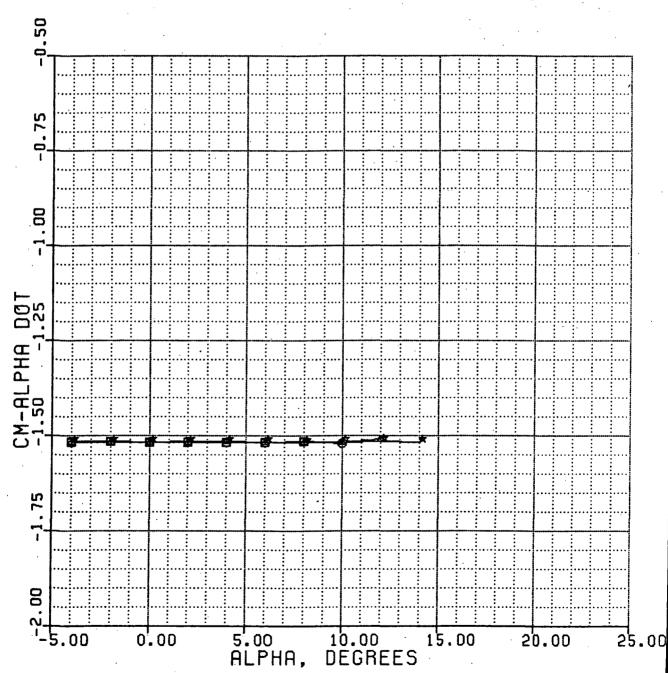


Figure 88(e)

7-27-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

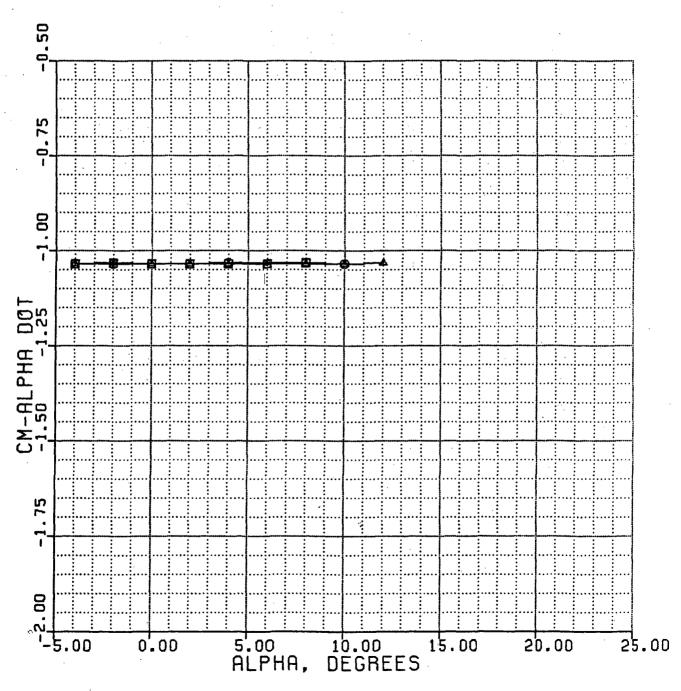


Figure 88(f)

CA-ALPHA DOT VS MACH # 7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

```
PALT = 5.L. M# = .2 TO 1.05

PALT = 10K M# = .2 TO 1.2

ALT = 20K M# = .3 TO 1.4
```

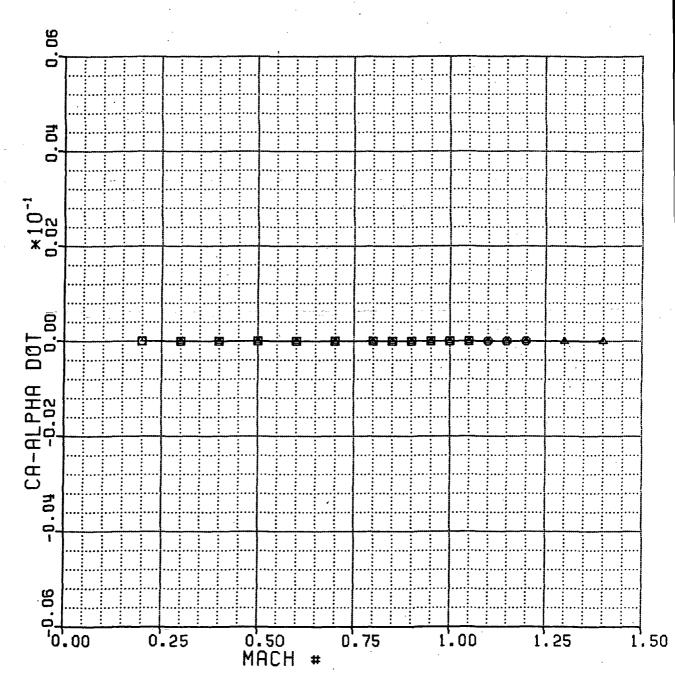
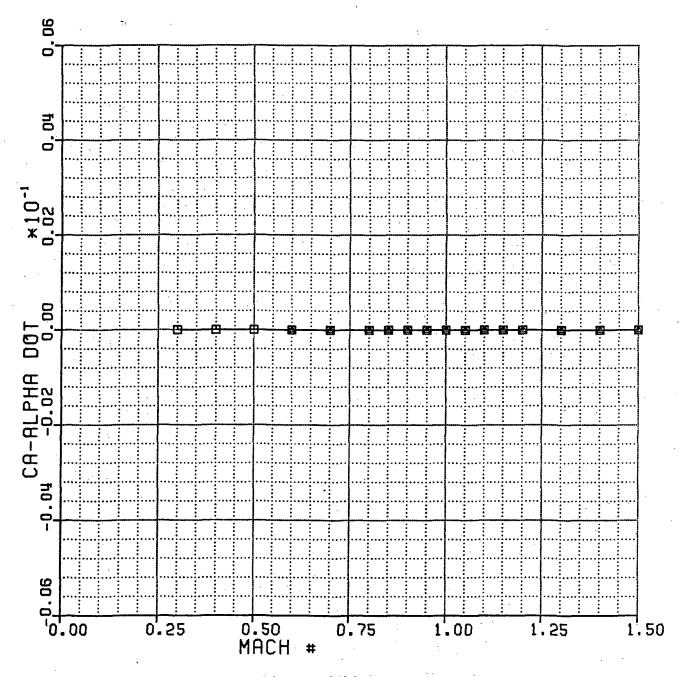
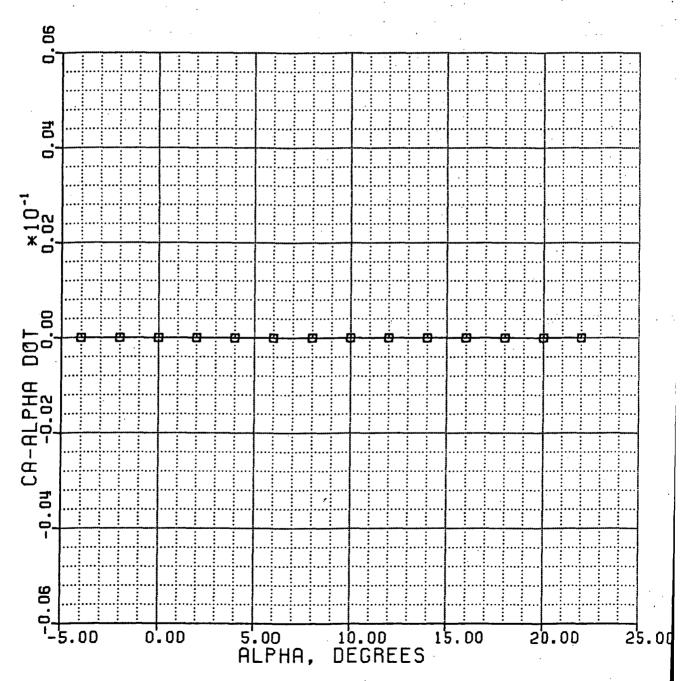


Figure 89(a)



CA-ALPHA DØT VS ALPHA 7-26-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM



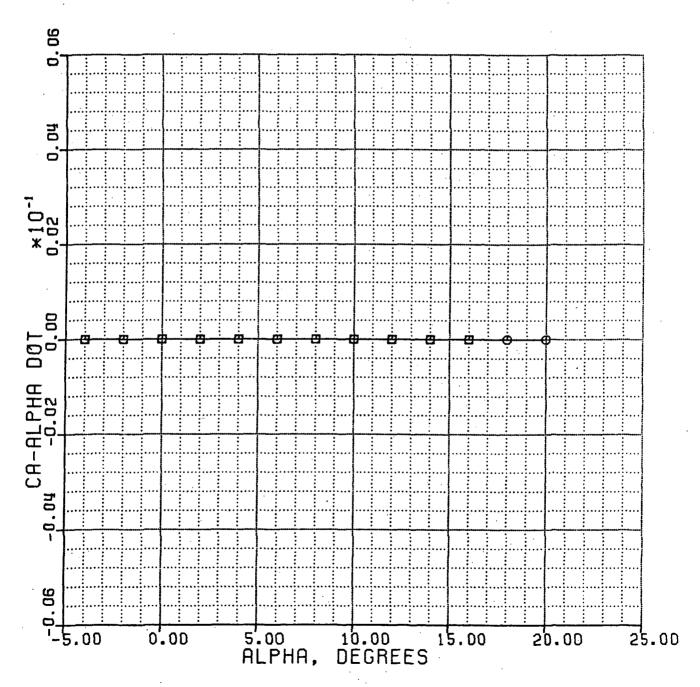
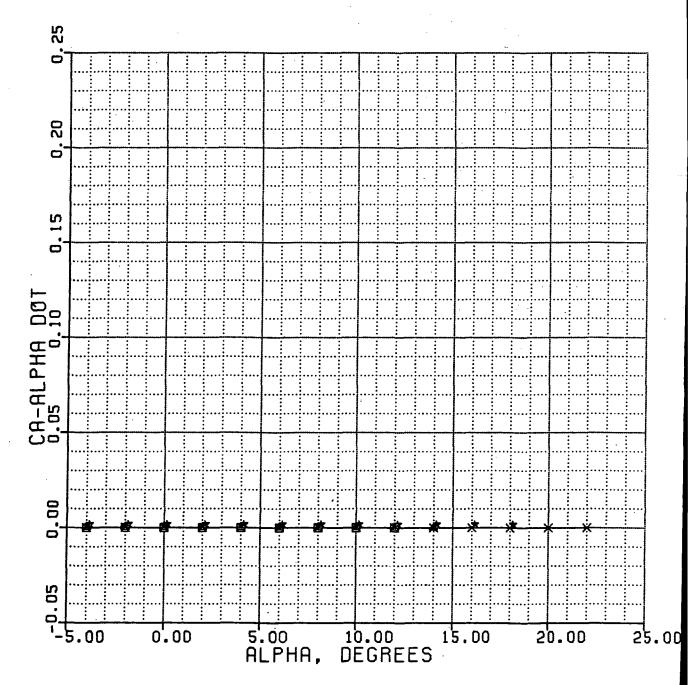


Figure 90(b)

CA-ALPHA DOT VS ALPHA 7-26-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM -E) ALT = 10K 0 TO 10 -O ALT = 20K ALP: -4 TO 12 ALT = 30KALP: -4 TO 14 ___★ ALT = 40K ALP: -4 TO 18 ORIGINAL PAGE 18 → ALT = 50K ALP: -4 TO 22

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7-27-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

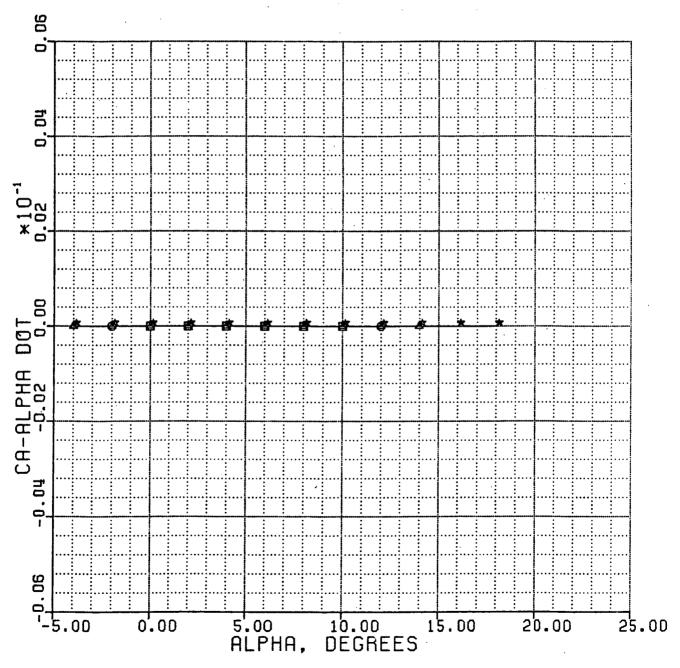


Figure 90(d)

7-27-83 X-29A M# = 1.2 NØRMAL MØDE ALPHA TRIM XCG = 451.0 WT = 15K

ALT = 20KALP: -4 TO 8 RLT = 30KALP: -4 TO 10 RLP: -4 TO 12 ORIGINAL PAGE IS ALT = 40KALP: -4 TO 14 ★ ALT = 50K

-: 554.

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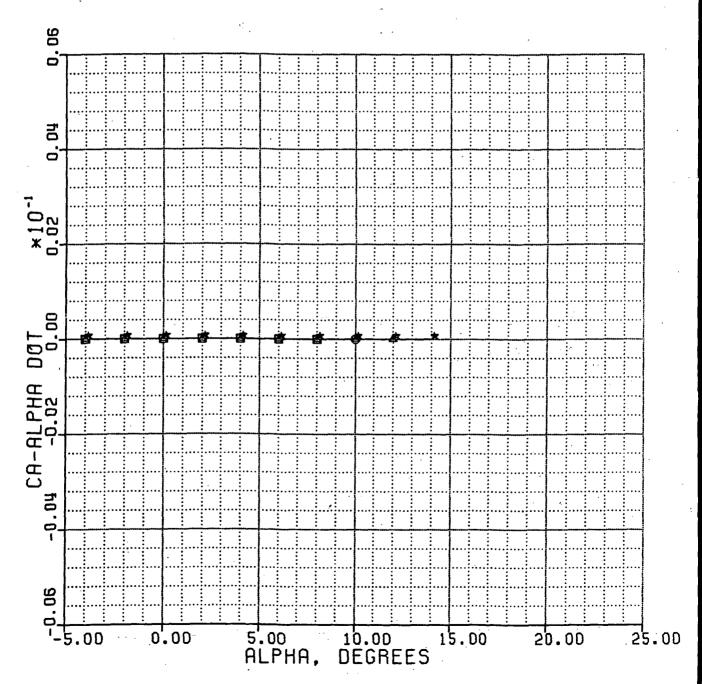


Figure 90(e)

CA-ALPHA DOT VS ALPHA 7-27-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 30K ALP: -4 TO 8

P ALT = 40K ALP: -4 TO 10

ALT = 50K ALP: -4 TO 12

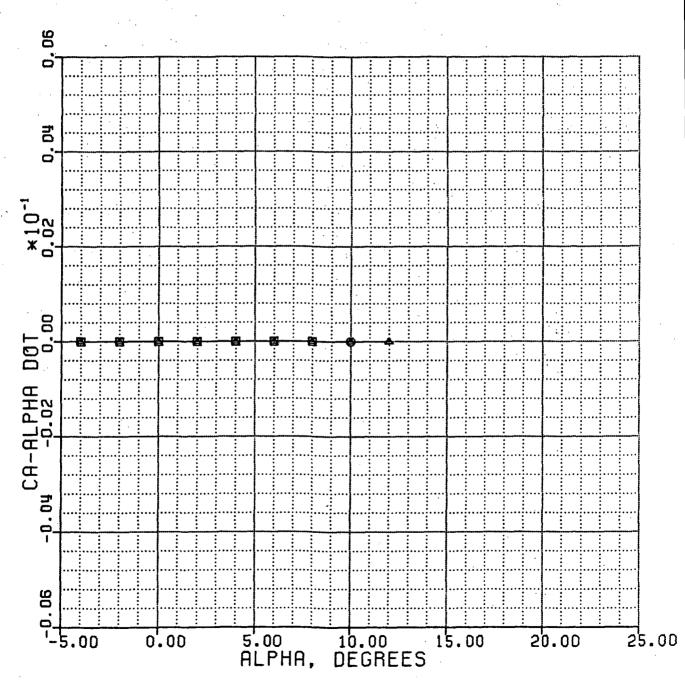
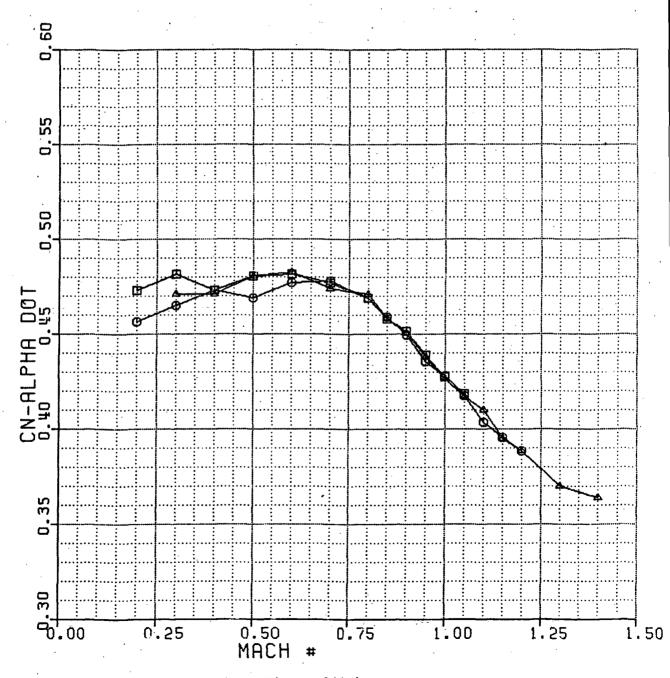


Figure 90(f)

```
CN-ALPHA DØT VS MACH
                                              #
                1-G TRIM NORMAL MODE
7-6-83 X-29A
XCG = 451.0 WT = 15K
                  M = .2 \text{ TO } 1.05
        ALT = S.L.
        ALT = 10K
                  M# = .2 T0 1.2
                                ORIGINAL PAGE IS
                  M = .3 \text{ TO } 1.4
        ALT = 20K
```

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CN-ALPHA DOT VS MACH # 7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 3.10.1.5

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

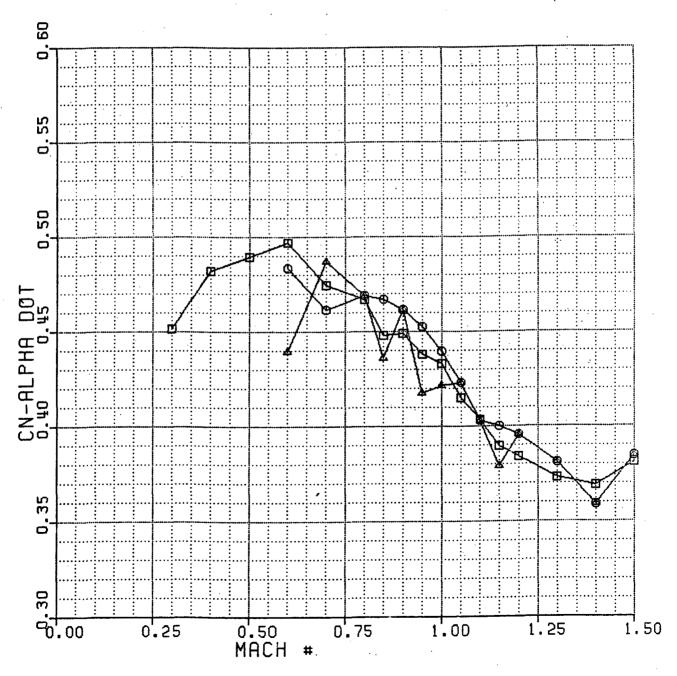


Figure 91(b)

CN-ALPHA DOT VS ALPHA 7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = S.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22

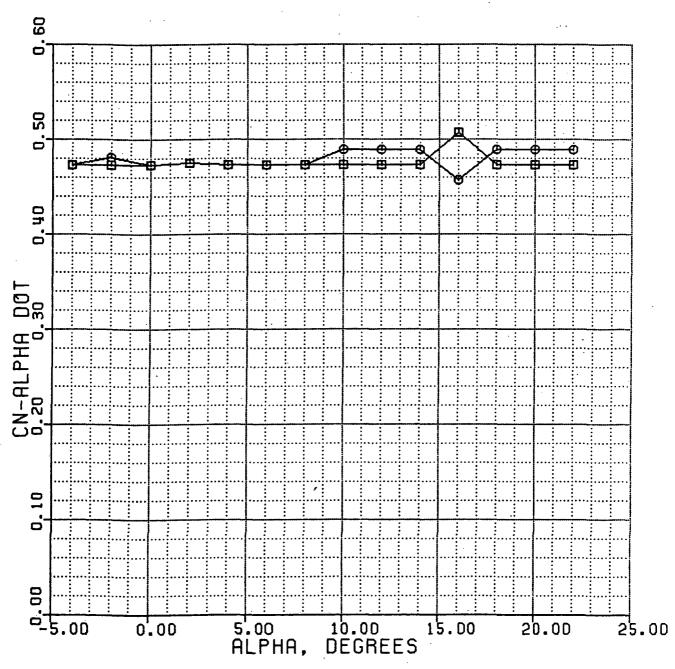


Figure 92(a)

7-26-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 10K ALP: -4 TO 16 0 ALT = 20K ALP: -4 TO 20

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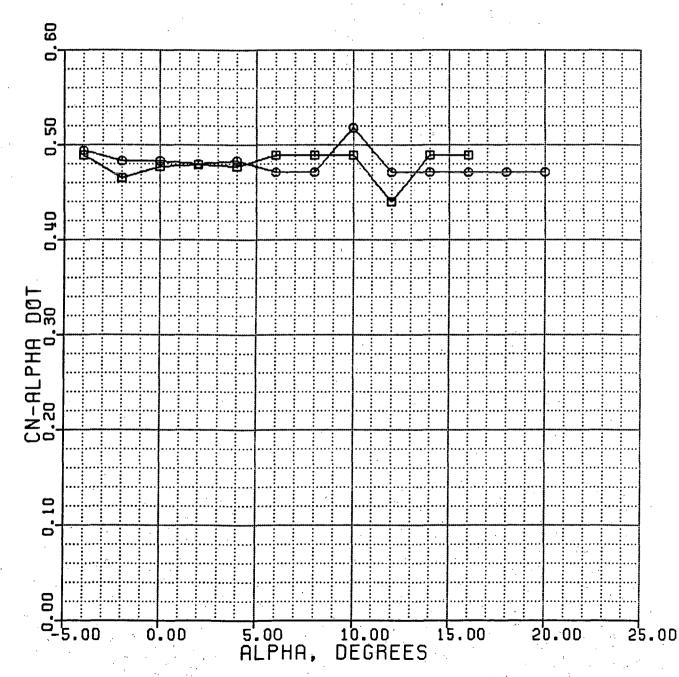


Figure 92(b)



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CN-ALPHA DOT VS ALPHA 7-26-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 T0 10

P ALT = 20K ALP: -4 T0 12

A ALT = 30K ALP: -4 T0 14

A ALT = 40K ALP: -4 T0 18

A ALT = 50K ALP: -4 T0 22
```

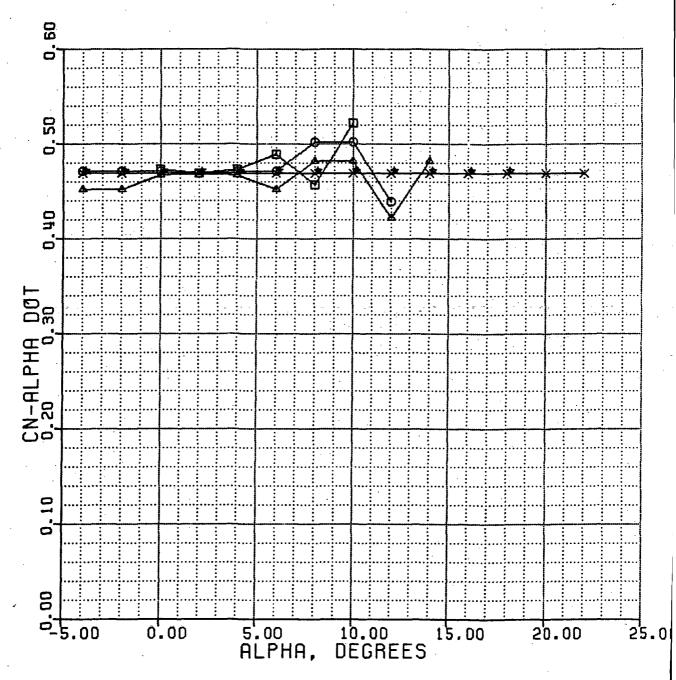


Figure 92(c)

CN-ALPHA DØT VS ALPHA 7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
ALP: 0 TO 10
         ALP: -2 TO 12
 _n RLT = 30K
CALT = 40K
         ALP: -4 TO 14
```

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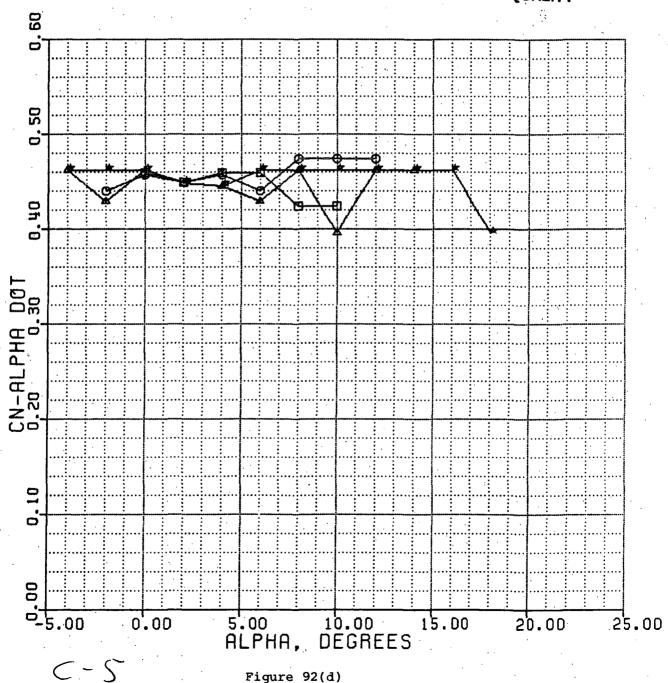


Figure 92(d)

387

7-27-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14

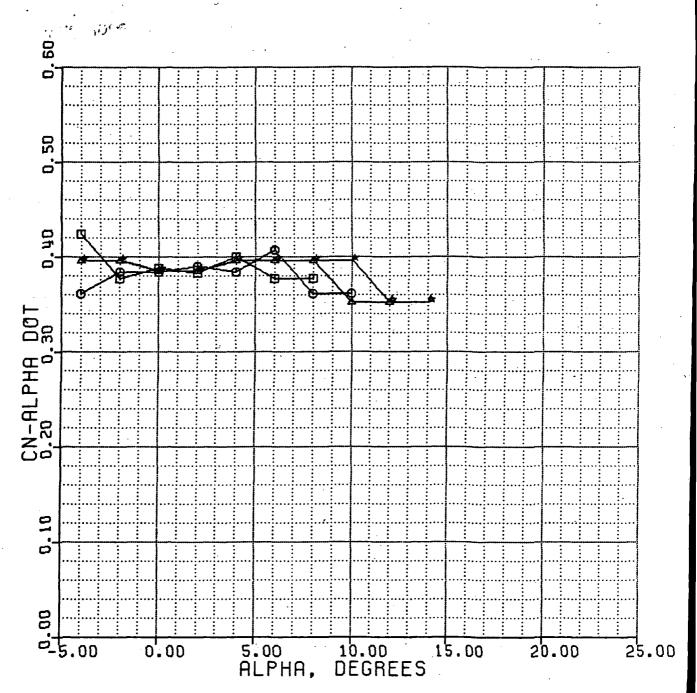


Figure 92(e)

7-27-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8 9 ALT = 40K ALP: -4 TO 10 A ALT = 50K ALP: -4 TO 12

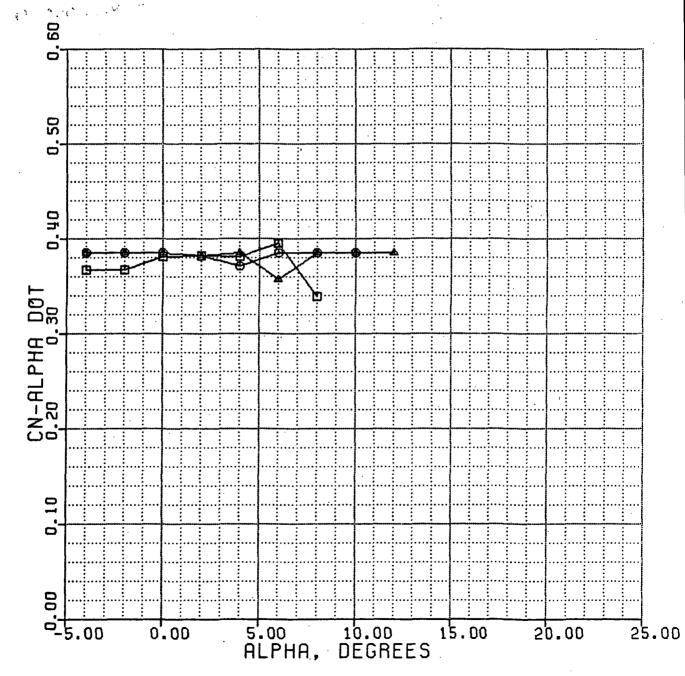


Figure 92(f)

CL-q VS MACH#

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

9 ALT = S.L. M# = .2 TO 1.05 9 ALT = 10K M# = .2 TO 1.2 ALT = 20K M# = .3 TO 1.4

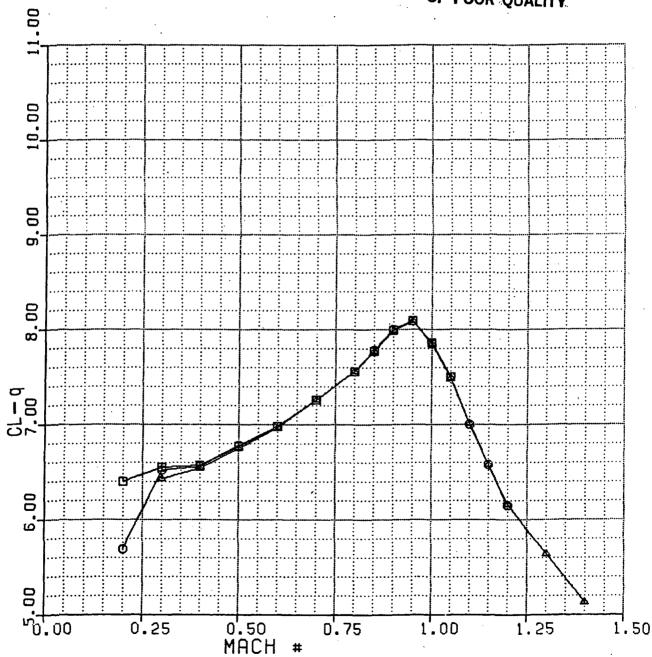


Figure 93(a)

CL - q VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 45K

m-m ALT = 30K M# = .3 TO 1.5 O ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

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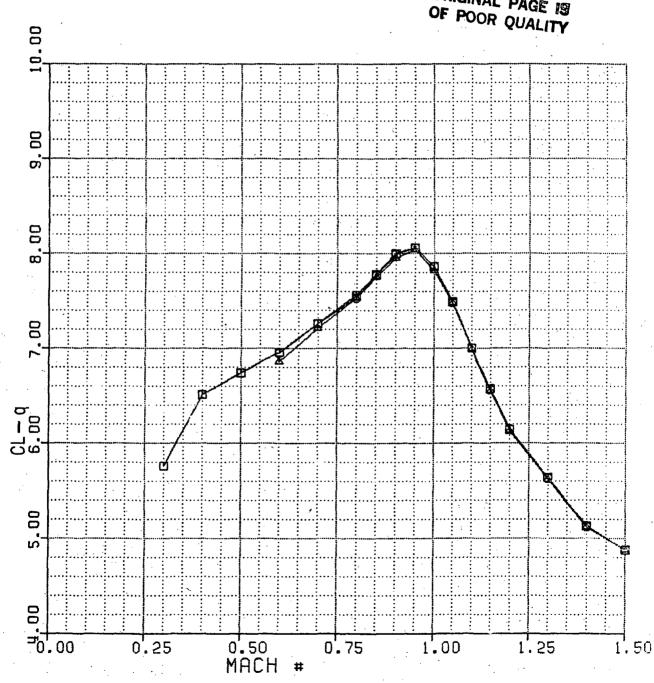


Figure 93(b)

CL-q VS ALPHA

6-16-83 X-29A M# = 0.4 NORMAL LODE XCG = 451.0 WT = 15K ALPHA TRIE

0 ALT = S.L. ALP: -4 TO 22 0 ALT = 10K ALP: -4 TO 22

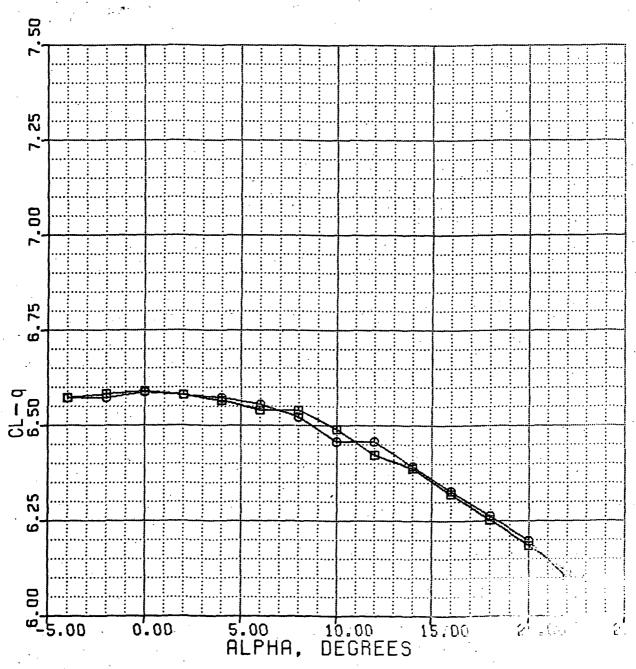


Figure 94(a)

CL-q VS ALPHA

6-17-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 10K ALP: -4 TO 16 O ALT = 20K ALP: -4 TO 20

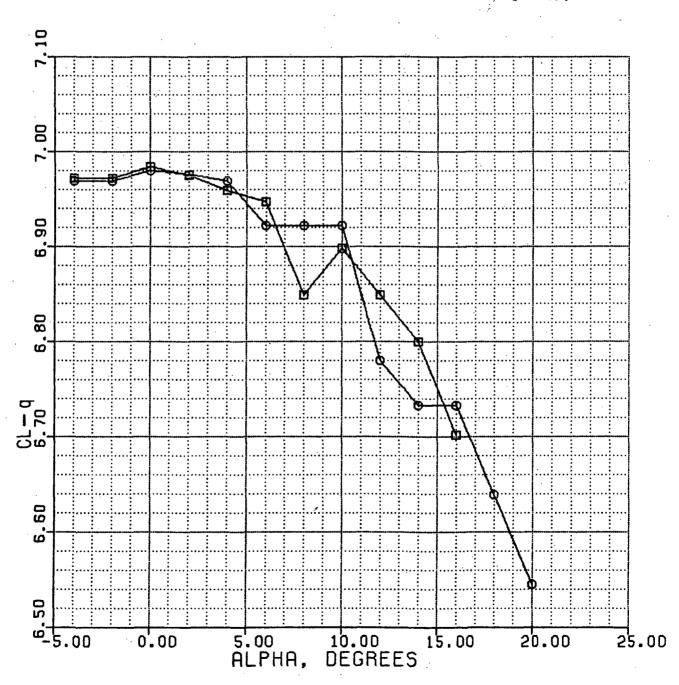


Figure 94(b)

CL-q VS ALPHA

6-30-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALP = 30K ALP: -4 TO 14

A ALT = 40K ALP: -4 TO 18

A ALT = 50K ALP: -4 TO 22
```

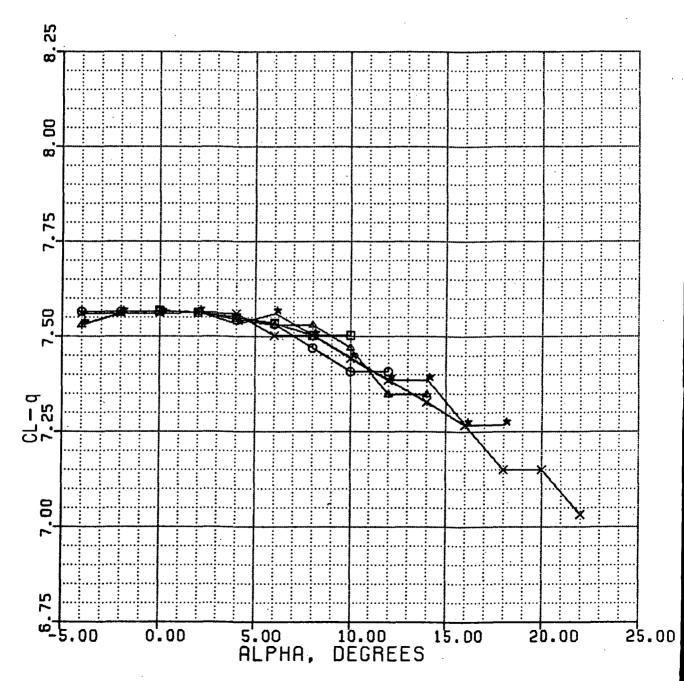


Figure 94(c)

7-1-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

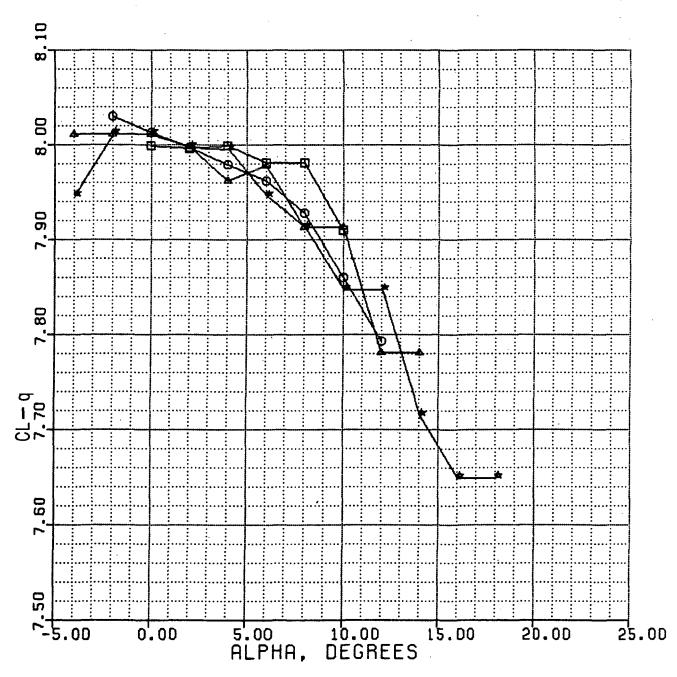


Figure 94(d)

7-27-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

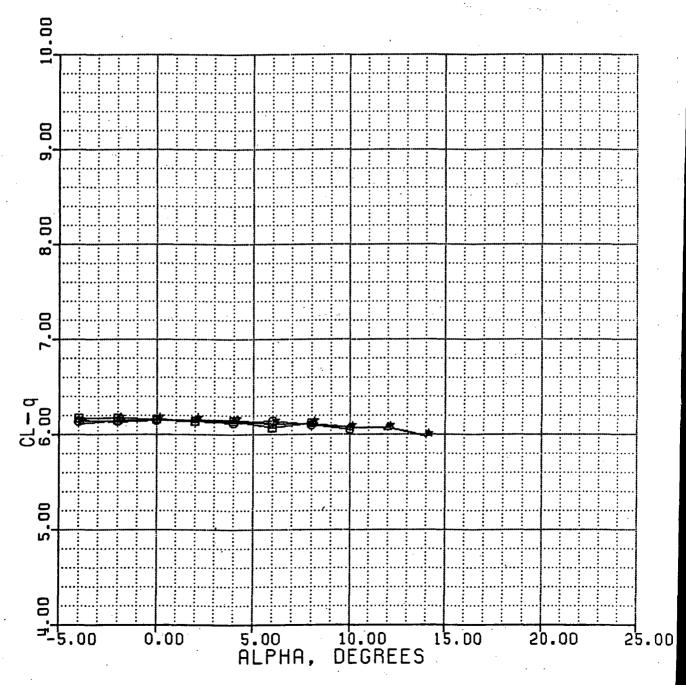


Figure 94(e)

7-27-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
O ALT = 30K ALP: -4 TO 8
O ALT = 40K ALP: -4 TO 10
A ALT = 50K ALP: -4 TO 12
```

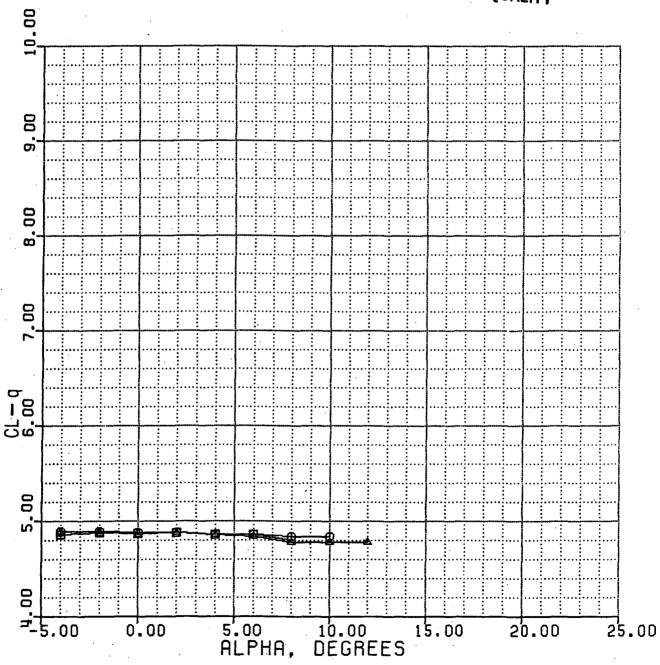


Figure 94(f)

CD - q VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 5.L. M# = .2 TO 1.05
P ALT = 10K M# = .2 TO 1.2
A ALT = 20K M# = .3 TO 1.4

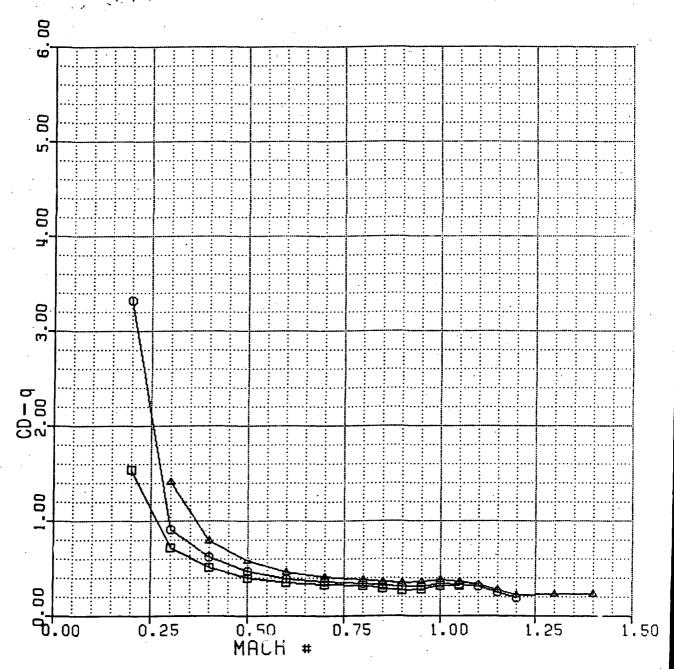


Figure 95(a)

CD-q VS MACH#

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7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

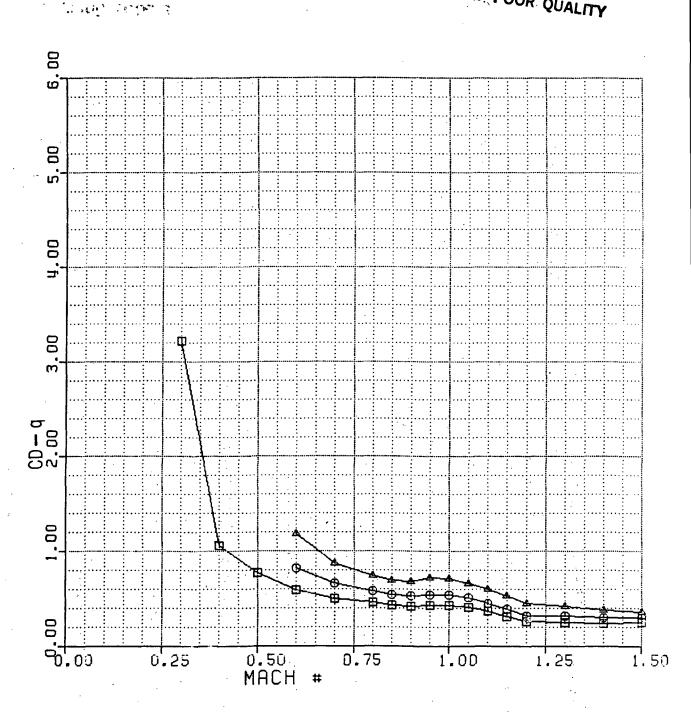


Figure 95(b)

6-16-83 X-29A M# = 0.4 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

B ALT = 10K ALP: -4 TO 22

C ALT = 20K ALP: -4 TO 22

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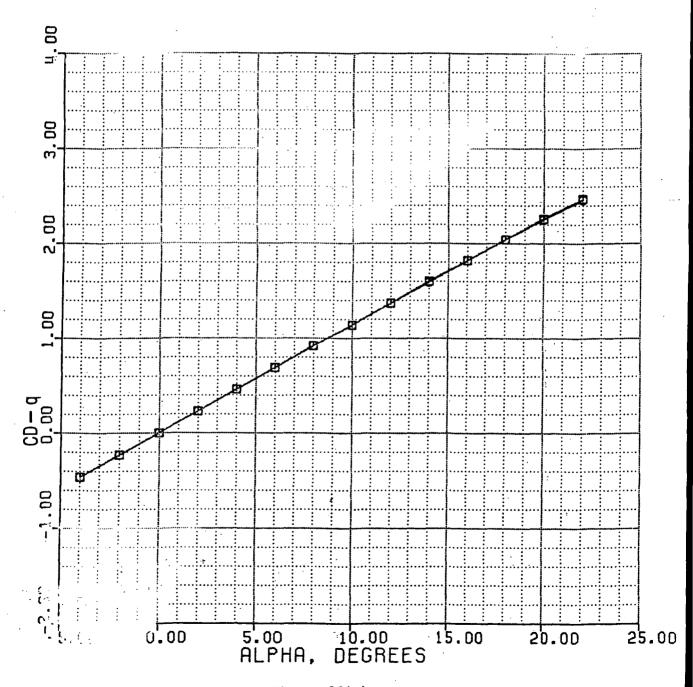


Figure 96(a)

वर्षका है।

6-17-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

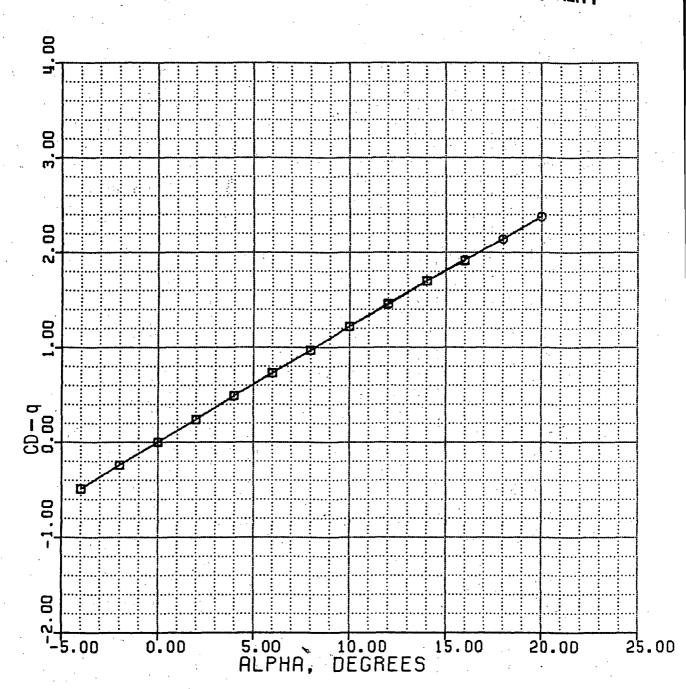


Figure 96(b)

```
6-30-83 X-29A M# = 0.8 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM
```

```
P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALP = 30K ALP: -4 TO 14

RLT = 40K ALP: -4 TO 18

RLT = 40K ALP: -4 TO 22

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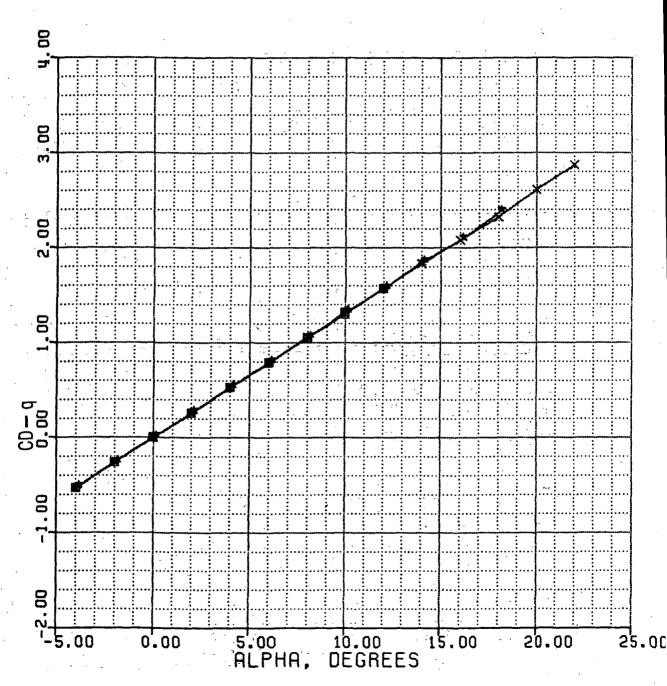


Figure 96(c)

7-1-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
_p ALT = 20K
                      ALP:
                              O TO 10
   _O ALT = 30K
                      ALP: -2 TO 12
ALT = 40K ALP: -4 TO 14 ORIGINAL PAGE IS

ALT = 50K ALP: -4 TO 18 OF POOR QUALITY
```

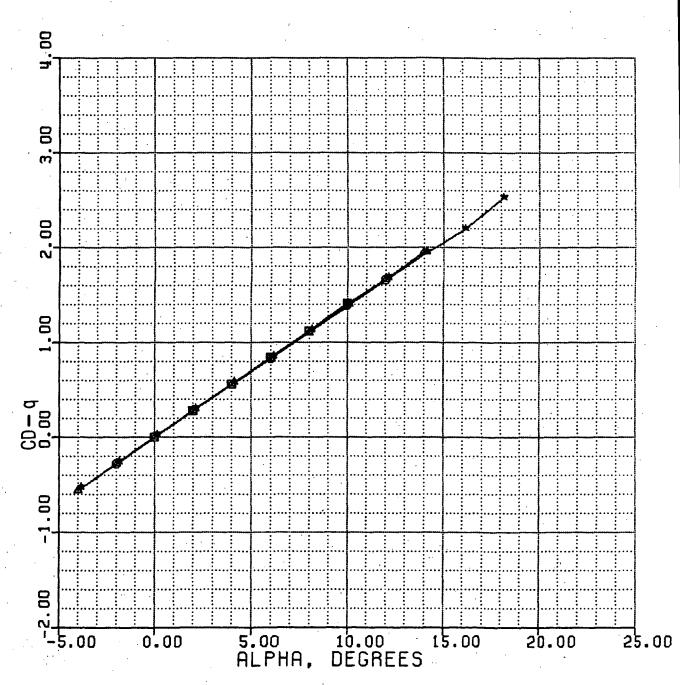


Figure 96(d)

7-1-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14

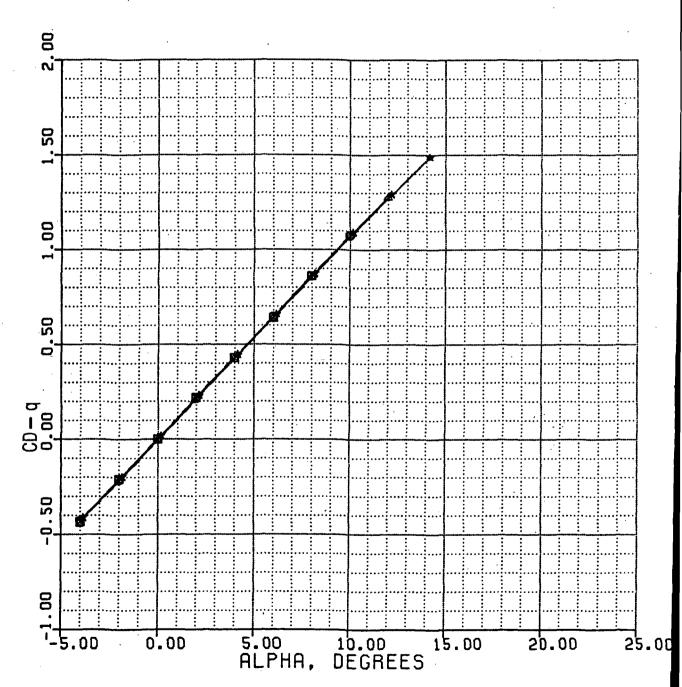


Figure 96(e)

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
O ALT = 30K ALP: -4 TO 8
O ALT = 40K ALP: -4 TO 10
A ALT = 50K ALP: -4 TO 12
```

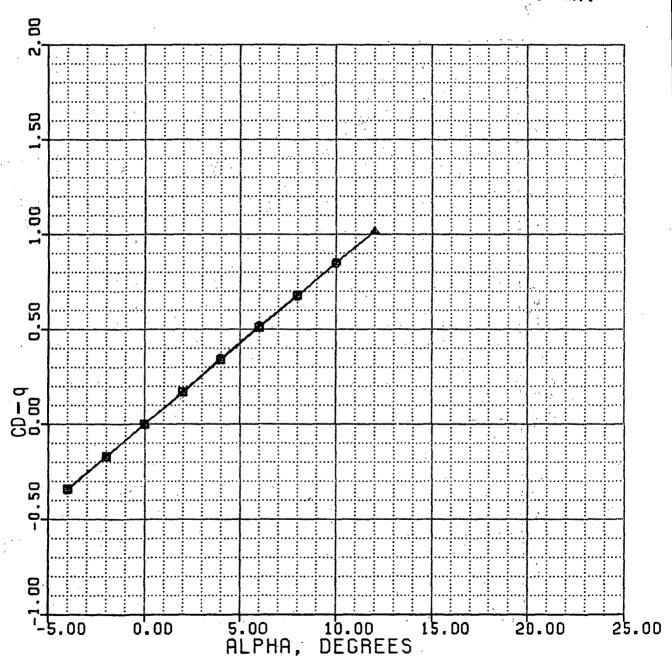


Figure 96(f)

CM - q VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

PALT = 5.L. M# = .2 TO 1.05 A PALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4

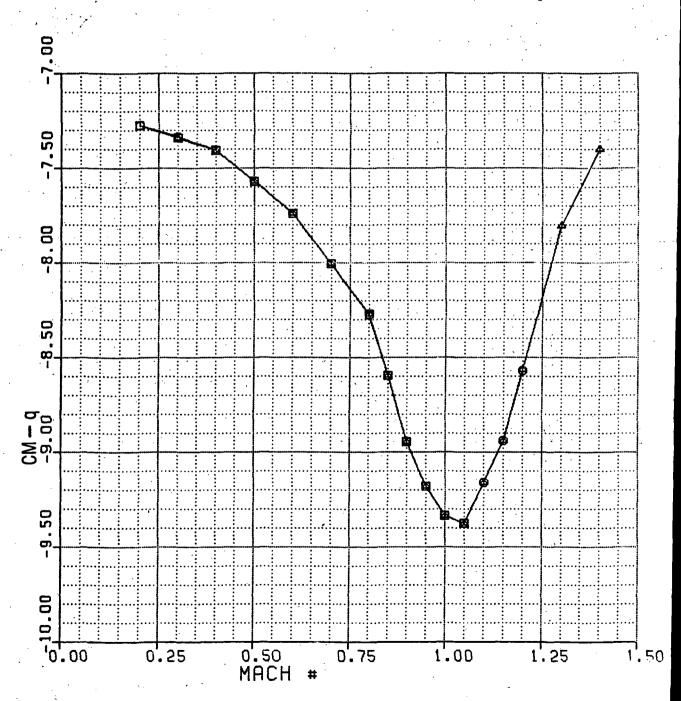


Figure 97(a)

CM-q VS MACH#

Fair Mark & Agri

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

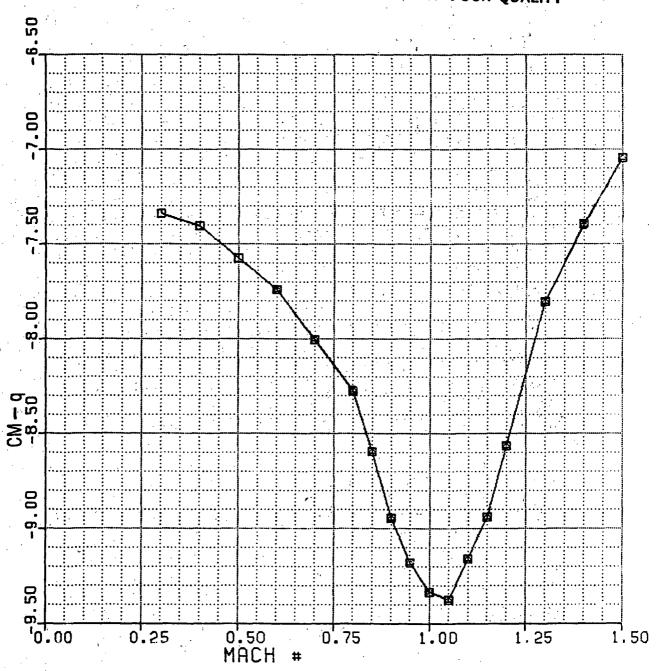


Figure 97(b)

7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P RLT = 5.L. ALP: -4 TO 22 P ALT = 10K ALP: -4 TO 22

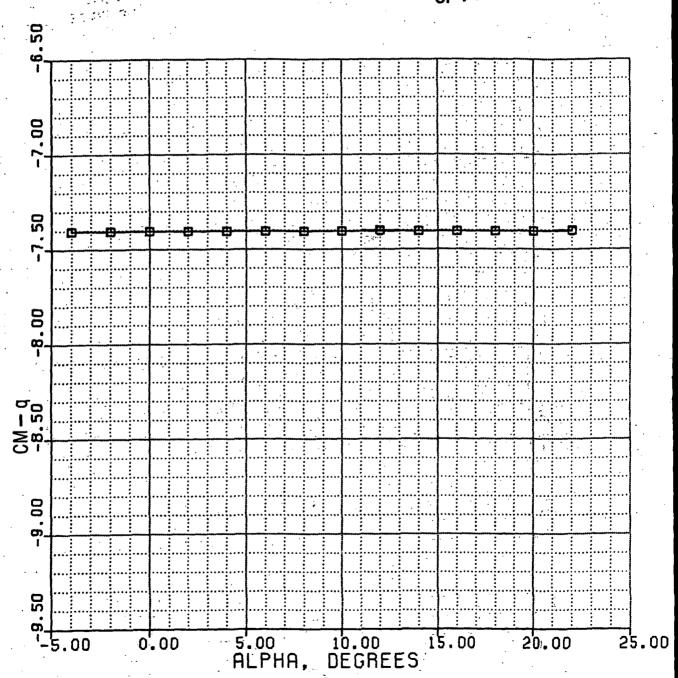


Figure 98(a)

Carlotte State

7-26-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P RLT = 10K RLP: -4 TO 16 P RLT = 20K RLP: -4 TO 20

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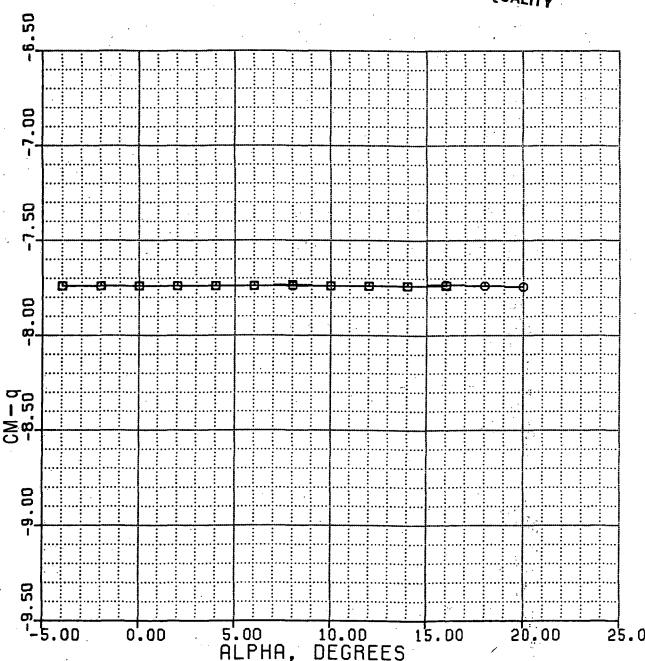


Figure 98(b)

```
7-26-83 X-29A M# = 0.8 NORMAL MODE
XCG = 451.0 WT = 15K ALPHA TRIM
    _p_ ALT = 10K
               ALP:
```

```
a ALT = 20K
              ALP: -4 TO 12
  ALT = 30K
              ALP: -4 TO 14
_★ ALT = 40K ALP: -4 TO 18
```

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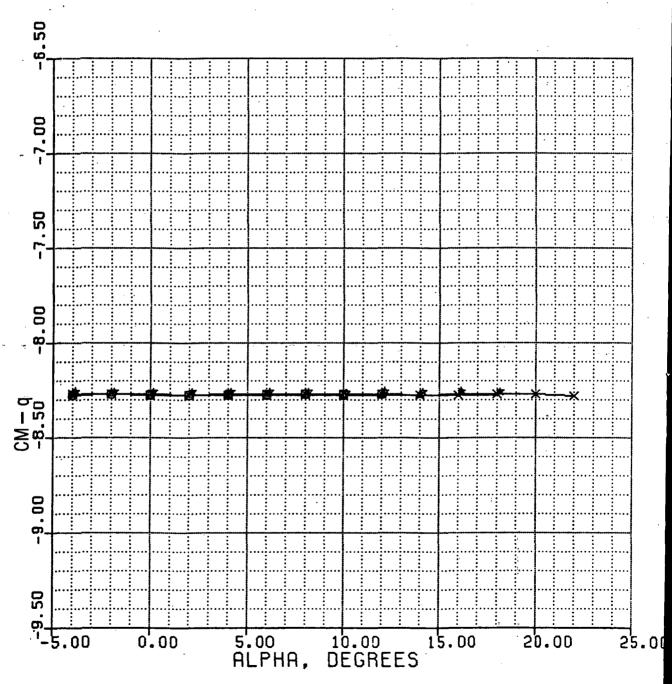


Figure 98(c)

7-27-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: 0 T0 10

P ALT = 30K ALP: -2 T0 12

A ALT = 40K ALP: -4 T0 14

A ALT = 50K ALP: -4 T0 18
```

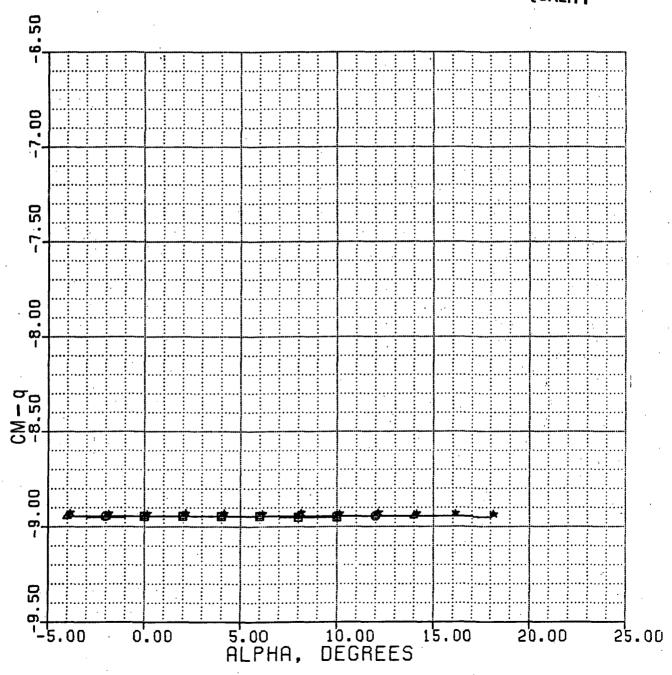


Figure 98(d)

7-27-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
O P ALT = 20K ALP: -4 TO 8
O P ALT = 30K ALP: -4 TO 10
A ALT = 40K ALP: -4 TO 12
A ALT = 50K ALP: -4 TO 14
```

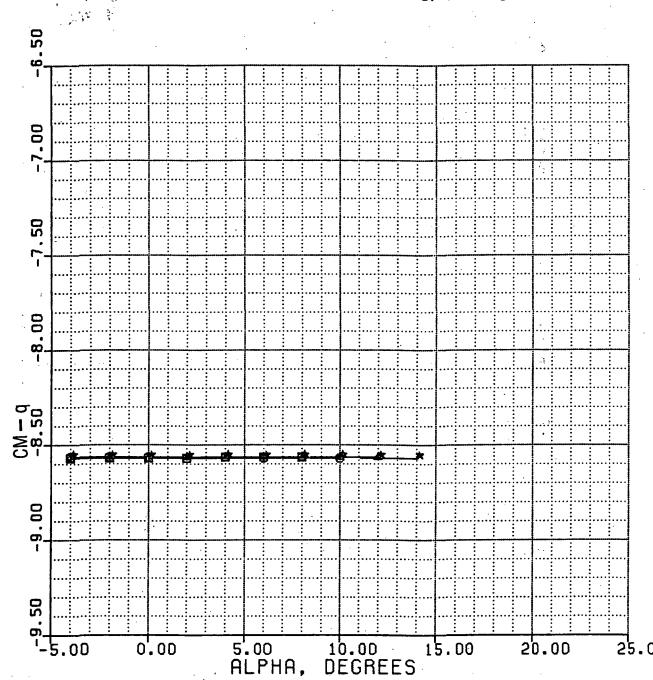
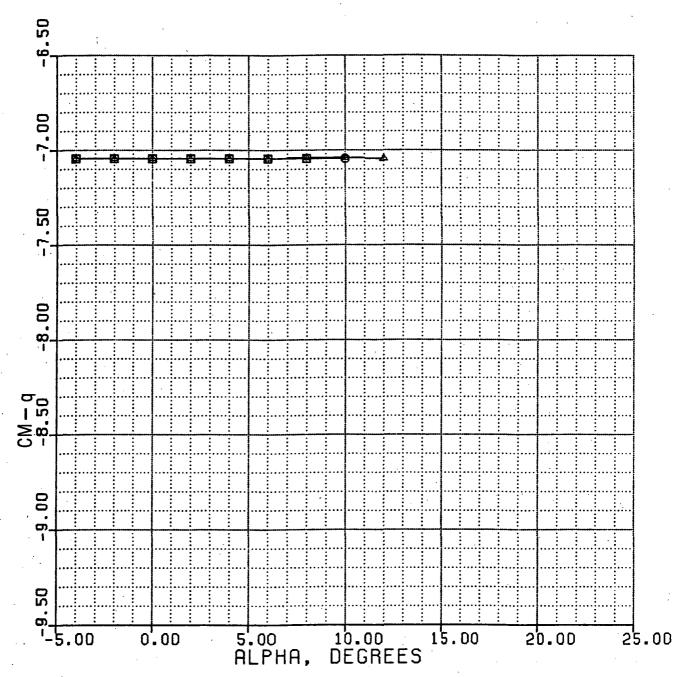


Figure 98(e)

7-27-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

O ALT = 30K ALP: -4 TO 8
O ALT = 40K ALP: -4 TO 10
A ALT = 50K ALP: -4 TO 12



CA - q VS MACH

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

9 ALT = S.L. M# = .2 TO 1.05 9 ALT = 10K M# = .2 TO 1.2 ALT = 20K M# = .3 TO 1.4

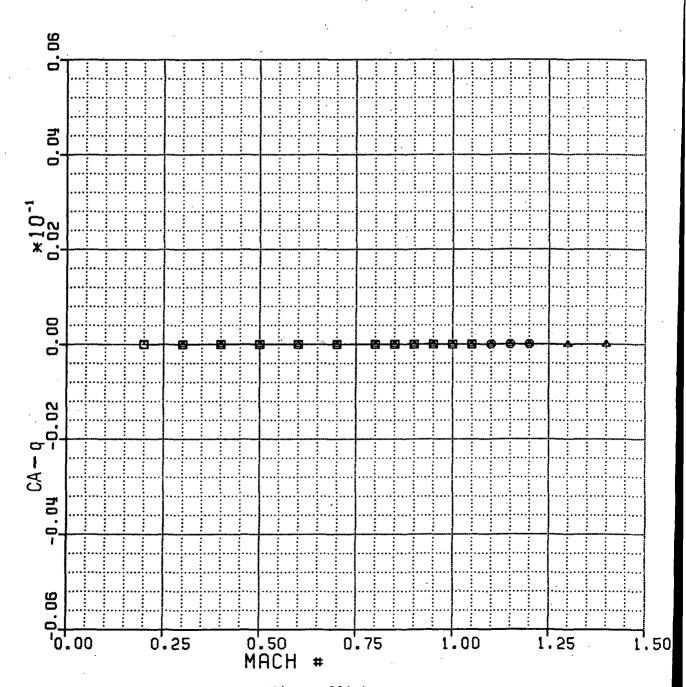


Figure 99(a)

CA-q VS MACH#

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

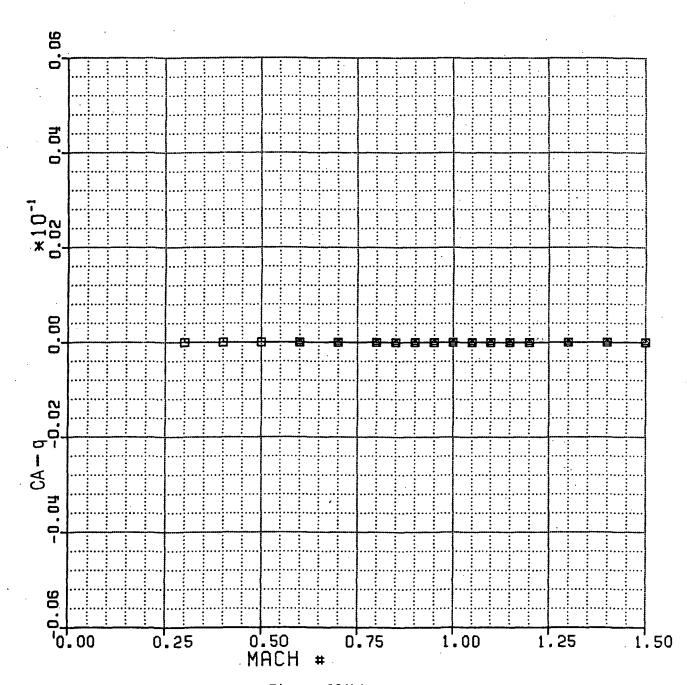


Figure 99(b)

7-26-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

PALT = S.L. ALP: -4 TO 22 PALT = 10K ALP: -4 TO 22

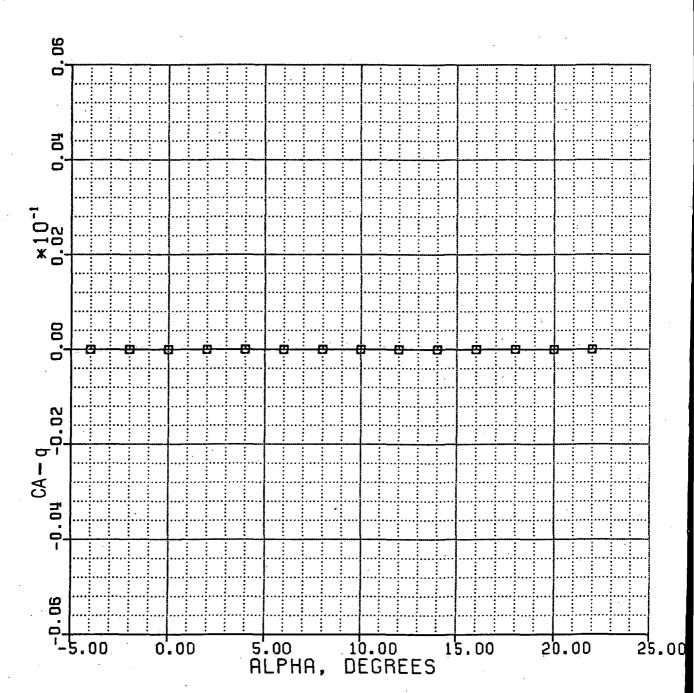
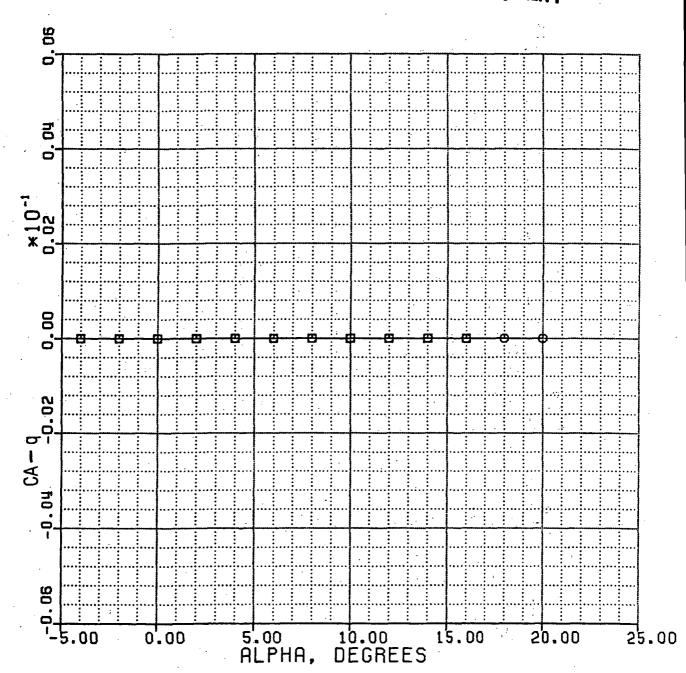


Figure 100(a)

7-26-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

0 PLT = 10K P: -4 TO 16 0 PLT = 20K PLP: -4 TO 20



7-26-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

en ALT = 10K ALP: 0 TO 10 Productions P ALT = 20K ALP: -4 TO 12

ALT = 30K ALP: -4 TO 14

ALT = 40K ALP: -4 TO 18 ORIGINAL PAGE IS
ALT = 50K ALP: -4 TO 22 OF POOR QUALITY

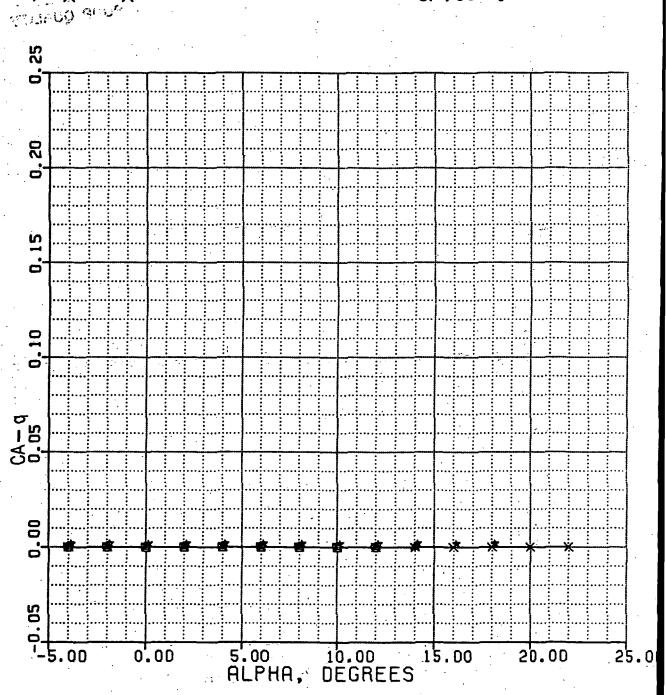


Figure 100(c)

7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: 0 TO 10

P ALT = 30K ALP: -2 TO 12

A ALT = 40K ALP: -4 TO 14

A ALT = 50K ALP: -4 TO 18
```

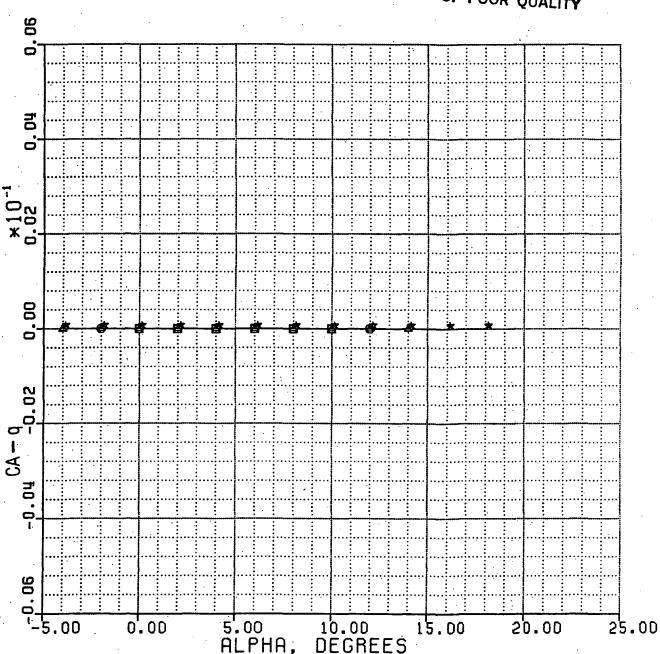


Figure 100(d)

7-27-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

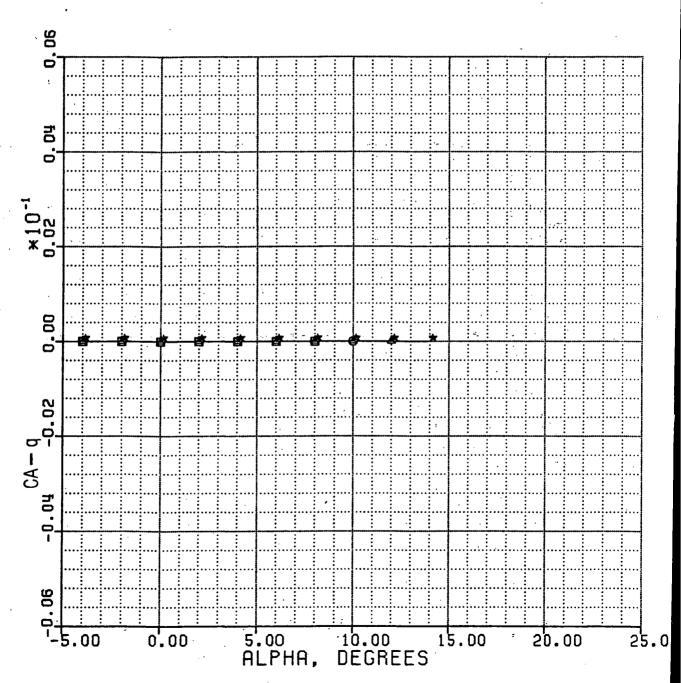


Figure 100(e)

7-27-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P RLT = 30K RLP: -4 TO 8

P PLT = 40K RLP: -4 TO 10

A RLT = 50K RLP: -4 TO 12
```

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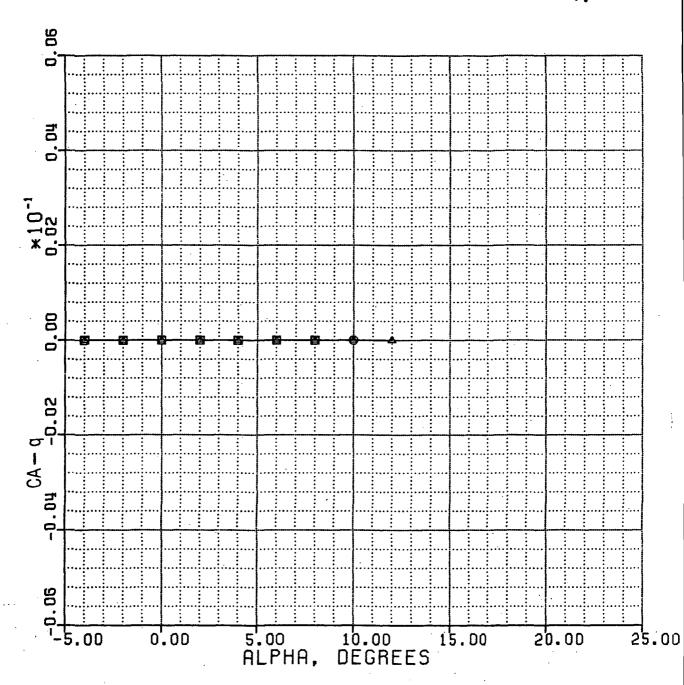
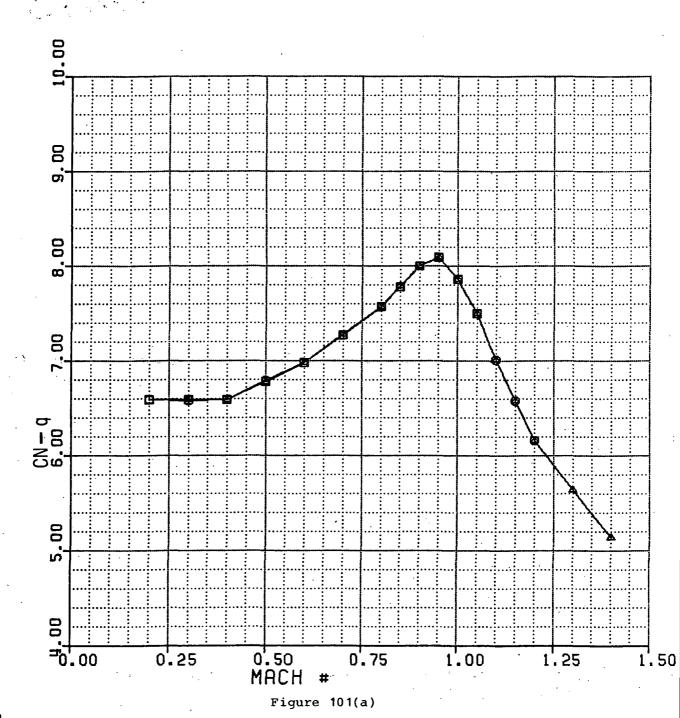


Figure 100(f)

CN-q VS MACH#

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

9 ALT = S.L. M# = .2 TO 1.05 9 ALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4

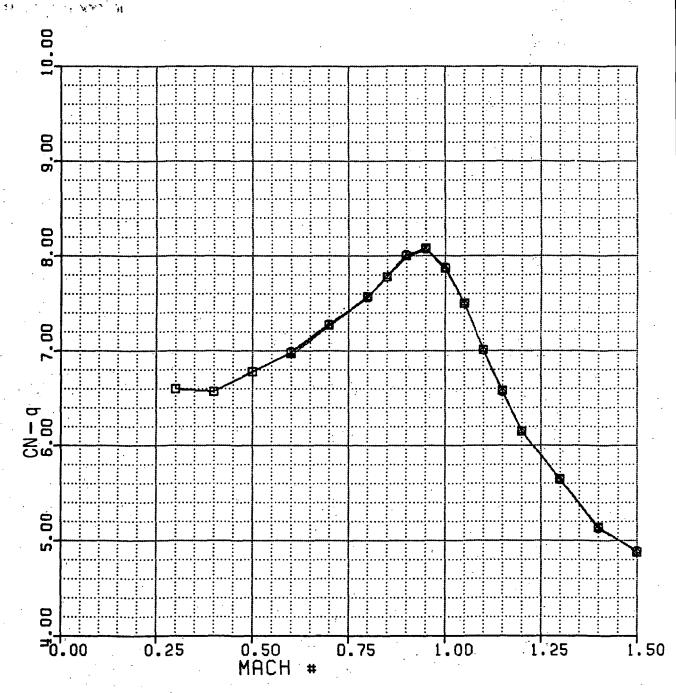


CN-q VS MACH#

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 A ALT = 50K M# = .6 TO 1.5

ALT = 50K M# = .6 TO 1.5 ORIGINAL PAGE IS OF POOR QUALITY



7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = S.L. ALP: -4 TO 22 0 ALT = 10K ALP: -4 TO 22

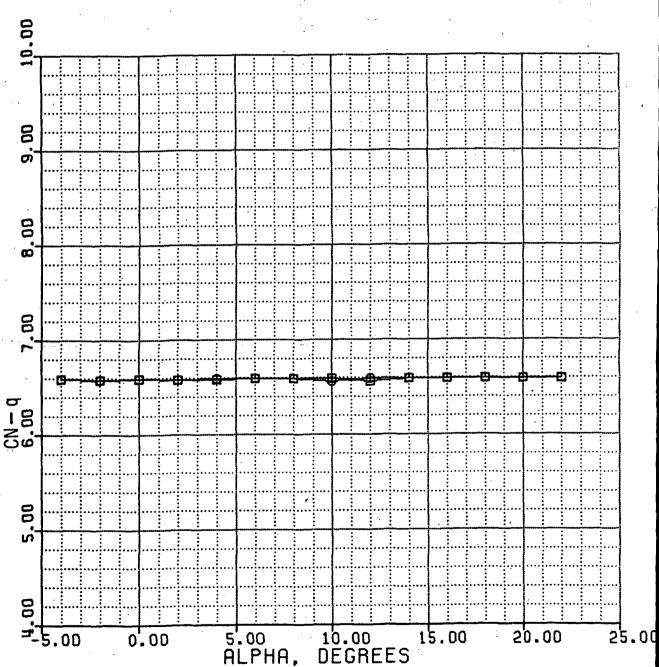
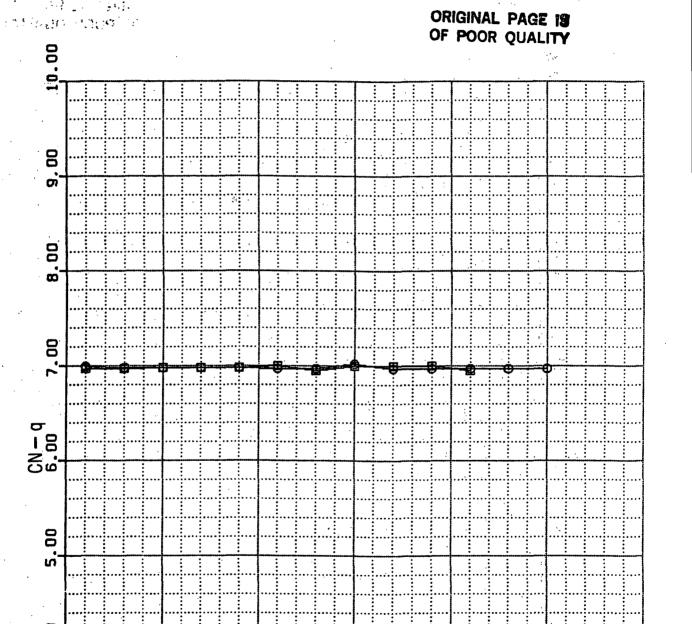


Figure 102(a)

7-26-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20



0.00

5.00 10.00 ALPHA, DEGREES

7-26-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: 0 T0 10

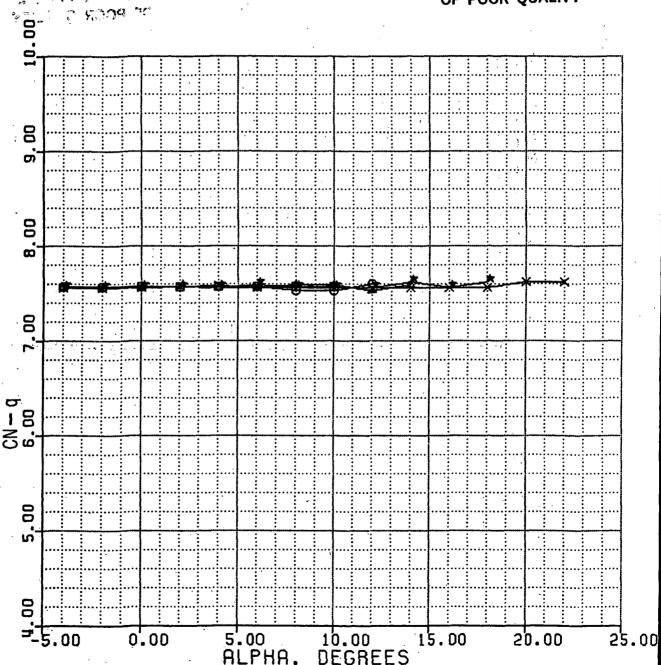
O ALT = 20K ALP: -4 T0 12

A ALT = 30K ALP: -4 T0 14

A ALT = 40K ALP: -4 T0 18

X ALT = 50K ALP: -4 T0 22

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 X_{i}^{N}

7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P RLT = 20K RLP: 0 T0 10

P RLT = 30K RLP: -2 T0 12

A RLT = 40K RLP: -4 T0 14

RLT = 50K RLP: -4 T0 18
```

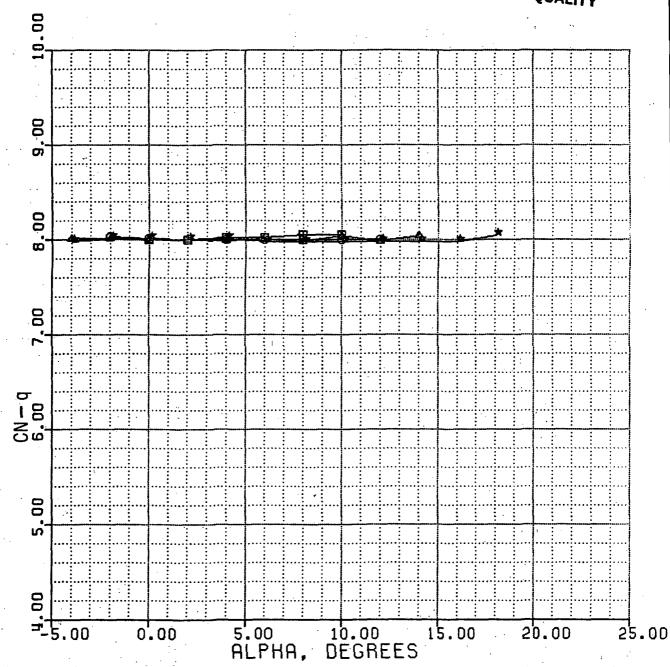


Figure 102(d)

.);;...

7-27-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

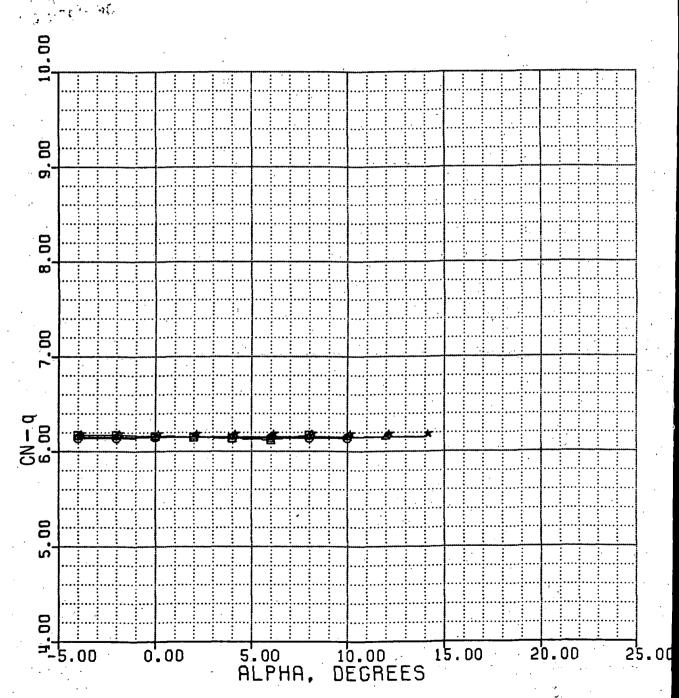


Figure 102(e)

10 47.15 A

7-27-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8

O ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12

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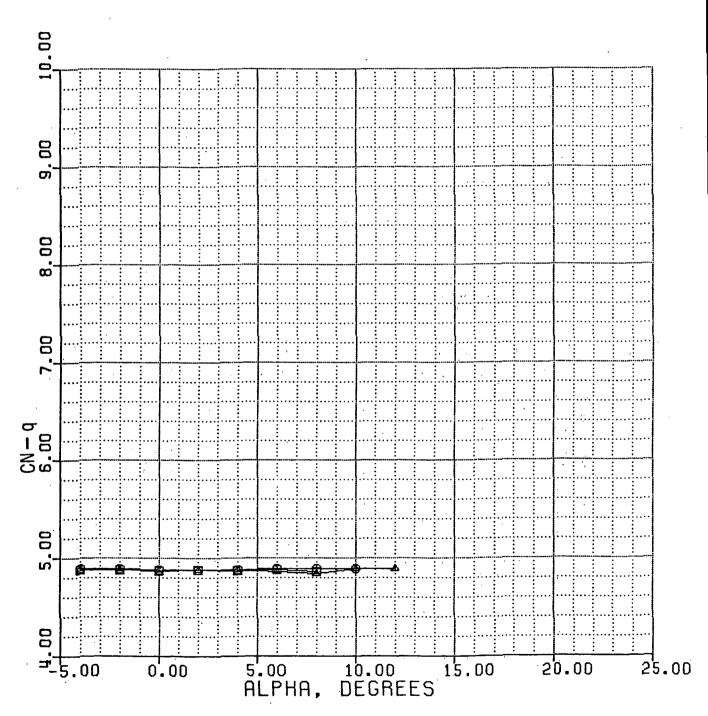


Figure 10.2(f)

Cy - ROLL RATE VS MACH

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

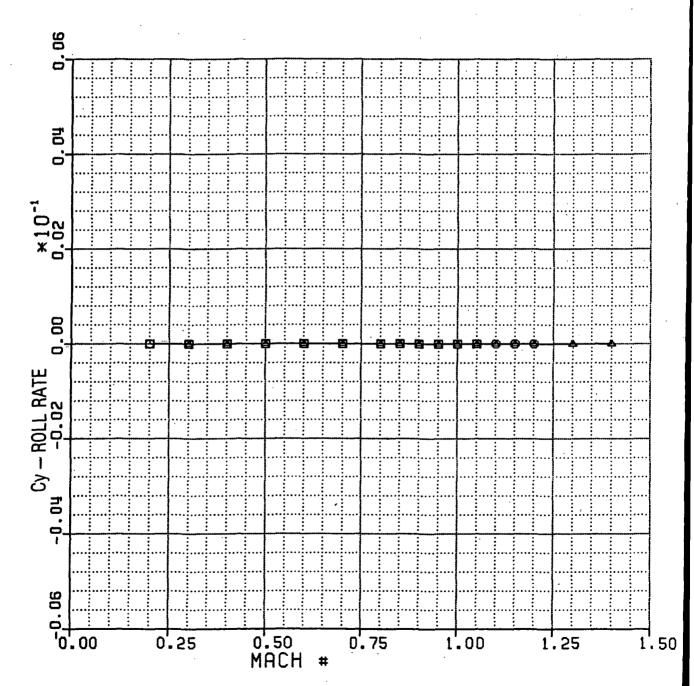
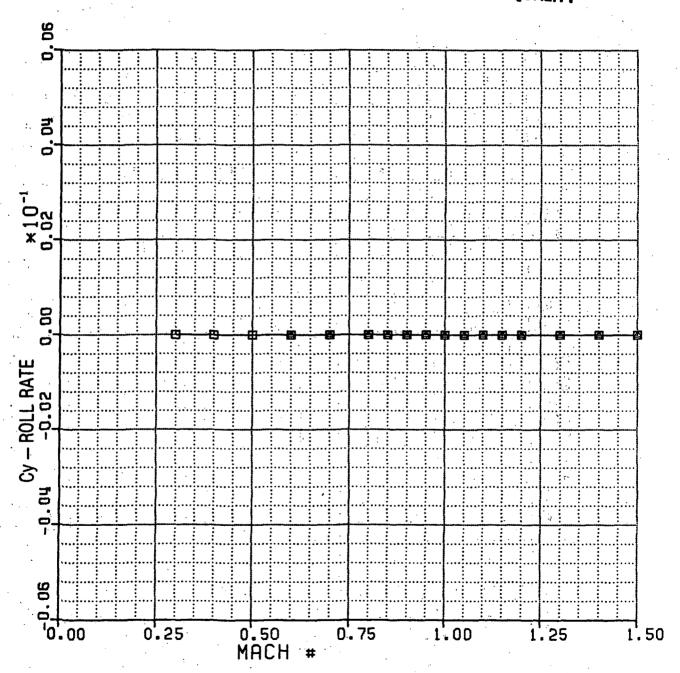


Figure 103(a)

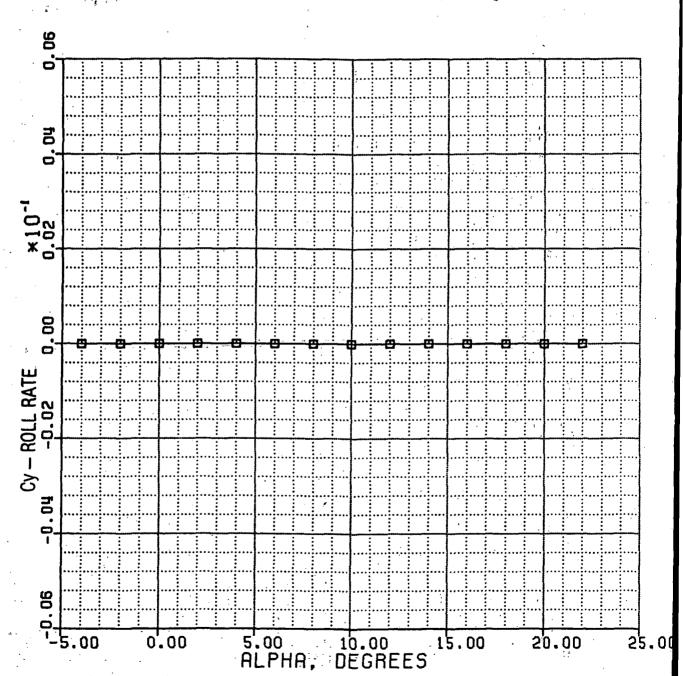
Cy — ROLL RATE VS MACH

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K



7-26-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = S.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22



7-26-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 10K ALP: -4 TO 16 0 ALT = 20K ALP: -4 TO 20

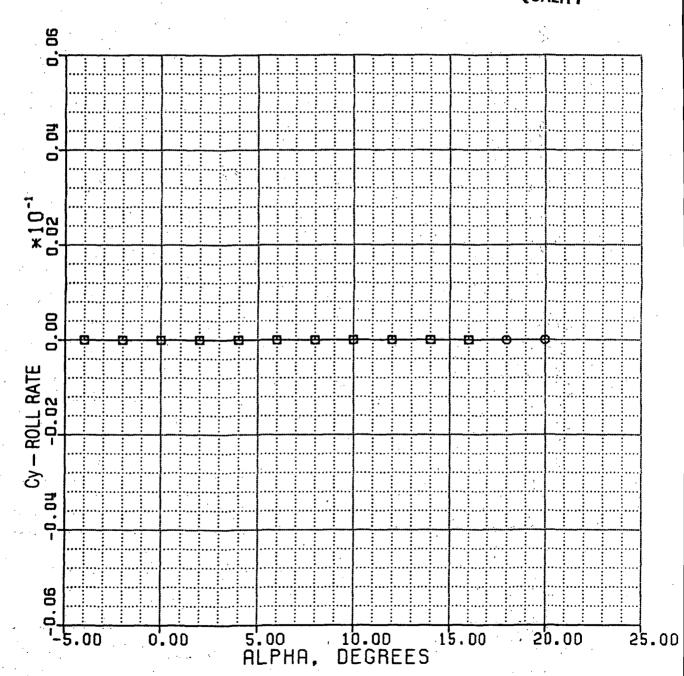


Figure 104(b)

7-26-83 X-29A M# = 0.8 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: 0 T0 10

P ALT = 20K ALP: -4 T0 12

A ALT = 30K ALP: -4 T0 14

A ALT = 40K ALP: -4 T0 18

A ALT = 50K ALP: -4 T0 22

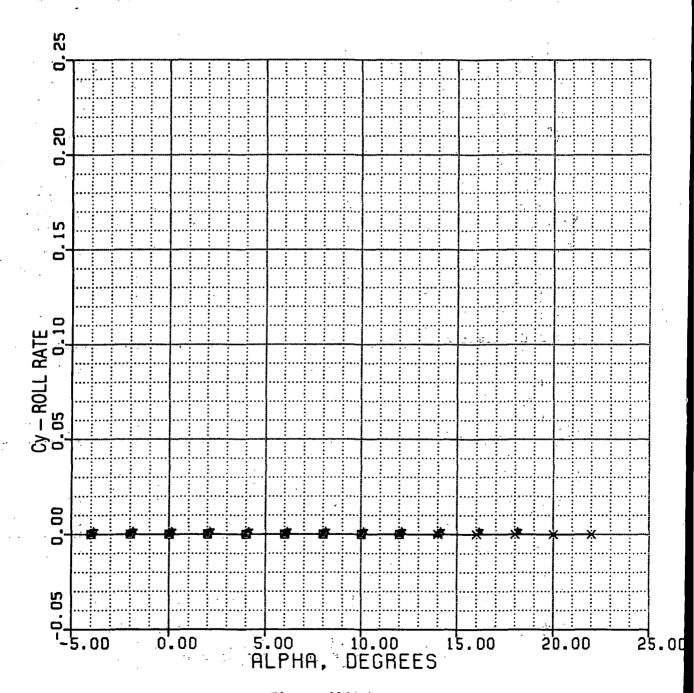


Figure 104(c)

7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: 0 TO 10

P ALT = 30K ALP: -2 TO 12

A ALT = 40K ALP: -4 TO 14

ALT = 50K ALP: -4 TO 18

THE HEART TO

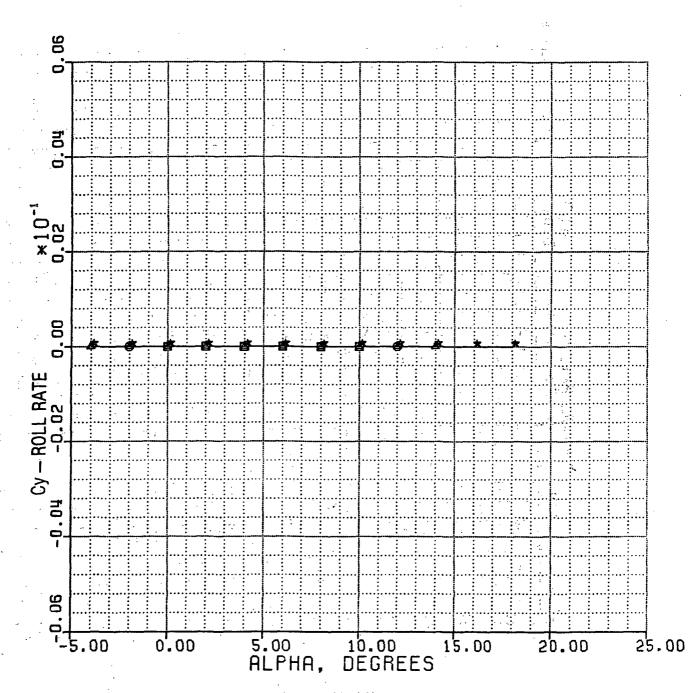


Figure 104(d)

7-27-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14

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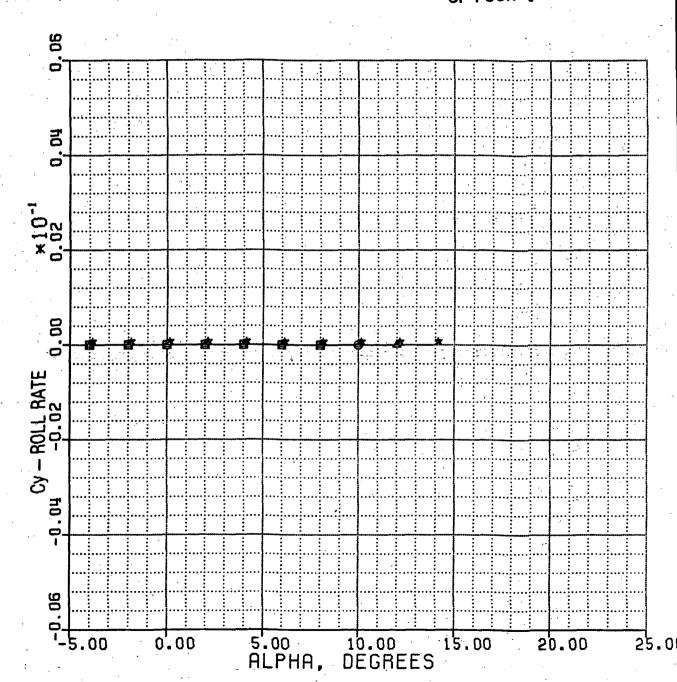


Figure 104(e)

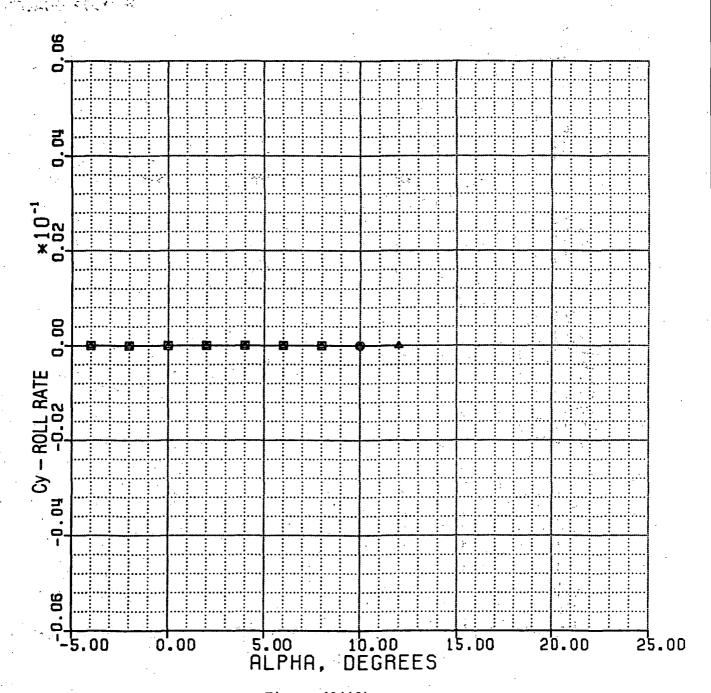
7-27-83 X-29A M# = 1.5 NORMAL MODE

XCG = 451.0 WT = 15K ALPHA TRIM

P RLT = 30K RLP: -4 TO 8

P PLT = 40K RLP: -4 TO 10

A RLT = 50K RLP: -4 TO 12



CI - ROLL RATE VS MACH

7-6-83 X-29A = 1-G TRIM > NORMALS MODE XCG = 451.0 WT = 15K

O ALT = S.L. M# = .2 TO 1.05 O ALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4

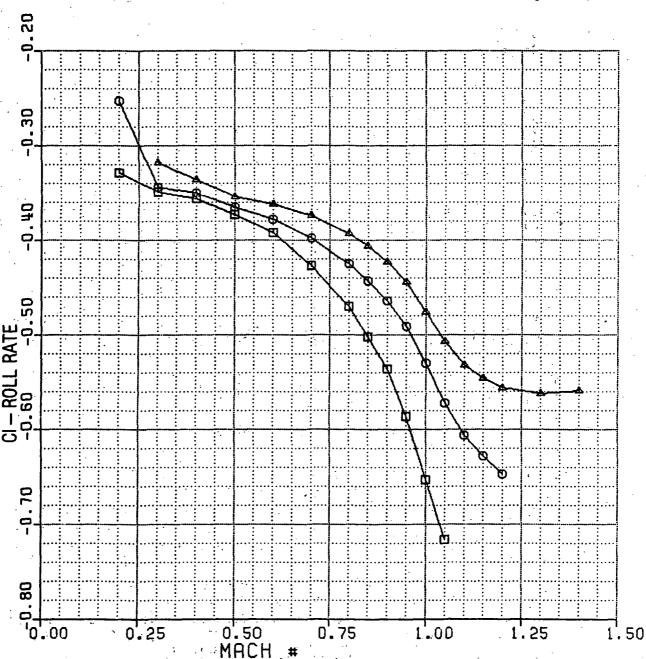


Figure 105(a)

CI - ROLL RATE VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

N34 : 41.

ा दशुः, स्त्रः त

_______ ALT = 30K M# = .3 TO 1.59 ALT = 40K M# = .6 TO 1.5 ____ ALT = 50K M# = .6 T0 1.5

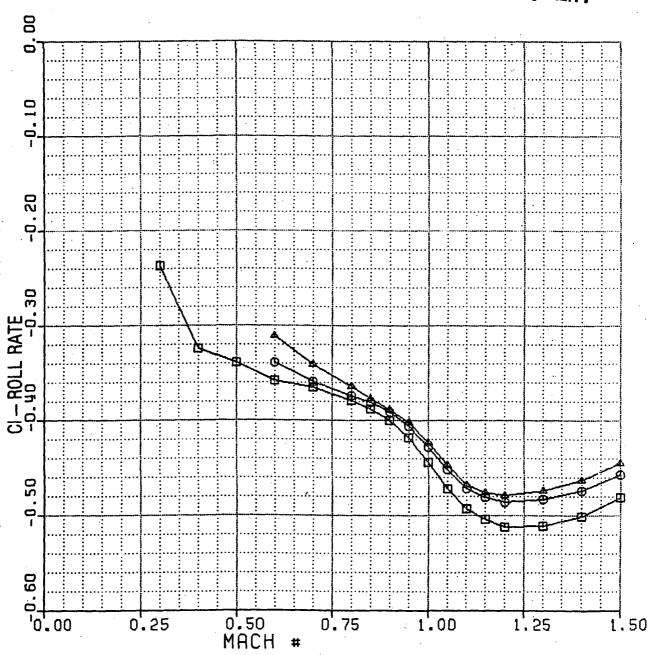


Figure 105(b)

6-16-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

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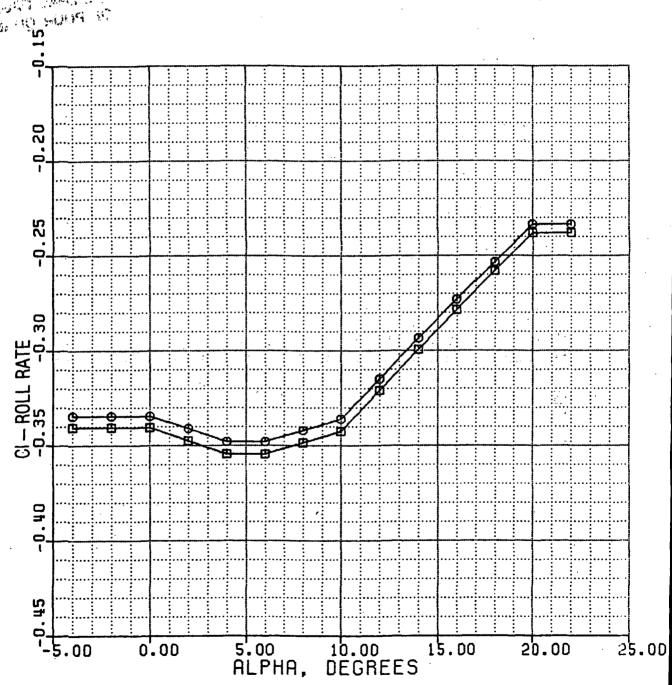
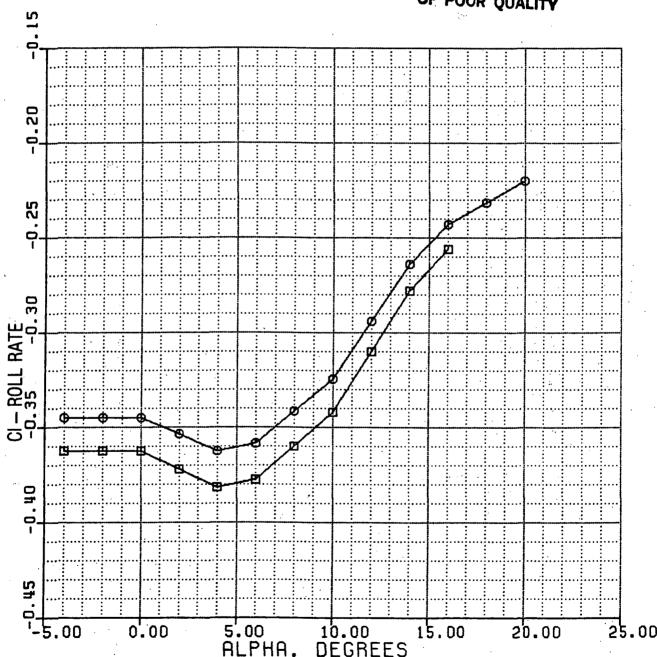


Figure 106(a)

6-17-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 10K ALP: -4 TO 16 0 ALT = 20K ALP: -4 TO 20

e nace si



6-30-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALP = 30K ALP: -4 TO 14

A ALT = 40K ALP: -4 TO 18

A ALT = 50K ALP: -4 TO 22

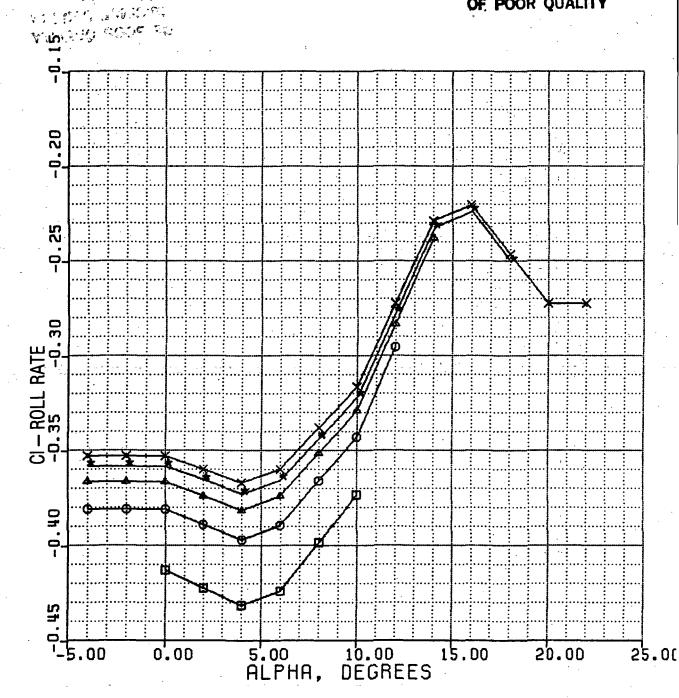


Figure 106(c)

7-1-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

PALT = 20K ALP: 0 T0 10

PALT = 30K ALP: -2 T0 12

ALT = 40K ALP: -4 T0 14

ALT = 50K ALP: -4 T0 18

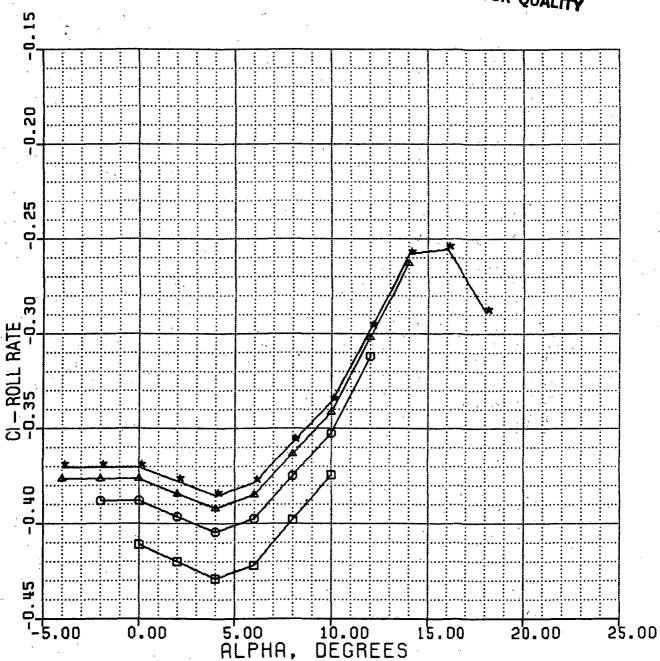


Figure 106(d)

7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
```

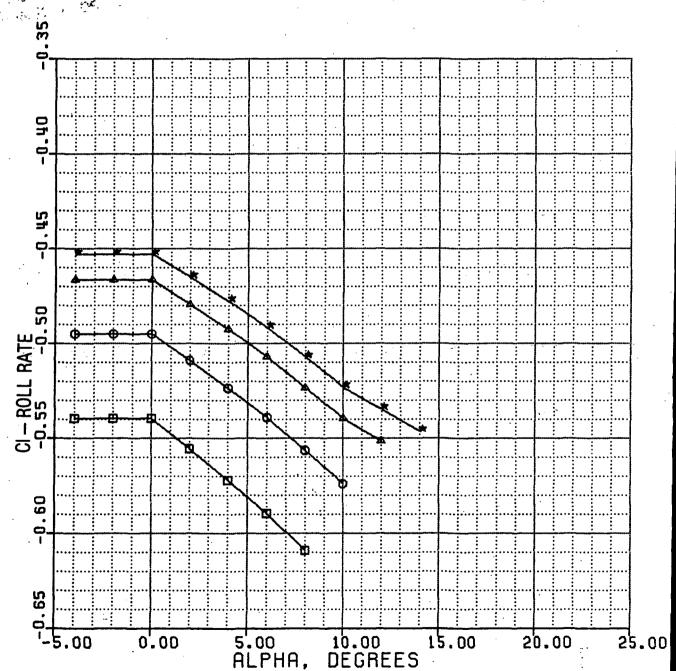


Figure 106(e)

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

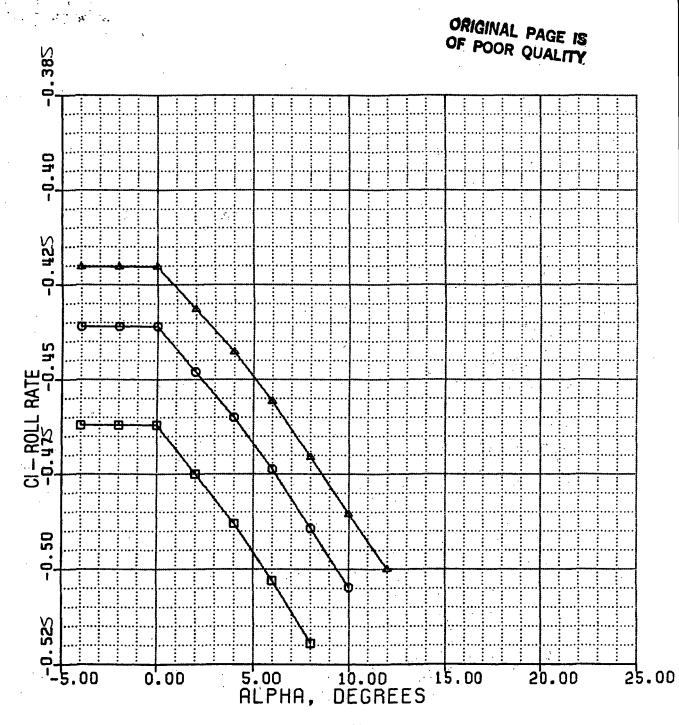
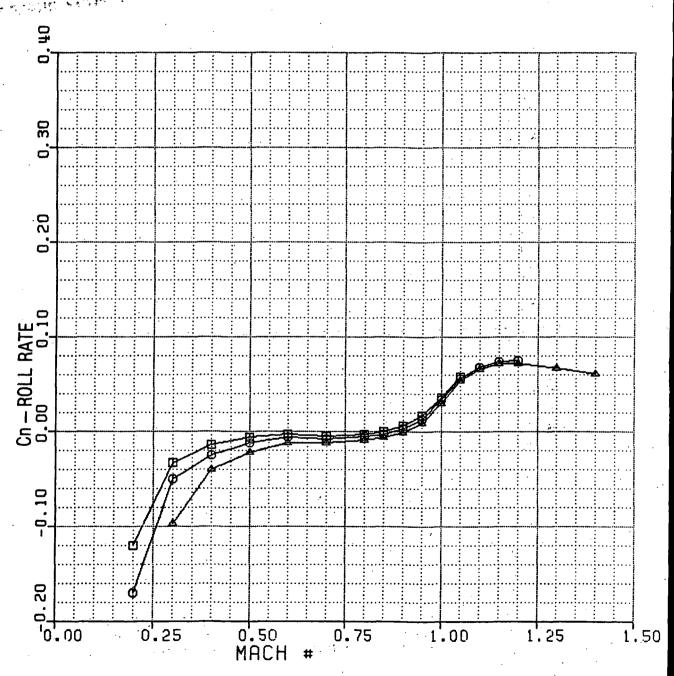


Figure 106(f)

Cn - ROLL RATE VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

9 ALT = S.L. M# = .2 TO 1.05 9 ALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4



Cn - ROLL RATE VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

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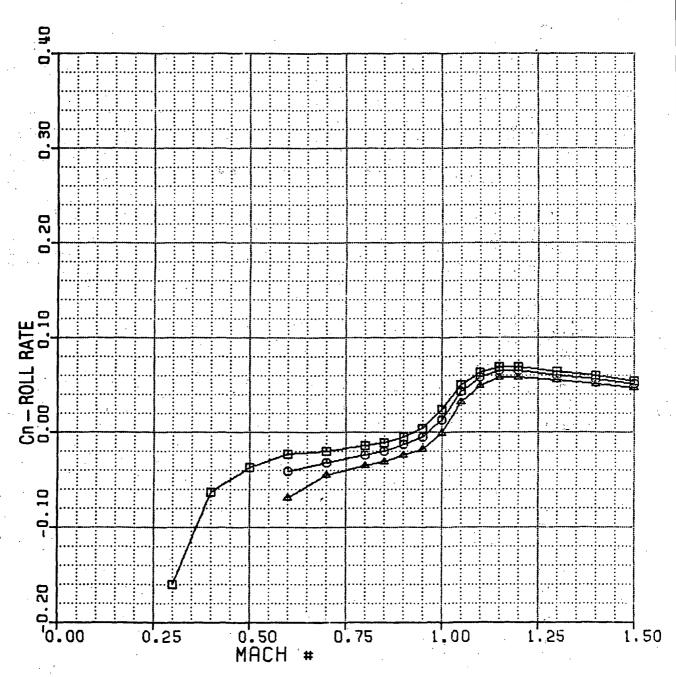
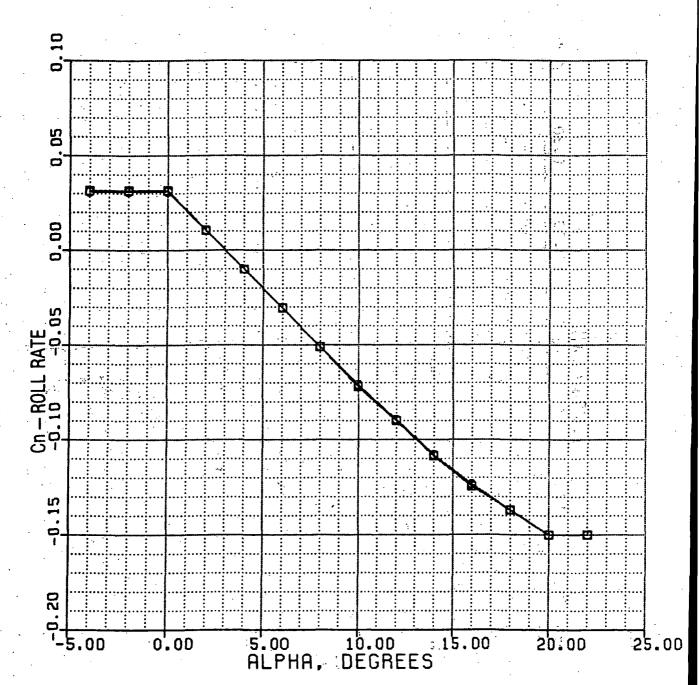


Figure 107(b)

6-16-83 X-29A M# = 0.4 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM



- Figure 108(a)

6-17-83 X-29A M# = 0.6 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

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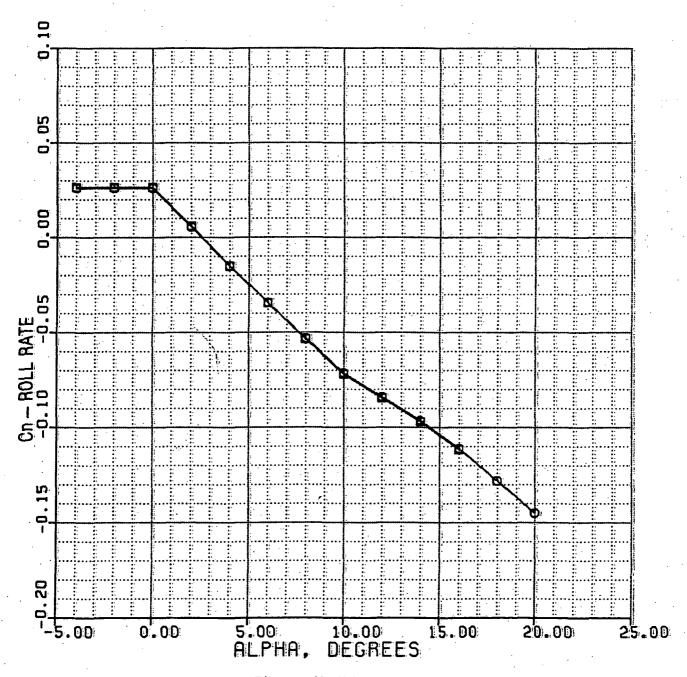


Figure 108(b)

6-30-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

A ALP = 30K ALP: -4 TO 14

A ALT = 40K ALP: -4 TO 18

A ALT = 50K ALP: -4 TO 22

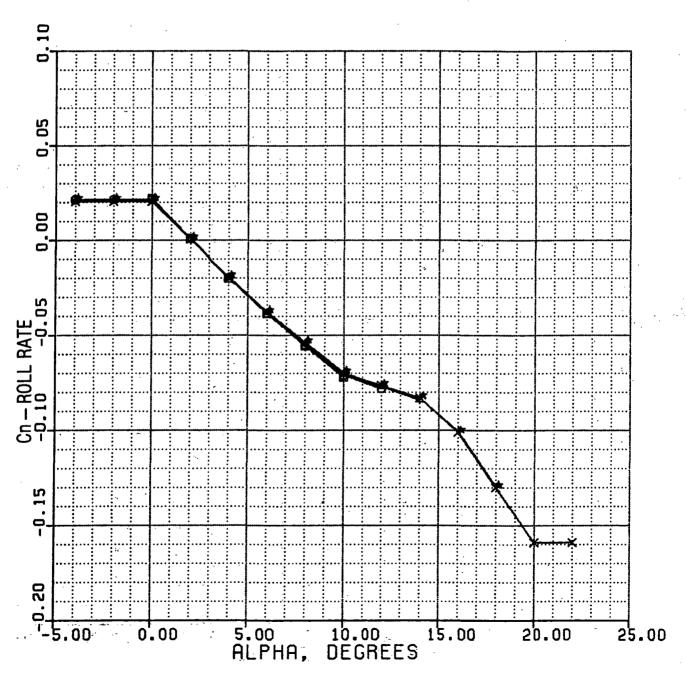


Figure 108(c)

7-1-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: 0 T0 10

P ALT = 30K ALP: -2 T0 12

A ALT = 40K ALP: -4 T0 14

A ALT = 50K ALP: -4 T0 18
```

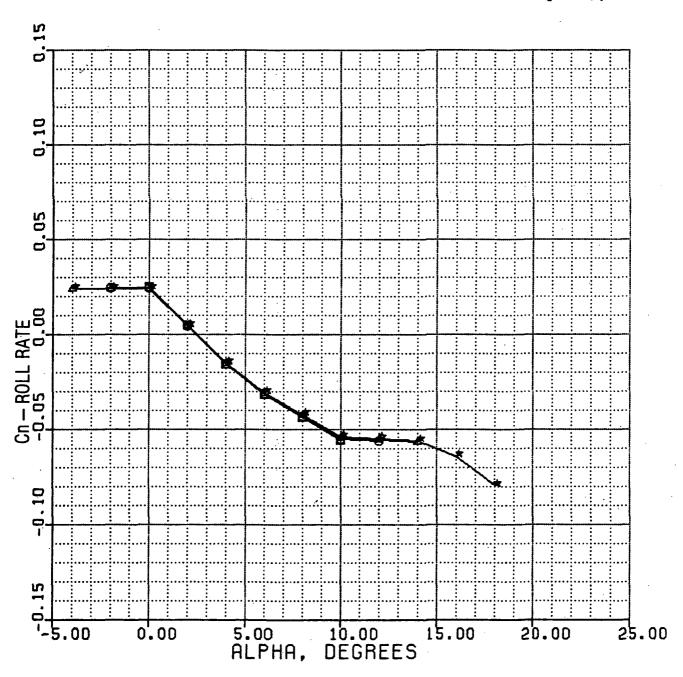


Figure 108(d)

7-1-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 20K ALP: -4 TO 8

9 ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14

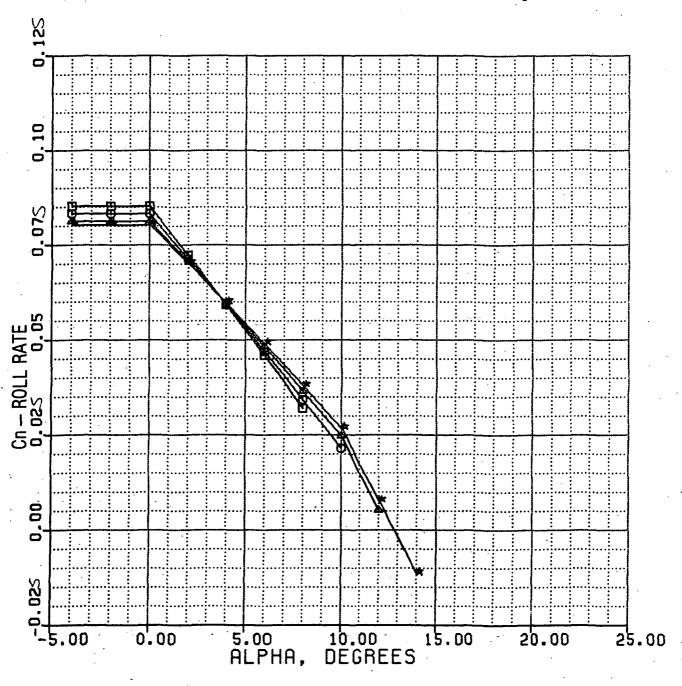


Figure 108(e)

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
9 ALT = 30K ALP: -4 TO 8

9 ALT = 40K ALP: -4 TO 10

A ALT = 50K ALP: -4 TO 12
```

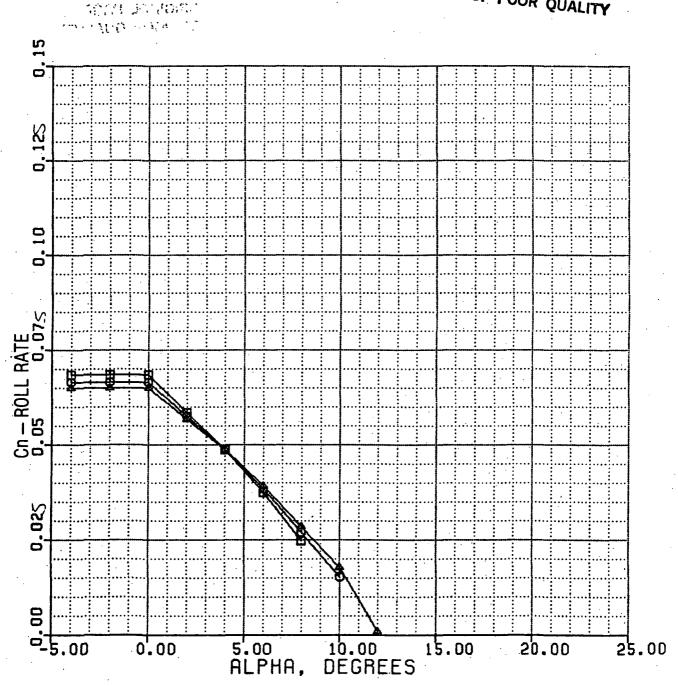


Figure 108(f)

Cy - YAW RATE VS MACH

7-27-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

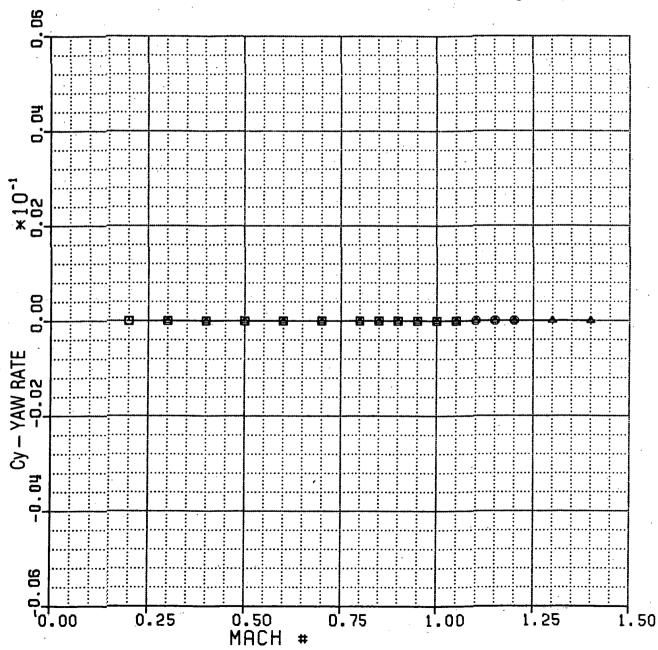


Figure 109(a)

Cy - YAW RATE VS MACH

7-27-83 X-29A 1-G TRIM NORMAL MODE

XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 A ALT = 50K M# = .6 TO 1.5

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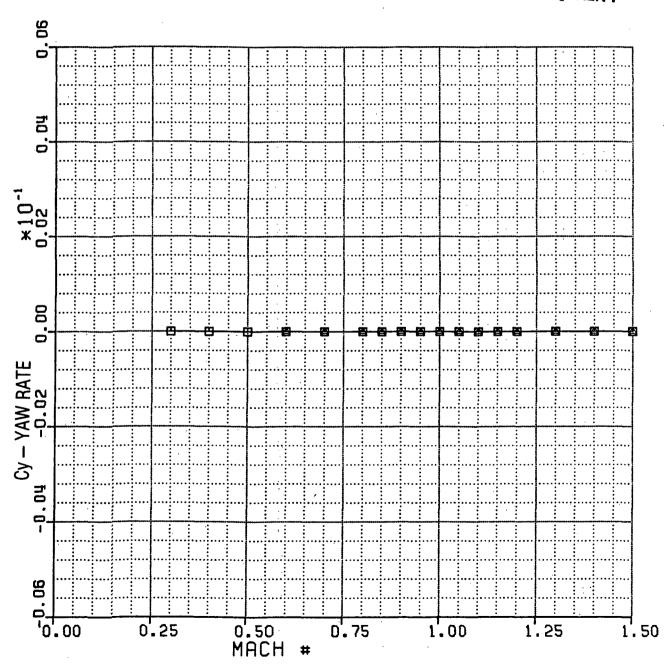


Figure 109(b)

7-26-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

0 ALT = 5.L. ALP: -4 TO 22 0 ALT = 10K ALP: -4 TO 22

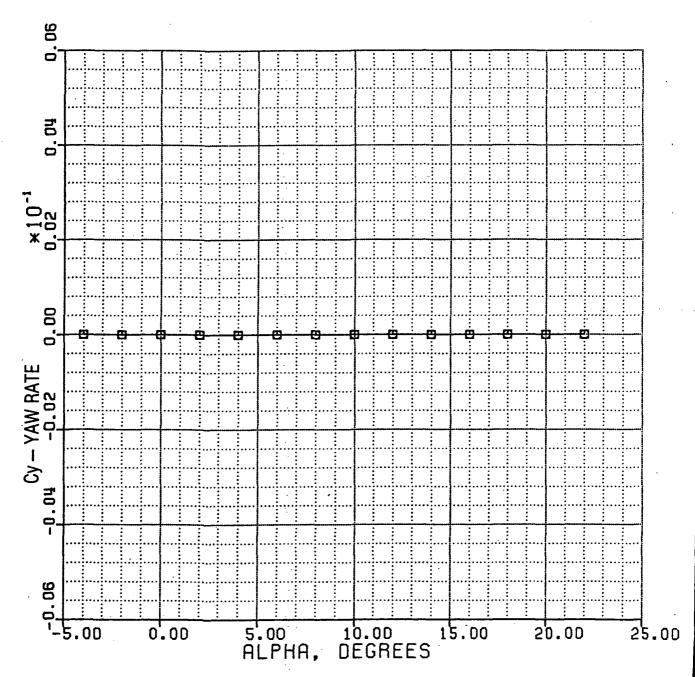


Figure 110(a)

7-26-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

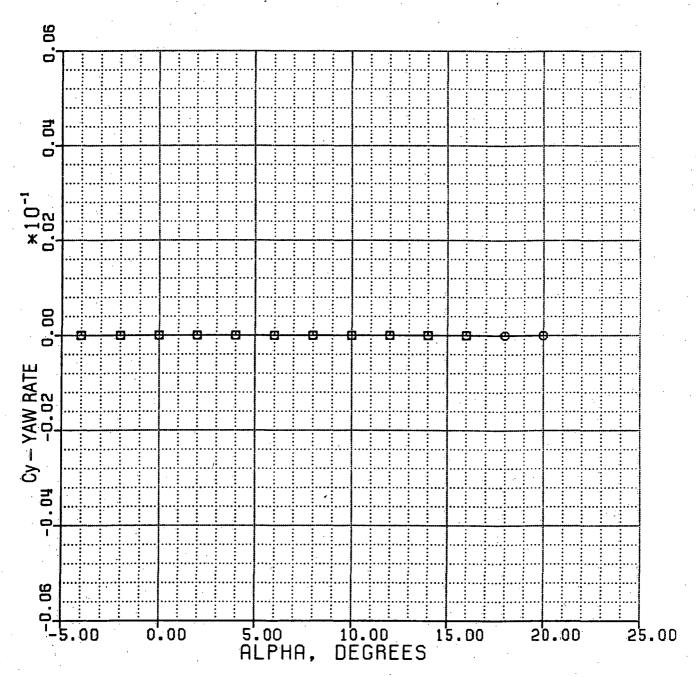


Figure 110(b)

7-26-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
9 ALT = 10K ALP: 0 T0 10

9 ALT = 20K ALP: -4 T0 12

A ALT = 30K ALP: -4 T0 14

** ALT = 40K ALP: -4 T0 18

** ALT = 50K ALP: -4 T0 22
```

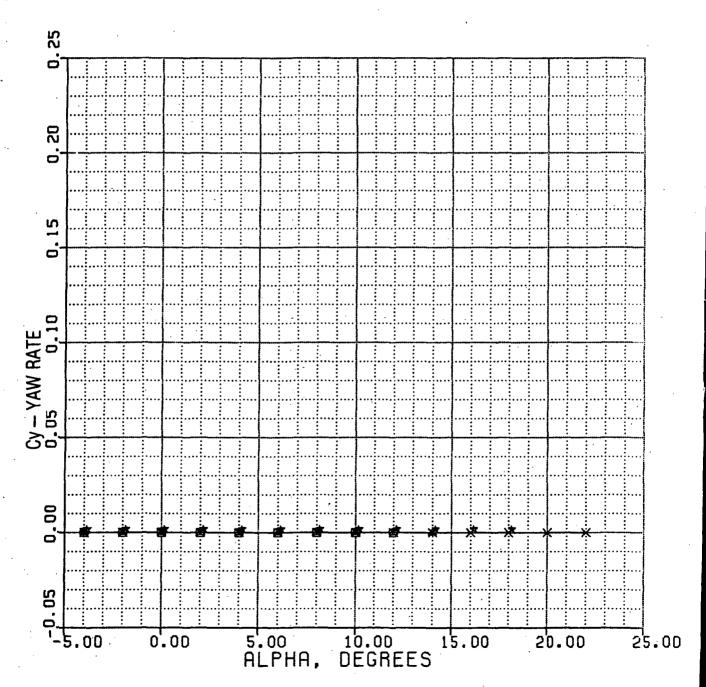


Figure 110(c)

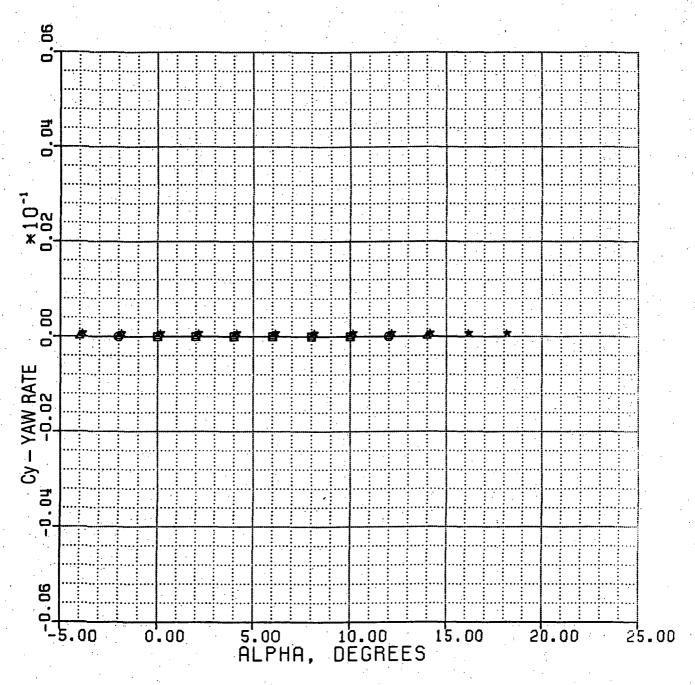
7-27-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: 0 T0 10

P ALT = 30K ALP: -2 T0 12

A ALT = 40K ALP: -4 T0 14

A ALT = 50K ALP: -4 T0 18
```



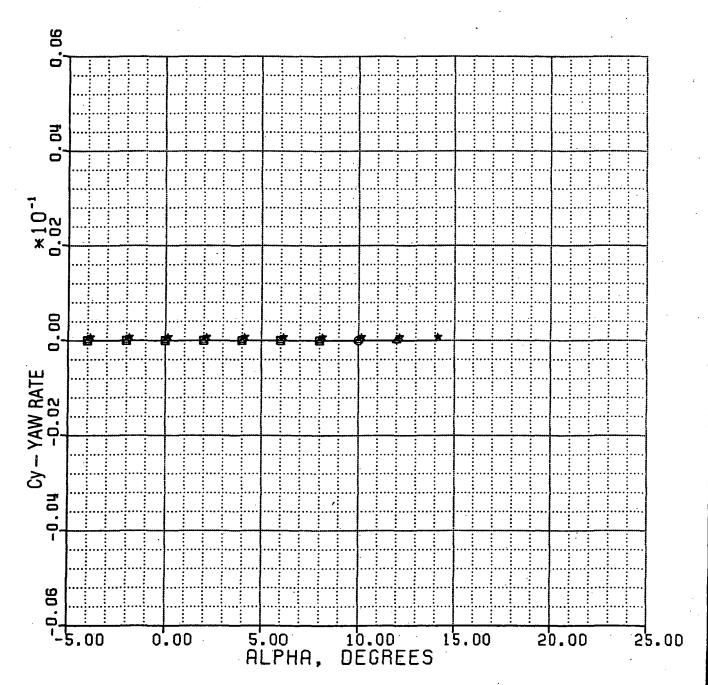
7-27-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14

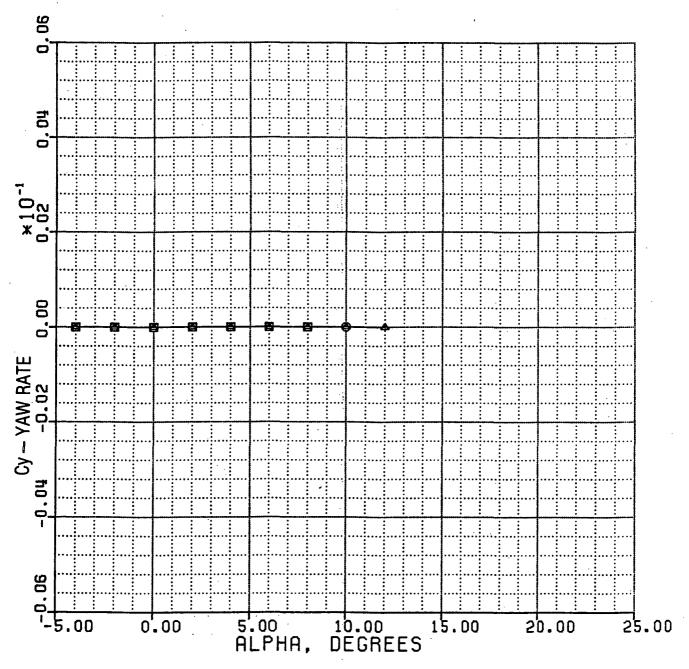


7-27-83 X-29A M# = 1.5 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 30K ALP: -4 TO 8

9 ALT = 40K ALP: -4 TO 10

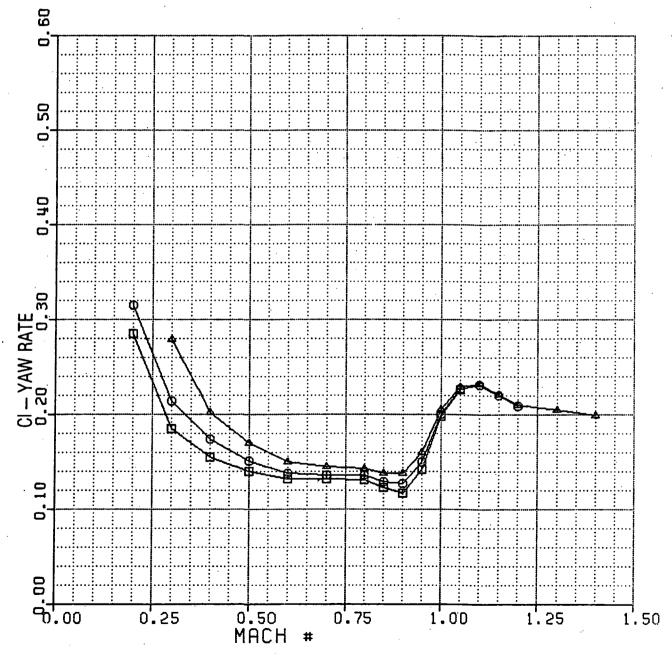
A ALT = 50K ALP: -4 TO 12



CI - YAW RATE VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

G ALT = S.L. M# = .2 TO 1.05 G ALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4

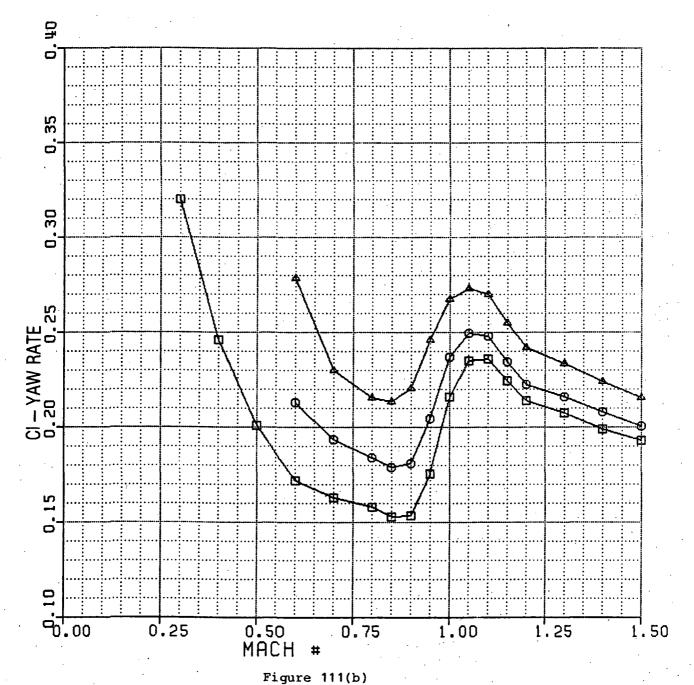


CI - YAW RATE VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 A ALT = 50K M# = .6 TO 1.5

The state of the s



6-16-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

9 ALT = 5.L. ALP: -4 TO 22 9 ALT = 10K ALP: -4 TO 22

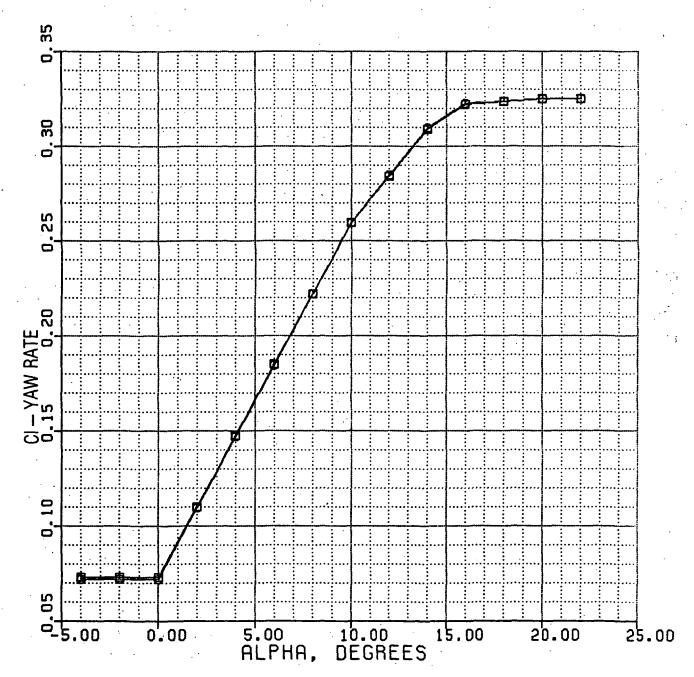


Figure 112(a)

6-17-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 O P ALT = 20K ALP: -4 TO 20

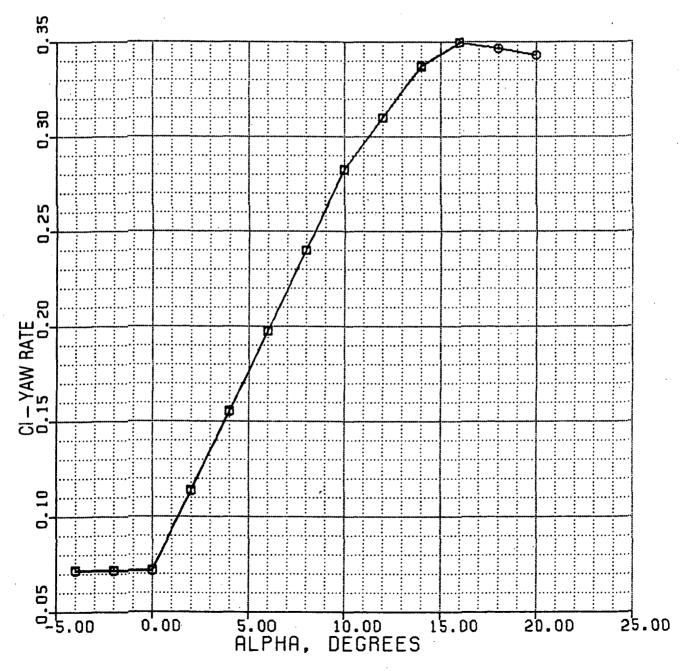


Figure 112(b)

6-30-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 10K ALP: 0 TO 10

P ALT = 20K ALP: -4 TO 12

ALP = 30K ALP: -4 TO 14

ALT = 40K ALP: -4 TO 18

ALT = 50K ALP: -4 TO 22
```

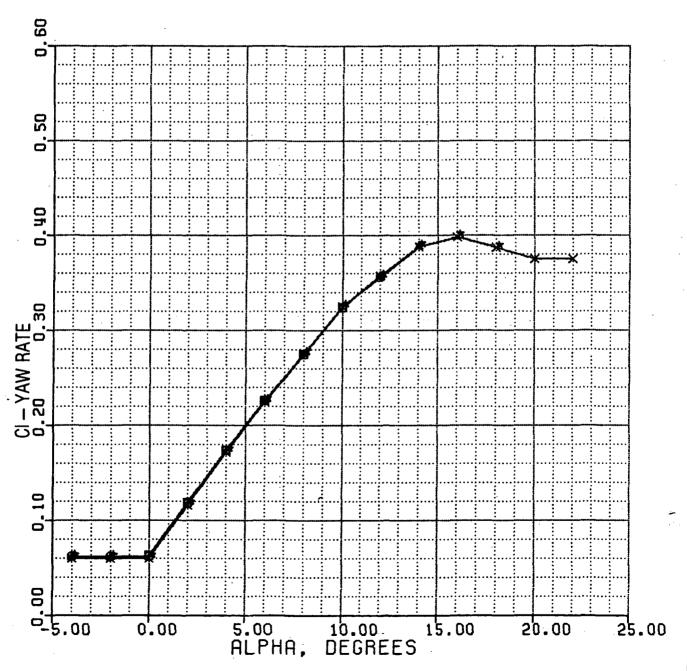


Figure 112(c)

CI - YAW RATE VS ALPHA

7-1-83 X-29A M# = 0.9 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

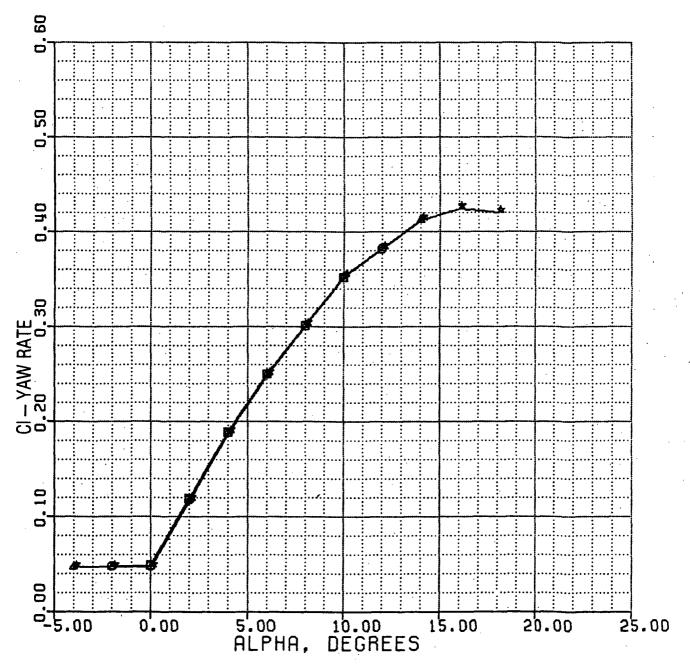


Figure 112(d)

CI - YAW RATE VS ALPHA

7-1-83 X-29A M# = 1.2 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: -4 TO 8

P ALT = 30K ALP: -4 TO 10

A ALT = 40K ALP: -4 TO 12

A ALT = 50K ALP: -4 TO 14
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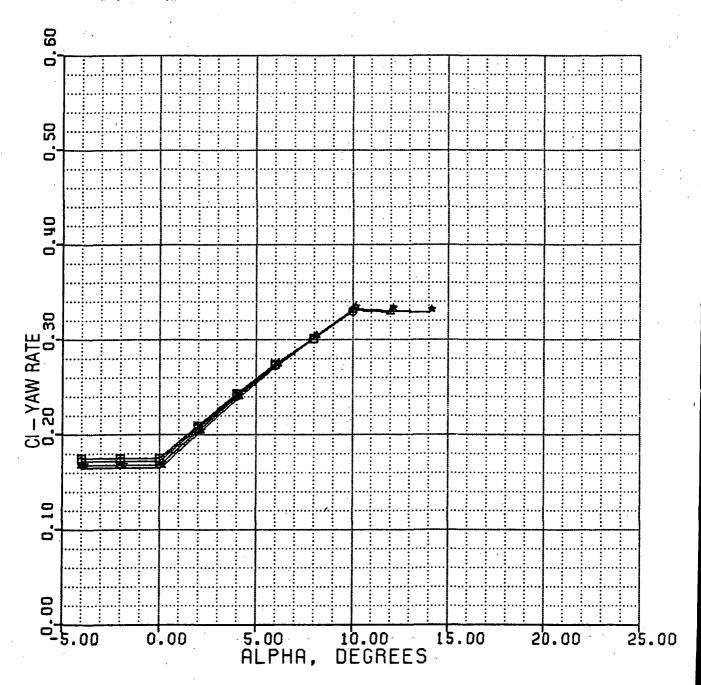
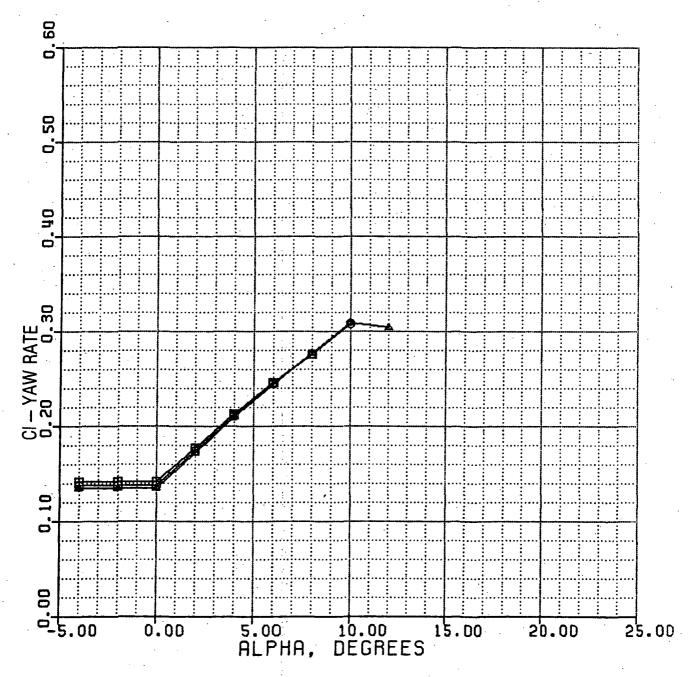


Figure 112(e)

CI - YAW RATE VS ALPHA

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

G ALT = 30K ALP: -4 TO 8
G ALT = 40K ALP: -4 TO 10
A ALT = 50K ALP: -4 TO 12



Cn - YAW RATE VS MACH

7-6-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

9 ALT = S.L. M# = .2 TO 1.05 9 ALT = 10K M# = .2 TO 1.2 A ALT = 20K M# = .3 TO 1.4

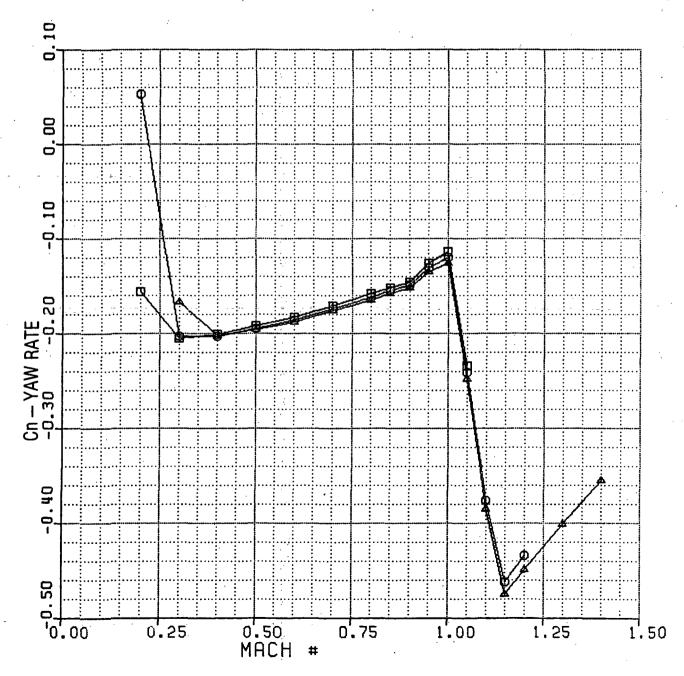


Figure 113(a)

Cn — YAW RATE VS MACH

7-7-83 X-29A 1-G TRIM NORMAL MODE XCG = 451.0 WT = 15K

P ALT = 30K M# = .3 TO 1.5 P ALT = 40K M# = .6 TO 1.5 ALT = 50K M# = .6 TO 1.5

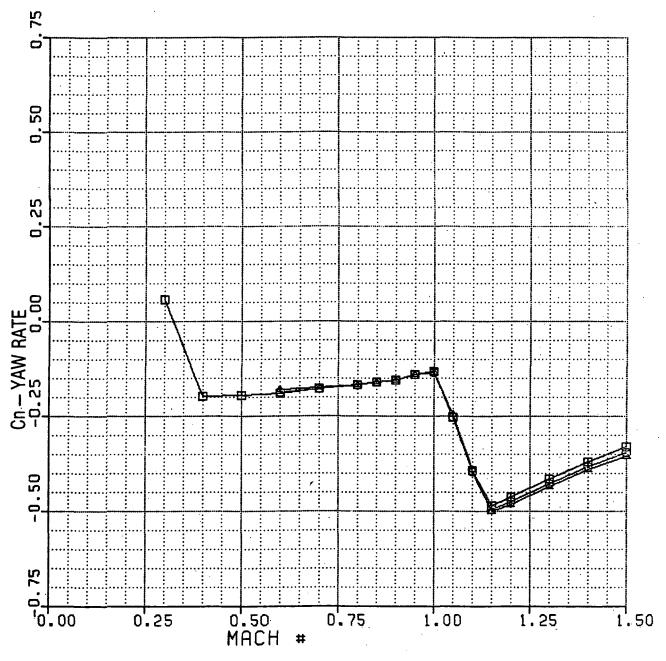


Figure 113(b)

Cn — YAW RATE VS ALPHA

6-16-83 X-29A M# = 0.4 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

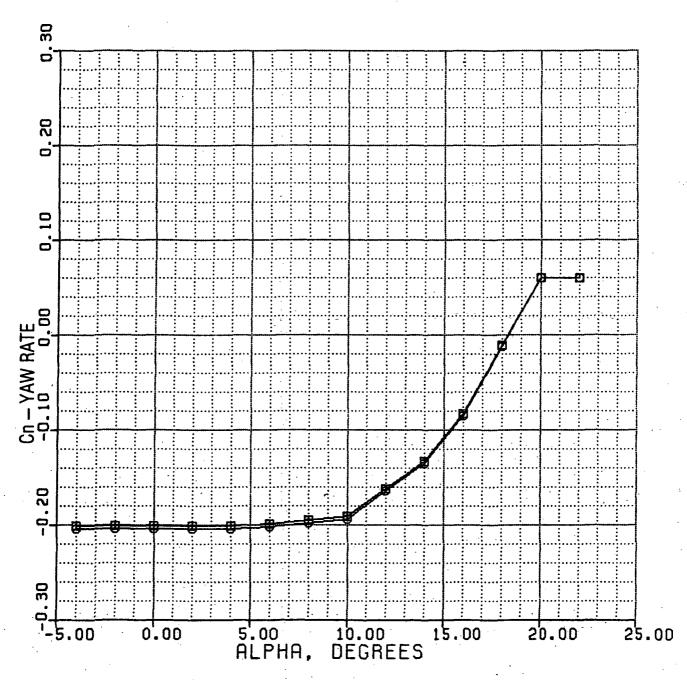


Figure 114(a)

Cn — YAW RATE VS ALPHA

6-17-83 X-29A M# = 0.6 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: -4 TO 16 P ALT = 20K ALP: -4 TO 20

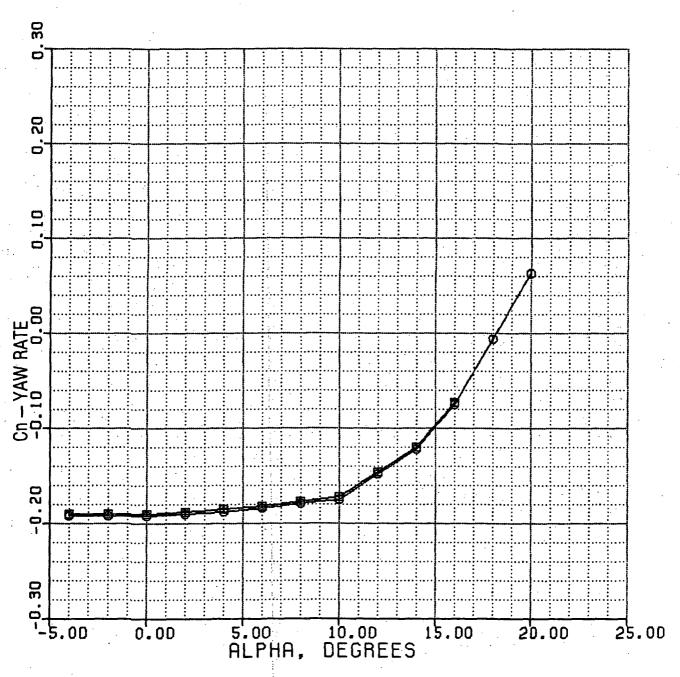


Figure 114(b)

Cn — YAW RATE VS ALPHA

6-30-83 X-29A M# = 0.8 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

P ALT = 10K ALP: 0 T0 10
P ALT = 20K ALP: -4 T0 12
A ALP = 30K ALP: -4 T0 14
A ALT = 40K ALP: -4 T0 18
A ALT = 50K ALP: -4 T0 22

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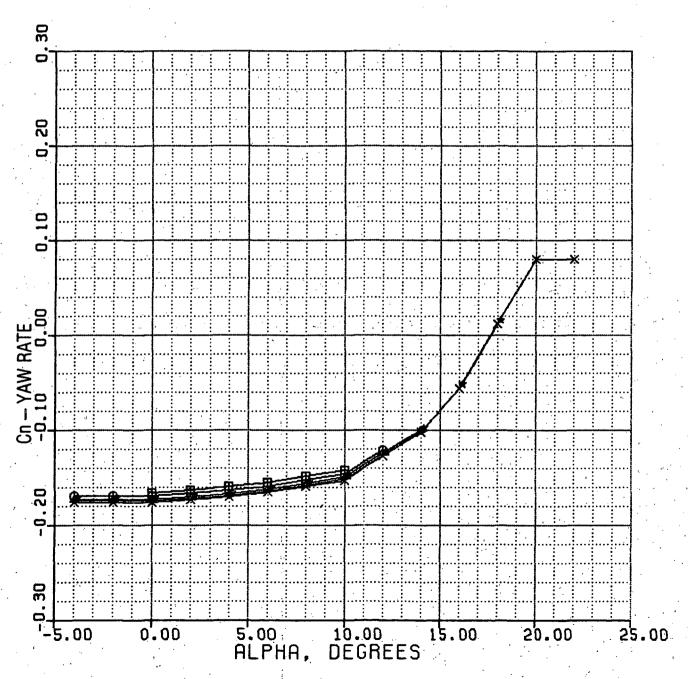


Figure 114(c)

Cn - YAW RATE VS ALPHA

7-1-83 X-29A M# = 0.9 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

```
P ALT = 20K ALP: 0 T0 10

P ALT = 30K ALP: -2 T0 12

A ALT = 40K ALP: -4 T0 14

A ALT = 50K ALP: -4 T0 18
```

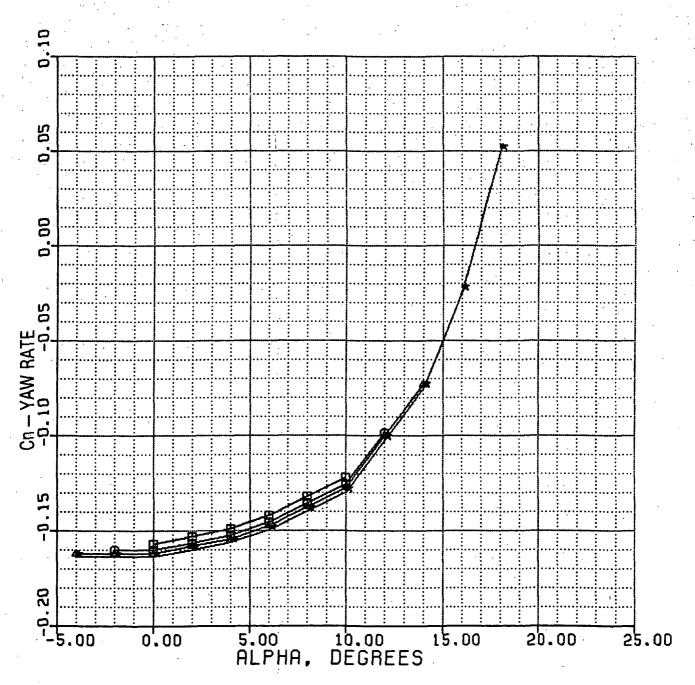


Figure 114(d)

Cn = YAW RATE VS ALPHA

7-1-83 X-29A M# = 1.2 NØRMAL MØDE XCG = 451.0 WT = 15K ALPHA TRIM

O ALT = 20K ALP: -4 TO 8
O ALT = 30K ALP: -4 TO 10
ALT = 40K ALP: -4 TO 12
ALT = 50K ALP: -4 TO 14

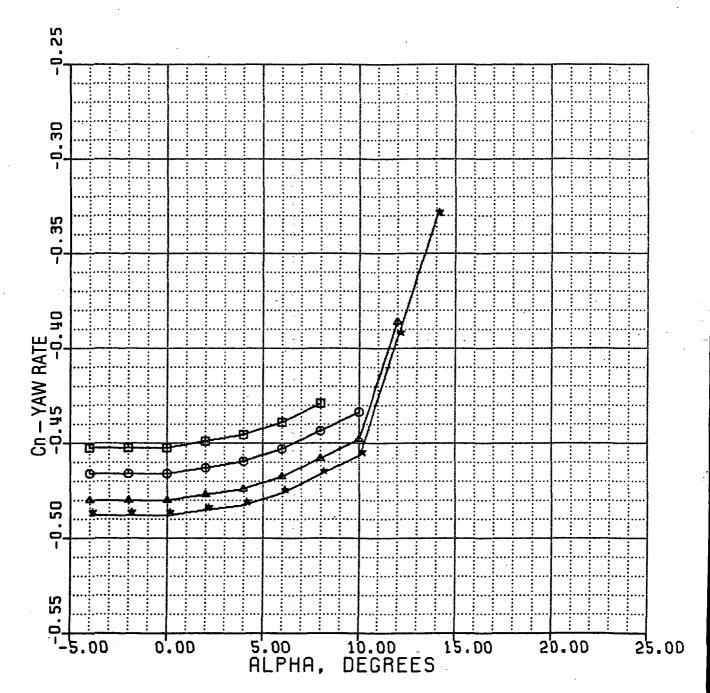


Figure 114(e)

Cn - YAW RATE VS ALPHA

7-1-83 X-29A M# = 1.5 NORMAL MODE XCG = 451.0 WT = 15K ALPHA TRIM

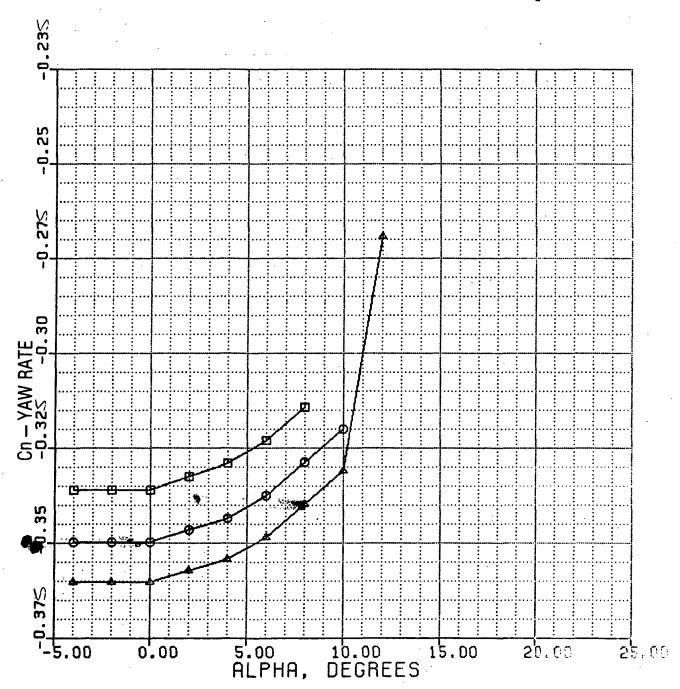


Figure 114(f)

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7. Author(s) Gerald D. Budd			8. Performing Organization Report No. H-1203	
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Dryden Flight Research Facility P.O. Box 273				
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